



August 4, 2026

Natalie Thomsen, Town Planner
Town of Windham
8 School Road
Windham, ME 04062

**Re: Response to Review Comments - Major Subdivision Preliminary Plan Application
Legacy Village Retirement Community on Webb Road
Robie Holdings, LLC - Applicant**

Dear Natalie:

Attached are revised plans and supplemental information for the above referenced project in response to review comments received from the Town Staff, Planning Board, Portland Water District and the Town's Engineering Consultant. The following is a summary of the enclosed documents:

Wastewater Disposal System for Retirement Community

Enclosed is the design for the Engineered Wastewater Disposal System to accommodate a design flow of 6,750 gallons per day (up to 75 bedrooms). We have included a complete copy of the application submitted to the Maine Department of Health and Human Services (DHHS), and a copy of the Approval Letter from DHHS.

Portland Water District Coordination

The Portland Water District has reviewed the project plans and provided comments. The enclosed plans have been revised to address the review comments from PWD and these plans have been provided to PWD for approval. An Ability to Serve Approval Letter, including approval of the off-site water main extension, will be included with the Final Plan application.

Traffic Engineering

Enclosed is a Vehicle Traffic Analysis Report prepared by Barton & Loguidice.

Landscaping Plan and Buffer Yards

The plans have been revised to designate retained natural buffer yard and supplemental landscaping in the perimeter buffer and street buffer as required in §120-511. A table has been added to the Site & Landscaping Plans to designate the species and size of street trees and buffer yard plantings. We are not proposing to specify landscaping around the individual home foundations because each homeowner will have a

preference as to the amount and type of landscaping that they would prefer to maintain in direct vicinity to their unit.

Basement Entry

Based on the current proposed grading, we anticipate that Units 7, 8 and 9 will be constructed with a basement that would require a bulkhead or doghouse entry. We have added bulkheads to those units on the project plans. The remaining units we anticipate will be constructed on a slab with no basement, or built with a full walk-out basement. This information will be further detailed on the Condominium Plat that will be submitted with the Final Plan.

Maine Historic Preservation Commission

Enclosed is a letter from the MHPC indicating that the project will not impact any properties of historical significance.

Exterior Lighting

Exterior light fixtures will be installed over the garage doors on each of the dwelling units, and on the porches adjacent to the driveways. These building-mounted lights will provide sufficient ambient lighting for the adjacent parking areas. A light pole has been proposed at the project entrance. The light pole will be metered privately by the Condominium Association. We have included photometrics and spec sheets for the proposed light fixture mounted on a pole.

Multifamily Development Standards and Open Space

We are proposing to install a network of walking trails through the woods that will extend off the end of the paved sidewalk and follow the utility line where the sewer force main will convey wastewater to the proposed leach field area, and then loop back through the woods. We are proposing to cut the trees on a high knoll at the end of the road and run the walking trail through this area, and install two picnic tables for sitting/congregating. The project is a Condominium, so all land outside of the Limited Common Elements and Units will be Common Land. The limits of the Common Land will be delineated on the Condominium Plat that will be submitted with the Final Plan.

MDEP Stormwater Permit Review Comments

The following is a list of the review comments contained in the Delegated Review Stormwater Application Checklist prepared by LJB Engineering dated June 15, 2026 followed by our response.

Comment #1 – Provide a construction schedule/sequence within the Erosion and Sediment Control Notes within the Plan Set.

Response #1 – The Construction Sequencing notes associated with the Stormwater BMPs are shown on Plan Sheet 10 (Stormwater Ponds Plan) as part of the Section Detail.

Comment #2 – A Class-A High Intensity Soil Survey of the site was completed by Mark Hampton Associates, Inc. and included in the application. Test pit logs were provided, however we could not determine the locations of these test pits to see if they aligned with the proposed UDSFs. Provide soil test pit symbols on the plans. All UDSFs propose to use a 30 mil HDPE liner, and no infiltration is proposed. Provide a test pit summary table within the detail sheets of the plan set for all test pits associated with a stormwater BMP.

Response #2 – We have added the Test Pit symbols to the plans, with notes on the Pond Plan indicating the test pit number for each test pit that is located near the UDSFs. Test Pits SS-6 and SS-8 are in the vicinity of FB-1&2, and Test Pit SS-20 is located in the vicinity of FB-3. All three test pits were excavated to a depth of at least 36" and all three encountered groundwater at a depth of 16" below existing grade. Based on the encountered depth to groundwater we are proposing a liner in all of the filter basins. If ledge is encountered during the construction of the filter basins, we will remove the ledge to a depth that will allow at least 4 inches of sand to be installed between the ledge and the pond liner.

Comment #3 – For FB-2 and FB-3 provide 20 feet of horizontal separation between the principal outlet pipe of the UDSFs and the emergency spillways in accordance with Chapter 500, Appendix E, 3.B – Emergency Spillways.

Response #3 – The emergency spillway was moved to provide the required separation distance.

Comment #4 – Provide a note on the Subdivision Plan requiring roof drip edges along rooflines as stated in the Stormwater Treatment Table.

Response #4 – The requested note was added as Note 17 to the Subdivision Plan.

Comment #5 – The Stormwater Treatment Table references a wetpond in the table's footnotes. Revise to only refer to the proposed BMPs.

Response #5 – A revised Stormwater Treatment Table is attached which removes the reference to a Wet Pond.

Comment #6 – Provide a detail for the 24-inch wide diversion berm.

Response #6 – A section detail has been added to sheet D-3 for the diversion berm and associated riprap swale.

Comment #7 – It appears that an underdrain outlet orifice is modeled in HydroCAD for FB 1 & 2 and FB 3. Provide details of the underdrain outlet orifice on the Stormwater Ponds Plan (Sheet P-1).

Response #7 – There is a note and leader on the Outlet Control Structure Detail which reads “INSTALL SOLID CAP AND CORE A HOLE AT PIPE INVERT, CORE HOLE DIAM=D” with a corresponding hole diameter in the Structure Data table for each of the Outlet Control Structures 1 & 2.

Comment #8 – The emergency spillway of UDSF’s FB-1&2 is activated during the 25-year, 24-hour storm event. The 2-, 10- and 25-year, 24-hour storm events shall be directed through the principal outlet without activating the emergency spillway per Appendix E.3.(a) – Principal Spillways.

Response #8 – The elevation of the emergency spillway crest was raised from 235.0 to 235.10 so that the 25-year storm is directed through the principal outlet without activating the emergency spillway. We have enclosed an updated HydroCAD node printout for the Filter Basin 1&2 for review.

Upon your review of the enclosed documents, please let us know if you have any questions or require any additional information.

Sincerely,

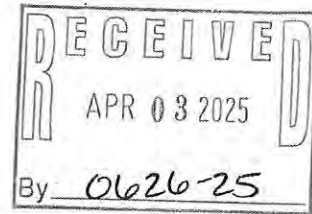
DM ROMA CONSULTING ENGINEERS

Dustin Roma

Dustin M. Roma, P.E.
President

DM ROMA
CONSULTING ENGINEERS

April 2, 2025



Mr. Kirk F. Mohny, Director
Maine Historic Preservation Commission
55 Capitol Street
65 State House Station
Augusta, ME 04333-0065

**Re: Review of Project Area
Residential Subdivision, Webb Road, Windham
Robie Holdings, LLC, Applicant**

Dear Mr. Mohny:

On behalf of our client Robie Holdings, LLC, DM Roma Consulting Engineers is submitting a request to have a proposed residential development off Webb Road in Windham be reviewed by the Maine Historic Preservation Commission for potential impacts to resources of historical significance.

The 28± acre property is identified as being Lot 33 on the Town of Windham Assessors Map 6 and is located in the Farm (F) zoning district. The applicant intends to develop a residential subdivision and will also include a roadway, private and public utility connections and stormwater infrastructure. The property is generally bounded by residential properties, utility corridor (CMP), and undeveloped woodland.

Based on available property information, there appears to be 4 houses in the vicinity of the project site that are over 50 years old. Photographs of each of the properties with structures older than 50 years and a map indicating locations of these structures have been included for review.

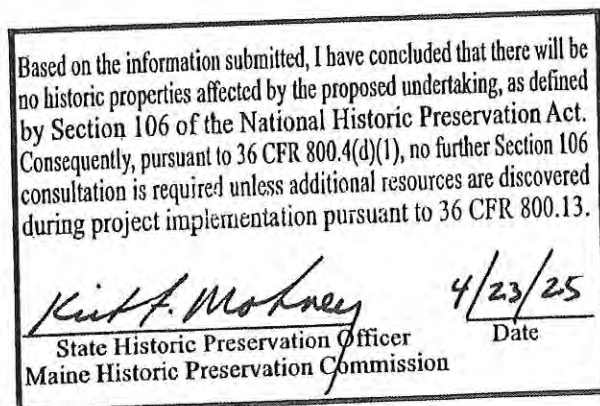
Enclosed is a vicinity map depicting the subject parcel and photographs and a location map for each abutting property over 50 years old. Upon your review of the material, please provide a letter indicating the findings of your initial screening and do not hesitate to contact us with any questions.

Sincerely,

DM Roma Consulting Engineers

J.P. Connolly
Senior Project Engineer

Cc: Robie Holdings, LLC, Applicant
Town of Windham
Maine Department of Environmental Protection
US Army Corps of Engineers



Traffic Assessment

Date: August 4, 2026

To: **Dustin M. Roma, P.E.**
DM Roma Consulting Engineers

From: Jacob W. Sirois, P.E. John Q. Adams, P.E., PTOE
Project Engineer Senior Associate
Barton & Loguidice, LLC Barton & Loguidice, LLC

Re: **Legacy Village**
Webb Road, Windham, Maine

1 Introduction

The applicant is proposing the development of 30 age-restricted (55+) single-family homes on Webb Road in the town of Windham. Refer to Image 1 for the approximate location of the development. Access to the site will be provided by a proposed driveway entrance that intersects with the southwest side of Webb Road, approximately 325 feet southeast of the Read Road intersection,

Image 1 – Site Location



The purpose of this traffic assessment is to evaluate and measure the level of impact on traffic operations and safety resulting with the development of the proposed project. Site generated trip projections are provided for “key” peak hour time periods throughout a typical week; road safety conditions were determined based upon a review of MaineDOT’s latest crash data, and intersection sight distance was field reviewed and measured to ensure safe and acceptable sight distance is provided at the proposed driveway entrance.

2 Trip Generation

Daily and peak hour site trip generation estimates have been prepared for the 30 proposed age-restricted single-family homes based on the trip generation tables presented in the 12th Edition of the Institute of Transportation Engineers (ITE) *Trip Generation Manual*. The ITE Manual provides numerous land use codes (LUCs) and the volume of site-generated trips produced by each category.

Trip generation estimates for the subdivision have been prepared using LUC #251 – Senior Adult Housing-Single Family, described by ITE as *“independent living developments that are called by various names including retirement communities, age-restricted housing, and active adult communities. The development has a specific age restriction for its residents, typically a minimum of 55 years of age for at least one resident of the household.”*

In the Trip Generation Manual, for LUC #251, ITE provides the “Average” trip generation rate and the “Fitted Curve” trip generation rates. MaineDOT guidelines state that when $R^2 \geq 0.80$, the “Fitted Curve” trip generation rate shall be used. For the PM peak hour of the generator, and the Saturday peak hour, the y-intercept in the fitted curve equation (+44.56 and +42.98) artificially inflates the peak hour trip generation. Accordingly, the average rates were used for these hours. The trip generation calculations are provided below:

Table 1.1 ITE Trip Generation Calculations							
Land Use	Multifamily Housing (Low-Rise) Not Close to Rail Transit - LUC 220						
Time Period	Dwelling Units (X)	R ²	Fitted Curve Equation/Avg. Rate	Trips Generated (T)	Distribution Entering / Exiting	Enter	Exit
Weekday	30	0.88	$\ln(T) = 0.80 \ln(X) + 2.71$	228	50% / 50%	114	114
AM Weekday Peak Hour (Street)	30	0.85	$\ln(T) = 0.71 \ln(X) + 0.40$	17	34% / 66%	6	11
PM Weekday Peak Hour (Street)	30	0.86	$\ln(T) = 0.79 \ln(X) + 0.15$	17	61% / 39%	10	7
AM Weekday Peak Hour (Generator)*	30	0.82	0.35	11	43% / 57%	5	6
PM Weekday Peak Hour (Generator)	30	0.81	$\ln(T) = 0.78 \ln(X) + 0.39$	21	55% / 45%	12	9
Saturday Peak Hour*	30	0.98	0.22	7	53% / 47%	4	3
Sunday Peak Hour	30	0.99	$\ln(T) = 0.80 \ln(X) - 0.05$	16	58% / 42%	9	7

*The average rate has been used instead of the fitted curve equation. Due to the relatively small size of the development, the y-intercepts (+44.56) and (+42.98) overestimate the peak hour trip generation for these hours.

Table 1 shows that the proposed development is expected to generate 17 trips during the AM and PM peak hours of the street (a.k.a. the commuter peak hour). During the AM and PM peak hours of the generator, the site is expected to produce 11 trips and 21 trips, respectively. On the weekend, the trip generation calculations show that the site will produce 7 trips during the Saturday peak hour and 16 trips during the Sunday peak hour.

3 Intersection Sight Distance

Intersection sight distances were recorded at the site’s proposed intersection with Webb Road in accordance with the criteria established within the MaineDOT’s *Highway Driveway and Entrance Rules* publication, which requires the following minimum sight distance for non-mobility roadways based on the posted speed limit:

MaineDOT Sight Distance Standards	
Posted Speed Limit	Minimum Sight Distance
25 mph	200 ft.
30 mph	250 ft.
35 mph	305 ft.
40 mph	360 ft.
45 mph	425 ft.
50 mph	495 ft.

The section of Webb Road fronting the development site is posted at 40 mph, requiring a minimum sight distance of 360 feet. MaineDOT's Rules and Regulations require sight distance to be measured in accordance with the following procedures: *"Sight distance is measured to and from the point on the centerline of the proposed access that is located 10 feet from the edge of traveled way. The height of the hypothetical person's view is considered to be 3½ feet above the pavement and the height of the object being viewed is considered to be 4¼ feet above the pavement."*

Our field measurements, looking left and right along Webb Road from the site approach, indicate that the existing sight distances exceed the requirements for the 40 mph speed limit. Looking left, we recorded a measurement in excess of 400 feet. Looking right, we recorded a measurement in excess of 600 feet. Refer to Image 2 and Image 3, attached below:

Image 2 - Sight Distance – Looking Left



Image 3 - Sight Distance – Looking Right



4 Existing Road Safety Conditions

Crash data for the latest three-year time period (2023-2025) was provided by MaineDOT's Crash Records Section for sections of Webb Road, Gray Road, River Road, Chute Road, and Read Road, within the vicinity of the site. A summary of crash data is provided below in Table 2. Intersections and sections with no recorded crashes were omitted from the table.

#	Location	Total Crashes	Critical Rate Factor
1	Main St @ Newhall Rd	3	0.93
2	Main St @ River Rd	14	0.79
3	River Rd @ Chute Rd/Depot St	16	4.74
4	River Rd @ Victoria Ln	2	0.68
5	Chute Rd @ Montgomery Rd/Webb Rd	2	1.57
6	Main St btw. River Rd and Gate Wy	1	0.17
7	Main St btw. Gate Wy and Barnes Rd	2	0.37
8	Main St btw. Barnes Rd and Node 13830 (non-intersection on Main St)	3	0.50
9	Main St btw. Node 13830 (non-intersection on Main St) and Newhall Rd	1	0.19
10	Main St btw. Newhall Rd and Neighborly Wy	3	1.31
11	Gray Rd btw. Neighborly Wy and Read Rd	4	0.38
12	Gray Rd btw. Read Rd and Fall Ridge Rd	6	0.77
13	Gray Rd btw. Fall Ridge Rd and Webb Rd	1	0.22
14	River Rd btw. Median south of Main St and Victoria Ln	7	0.86
15	River Rd btw. Victoria Ln and Chute Rd/Depot St	3	0.45
16	Chute Rd btw. River Rd and Montgomery Rd/Webb Rd	4	0.31
17	Webb Rd btw. Chute Rd and Read Rd	4	0.72

MaineDOT considers any roadway intersection or segment a high crash location (HCL) if both of the following criteria are met:

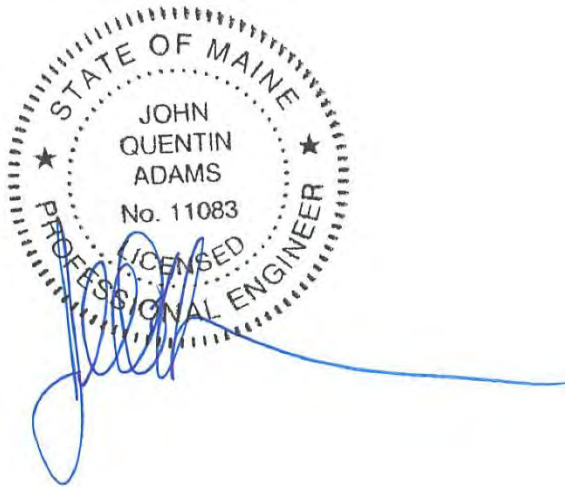
- **8 or more crashes in the latest three-year period, and**
- **A Critical Rate Factor (CRF) greater than or equal to 1.00**

As the data presented in the table shows, Location #3, River Road at Chute Road and Depot Street, meets MaineDOT's dual HCL criteria with 16 total crashes and a CRF of 4.74. This HCL is located more than 2 miles from the site.

5 Summary

The proposed age-restricted residential development is expected to generate 17 trips during the AM and PM peak hours of the street (a.k.a. the commuter peak hour). During the AM and PM peak hours of the generator, the site is expected to produce 11 trips and 21 trips, respectively. On the weekend, the trip generation calculations show that the site will produce 7 trips during the Saturday peak hour and 16 trips during the Sunday peak hour. Overall, the project will remain well below the 100-trip threshold required to trigger a MaineDOT Traffic Movement Permit.

- Vehicle sight distance measurements were field recorded from the proposed site entrance, looking left and right directionally onto Webb Road. Our field measurements showed that the existing sightlines exceed MaineDOT's minimum requirement for a 40 mph roadway (360 feet)
- Crash data for the latest 3-year time period (2023 to 2025) was provided by MaineDOT's Crash Records Section for Webb Road, Gray Road, River Road, and Chute Road around the site. Our review of the crash data showed that there are no high crash locations on Webb Road or within the general vicinity of the site. There is a high crash location at the intersection of River Road, Chute Road, and Depot Street, over 2 miles away from the site.



John Q. Adams, P.E., PTOE
Date: 8/4/2026

APPENDIX

- **MAINEDOT CRASH DATA**



Crash Summary Report

Report Selections and Input Parameters

REPORT SELECTIONS

☒ Crash Summary I ☐ Section Detail ☒ Crash Summary II ☐ 1320 Public ☐ 1320 Private ☐ 1320 Summary

REPORT DESCRIPTION

Windham

Webb Rd-Chute Rd-Gray Rd-Main St-Read Rd-River Rd area

REPORT PARAMETERS

Year 2023, Start Month 1 through Year 2025 End Month: 12

Route: 0202X	Start Node: 15724 End Node: 15728	Start Offset: 0 End Offset: 0	☐ Exclude First Node ☐ Exclude Last Node
Route: 3209658	Start Node: 66694 End Node: 15724	Start Offset: 0 End Offset: 0	☒ Exclude First Node ☒ Exclude Last Node
Route: 0500782	Start Node: 15724 End Node: 15960	Start Offset: 0 End Offset: 0	☒ Exclude First Node ☐ Exclude Last Node
Route: 0500711	Start Node: 11026 End Node: 15960	Start Offset: 0 End Offset: 0	☐ Exclude First Node ☒ Exclude Last Node
Route: 0500708	Start Node: 11026 End Node: 15728	Start Offset: 0 End Offset: 0	☒ Exclude First Node ☒ Exclude Last Node
Route: 0501175	Start Node: 11033 End Node: 15727	Start Offset: 0 End Offset: 0	☒ Exclude First Node ☒ Exclude Last Node

Maine Department Of Transportation - Office of Safety, Crash Records Section

Crash Summary I

Nodes															
Node	Route - MP	Node Description	U/R	Total Crashes	K	Injury A	Crashes B	C	PD	Percent Injury	Annual M Ent-Veh	Crash Rate	Critical Rate	CRF	
15728	0202X - 46.47	Int of GRAY RD WEBB RD	2	0	0	0	0	0	0	0.0	2.463	0.00	0.45	0.00	
												Statewide Crash Rate:	0.15		
13830	0202X - 45.52	Non-Int MAIN ST	2	0	0	0	0	0	0	0.0	2.112	0.00	0.47	0.00	
												Statewide Crash Rate:	0.15		
15726	0202X - 45.68	Int of MAIN ST NEWHALL RD	2	3	0	0	1	0	2	33.3	2.300	0.43	0.46	0.00	
												Statewide Crash Rate:	0.15		
15727	0202X - 46.10	Int of GRAY RD READ RD	2	0	0	0	0	0	0	0.0	2.358	0.00	0.45	0.00	
												Statewide Crash Rate:	0.15		
P15724	0202X - 44.92	Int of MAIN ST RIVER RD	9	14	0	0	0	2	12	14.3	4.844	0.96	1.22	0.79	
												Statewide Crash Rate:	0.69		
19552	0202X - 45.73	Int of GRAY RD MAIN ST NEIGHBORLY WY	2	0	0	0	0	0	0	0.0	2.326	0.00	0.46	0.00	
												Statewide Crash Rate:	0.15		
59501	0202X - 45.14	Int of GATE WY MAIN ST	2	0	0	0	0	0	0	0.0	1.972	0.00	0.48	0.00	
												Statewide Crash Rate:	0.15		
59515	0202X - 46.35	Int of FALL RIDGE RD GRAY RD	2	0	0	0	0	0	0	0.0	2.395	0.00	0.45	0.00	
												Statewide Crash Rate:	0.15		
15725	0202X - 45.32	Int of BARNES RD MAIN ST	2	0	0	0	0	0	0	0.0	2.098	0.00	0.47	0.00	
												Statewide Crash Rate:	0.15		
15960	0500782 - 6.60	Int of CHUTE RD DEPOT ST RIVER RD	2	16	0	0	2	3	11	31.3	2.904	1.84	0.39	4.74	
												Statewide Crash Rate:	0.13		
62683	0500782 - 6.35	Int of RIVER RD VICTORIA LN	2	2	0	0	0	0	2	0.0	2.369	0.28	0.41	0.00	
												Statewide Crash Rate:	0.13		
A66694	0500782 - 6.02	Int of RD INV 3142105 RIVER RD	2	0	0	0	0	0	0	0.0	0.000	0.00	0.00	0.00	
												Statewide Crash Rate:	0.15		
11026	0500711 - 1.33	Int of CHUTE RD MONTGOMERY RD WEBB RD	2	2	0	0	0	0	2	0.0	0.762	0.88	0.56	1.57	
												Statewide Crash Rate:	0.14		
11033	0500708 - 2.14	Int of READ RD WEBB RD	2	0	0	0	0	0	0	0.0	0.181	0.00	0.53	0.00	
												Statewide Crash Rate:	0.14		
10186	0501175 - 0.15	Non Int READ RD	2	0	0	0	0	0	0	0.0	0.017	0.00	-5.33	0.00	
												Statewide Crash Rate:	0.14		
Study Years: 3.00		NODE TOTALS:		37	0	0	3	5	29	21.6	29.101	0.42	0.36	1.16	

Crash Summary I

Sections																		
Start Node	End Node	Element	Offset Begin - End	Route - MP	Section U/R Length	Total Crashes	K	Injury A	Crashes B	Percent C	Annual PD	Percent Injury	Annual HMVM	Crash Rate	Critical Rate	CRF		
15724	59501	3142036	0 - 0.22	0202X - 44.92 US 202	0.22	2	1	0	0	0	0	1	0.0	0.00422	79.07	477.51	0.00	
Int of MAIN ST RIVER RD															Statewide Crash Rate: 196.20			
59501	15725	3115029	0 - 0.18	0202X - 45.14 US 202	0.18	2	2	0	0	0	1	1	50.0	0.00360	185.17	497.09	0.00	
Int of GATE WY MAIN ST															Statewide Crash Rate: 196.20			
13830	15725	3106320	0 - 0.20	0202X - 45.32 US 202	0.20	2	3	0	0	0	1	2	33.3	0.00417	239.95	478.90	0.00	
Non-Int MAIN ST															Statewide Crash Rate: 196.20			
13830	15726	3106321	0 - 0.16	0202X - 45.52 US 202	0.16	2	1	0	0	0	0	1	0.0	0.00342	97.35	503.54	0.00	
Non-Int MAIN ST															Statewide Crash Rate: 196.20			
15726	19552	3122251	0 - 0.05	0202X - 45.68 US 202	0.05	2	3	0	0	1	2	0	100.0	0.00115	871.14	665.87	1.31	
Int of MAIN ST NEWHALL RD															Statewide Crash Rate: 196.20			
15727	19552	3105844	0 - 0.37	0202X - 45.73 US 202	0.37	2	4	0	0	1	0	3	25.0	0.00869	153.50	400.53	0.00	
Int of GRAY RD READ RD															Statewide Crash Rate: 196.20			
15727	59515	3138986	0 - 0.25	0202X - 46.10 US 202	0.25	2	6	0	0	0	0	6	0.0	0.00588	340.34	439.59	0.00	
Int of GRAY RD READ RD															Statewide Crash Rate: 196.20			
59515	15728	3115030	0 - 0.12	0202X - 46.35 US 202	0.12	2	1	0	0	0	0	1	0.0	0.00286	116.56	527.48	0.00	
Int of FALL RIDGE RD GRAY RD															Statewide Crash Rate: 196.20			
66694	15724	3142048	0 - 0.03	3209658 - 0 RD INV 3209658	0.03	2	0	0	0	0	0	0	0.0	0.00029	0.00	695.55	0.00	
Int of RD INV 3142105 RIVER RD															Statewide Crash Rate: 161.30			
15724	66694	3142046	0 - 0.02	0500782 - 6 RD INV 05 00782	0.02	2	0	0	0	0	0	0	0.0	0.00025	0.00	689.10	0.00	
Int of MAIN ST RIVER RD															Statewide Crash Rate: 161.30			
62683	66694	3939595	0 - 0.33	0500782 - 6.02 RD INV 05 00782	0.33	2	7	0	0	1	1	5	28.6	0.00768	303.63	355.08	0.86	
Int of RIVER RD VICTORIA LN															Statewide Crash Rate: 161.30			
15960	62683	3139268	0 - 0.25	0500782 - 6.35 RD INV 05 00782	0.25	2	3	0	0	0	0	3	0.0	0.00590	169.38	378.90	0.00	
Int of CHUTE RD DEPOT ST RIVER RD															Statewide Crash Rate: 161.30			
11026	15960	5087745	0 - 1.11	0500711 - 1.33 RD INV 05 00711	1.11	2	4	0	0	0	2	2	50.0	0.00652	204.41	665.16	0.00	
Int of CHUTE RD MONTGOMERY RD WEBB RD															Statewide Crash Rate: 347.46			
11026	11033	5087742	0 - 1.21	0500708 - 0.93 RD INV 05 00708	1.21	2	4	0	0	0	0	4	0.0	0.00212	628.95	870.95	0.00	
Int of CHUTE RD MONTGOMERY RD WEBB RD															Statewide Crash Rate: 347.46			
11033	15728	5087743	0 - 0.15	0500708 - 2.14 RD INV 05 00708	0.15	2	0	0	0	0	0	0	0.0	0.00025	0.00	1430.74	0.00	
Int of READ RD WEBB RD															Statewide Crash Rate: 347.46			
10186	11033	5096588	0 - 0.15	0501175 - 0 RD INV 05 01175	0.15	2	0	0	0	0	0	0	0.0	0.00003	0.00	-664.35	0.00	
Non Int READ RD															Statewide Crash Rate: 347.46			
10186	15727	5096587	0 - 0.16	0501175 - 0.15 RD INV 05 01175	0.16	2	0	0	0	0	0	0	0.0	0.00003	0.00	-433.09	0.00	
Non Int READ RD															Statewide Crash Rate: 347.46			
Study Years: 3.00				Section Totals:		4.96		39	0	0	3	7	29	25.6	0.05705	227.86	298.87	0.76
				Grand Totals:		4.96		76	0	0	6	12	58	23.7	0.05705	444.03	412.39	1.08

Crash Summary

Section Details

Start Node	End Node	Element	Offset Begin - End	Route - MP	Total Crashes	K	Injury A	Crashes B	Crashes C	Crashes PD	Crash Report	Crash Date	Crash Mile Point	Injury Degree
15724	59501	3142036	0 - 0.22	0202X - 44.92	1	0	0	0	0	1	2024-26474	09/25/2024	45.01	PD
59501	15725	3115029	0 - 0.18	0202X - 45.14	2	0	0	0	1	1	2025-24455	08/26/2025	45.24	C
											2025-26602	09/16/2025	45.30	PD
13830	15725	3106320	0 - 0.20	0202X - 45.32	3	0	0	0	1	2	2025-2114	01/21/2025	45.33	PD
											2024-5864	02/26/2024	45.42	PD
											2023-7063	03/02/2023	45.47	C
13830	15726	3106321	0 - 0.16	0202X - 45.52	1	0	0	0	0	1	2025-38089	12/16/2025	45.67	PD
15726	19552	3122251	0 - 0.05	0202X - 45.68	3	0	0	1	2	0	2023-28965	10/06/2023	45.72	B
											2025-32585	11/07/2025	45.72	C
											2025-27544	09/26/2025	45.72	C
15727	19552	3105844	0 - 0.37	0202X - 45.73	4	0	0	1	0	3	2025-6396	02/25/2025	45.79	B
											2023-35746	11/30/2023	45.84	PD
											2025-33096	11/13/2025	45.94	PD
											2024-5923	02/26/2024	46.07	PD
15727	59515	3138986	0 - 0.25	0202X - 46.10	6	0	0	0	0	6	2025-37735	12/15/2025	46.11	PD
											2024-11552	03/21/2024	46.16	PD
											2023-23	01/02/2023	46.23	PD
											2024-31262	11/06/2024	46.25	PD
											2023-30303	10/17/2023	46.26	PD
											2024-34007	11/30/2024	46.29	PD
59515	15728	3115030	0 - 0.12	0202X - 46.35	1	0	0	0	0	1	2023-29725	10/14/2023	46.40	PD
66694	15724	3142048	0 - 0.03	3209658 - 0	0	0	0	0	0	0				
15724	66694	3142046	0 - 0.02	0500782 - 6	0	0	0	0	0	0				
62683	66694	3939595	0 - 0.33	0500782 - 6.02	7	0	0	1	1	5	2025-37176	12/11/2025	6.04	B
											2023-30283	10/18/2023	6.07	PD
											2025-13321	05/13/2025	6.14	PD
											2025-9218	03/24/2025	6.16	PD
											2023-16747	06/09/2023	6.17	C
											2024-31543	11/10/2024	6.24	PD
											2025-14521	05/27/2025	6.24	PD
15960	62683	3139268	0 - 0.25	0500782 - 6.35	3	0	0	0	0	3	2023-37025	12/09/2023	6.43	PD
											2025-2012	01/19/2025	6.49	PD
											2023-34720	11/24/2023	6.51	PD

Crash Summary

Section Details

Start Node	End Node	Element	Offset Begin - End	Route - MP	Total Crashes	K	Injury Crashes				Crash Report	Crash Date	Crash Mile Point	Injury Degree
A	B	C	PD											
11026	15960	5087745	0 - 1.11	0500711 - 1.33	4	0	0	0	2	2	2025-27235	09/24/2025	1.83	PD
											2023-10696	04/08/2023	1.86	C
											2024-11533	03/04/2024	1.97	C
											2024-28262	10/13/2024	2.22	PD
11026	11033	5087742	0 - 1.21	0500708 - 0.93	4	0	0	0	0	4	2024-11536	03/05/2024	1.15	PD
											2023-28860	10/05/2023	1.69	PD
											2023-10205	04/03/2023	1.77	PD
											2024-24589	09/03/2024	1.95	PD
11033	15728	5087743	0 - 0.15	0500708 - 2.14	0	0	0	0	0	0				
10186	11033	5096588	0 - 0.15	0501175 - 0	0	0	0	0	0	0				
10186	15727	5096587	0 - 0.16	0501175 - 0.15	0	0	0	0	0	0				
Totals:					39	0	0	3	7	29				

Crash Summary II - Characteristics

Crashes by Day and Hour

	AM											Hour of Day											PM												
Day Of Week	12	1	2	3	4	5	6	7	8	9	10	11	12	1	2	3	4	5	6	7	8	9	10	11	Un	Tot									
SUNDAY	0	0	0	0	0	0	0	1	1	0	0	1	0	1	0	1	0	1	0	1	0	0	0	0	0	7									
MONDAY	0	0	0	0	0	1	0	0	0	0	0	0	0	0	1	1	3	0	0	2	0	0	0	1	0	9									
TUESDAY	0	1	0	0	0	0	0	2	0	0	0	1	0	3	2	1	0	1	1	1	2	0	0	0	0	15									
WEDNESDAY	0	1	0	0	0	0	0	2	0	1	0	1	1	0	1	1	0	3	1	0	0	0	1	0	0	13									
THURSDAY	0	0	0	0	0	2	1	0	0	1	0	0	1	0	0	1	0	1	1	1	0	0	0	1	0	10									
FRIDAY	0	0	0	0	0	0	0	1	0	0	2	0	0	1	1	0	1	2	0	1	0	0	0	0	0	9									
SATURDAY	1	0	0	0	0	1	1	0	0	0	0	0	2	1	1	1	0	1	2	1	0	0	1	0	0	13									
Totals	1	2	0	0	0	4	2	6	1	2	2	3	4	6	6	6	4	9	5	7	2	0	2	2	0	76									

Vehicle Counts by Type

Unit Type	Total	Unit Type	Total
1-Passenger Car	42	23-Bicyclist	0
2-(Sport) Utility Vehicle	51	24-Witness	9
3-Passenger Van	1	25-Other	0
4-Cargo Van (10K lbs or Less)	1	26-Construction	0
5-Pickup	27	27-Farm Vehicle	0
6-Motor Home	0	28-Horse and Buggy	0
7-School Bus	0	Total	133
8-Transit Bus	0		
9-Motor Coach	0		
10-Other Bus	0		
11-Motorcycle	0		
12-Moped	0		
13-Low Speed Vehicle	0		
14-Autocycle	0		
15-Experimental	0		
16-Other Light Trucks (10,000 lbs or Less)	1		
17-Medium/Heavy Trucks (More than 10,000 lbs)	1		
18-ATV - (4 wheel)	0		
20-ATV - (2 wheel)	0		
21-Snowmobile	0		
22-Pedestrian	0		

Maine Department Of Transportation - Office of Safety, Crash Records Section

Crash Summary II - Characteristics

Crashes by Driver Action at Time of Crash

Driver Action at Time of Crash	Dr 1	Dr 2	Dr 3	Dr 4	Dr 5	Other	Total
No Contributing Action	31	32	2	1	0	0	66
Ran Off Roadway	4	0	0	0	0	0	4
Failed to Yield Right-of-Way	13	6	0	0	0	0	19
Ran Red Light	3	0	0	0	0	0	3
Ran Stop Sign	0	0	0	0	0	0	0
Disregarded Other Traffic Sign	0	0	0	0	0	0	0
Disregarded Other Road Markings	0	0	0	0	0	0	0
Exceeded Posted Speed Limit	0	0	0	0	0	0	0
Drove Too Fast For Conditions	0	0	0	0	0	0	0
Improper Turn	2	0	0	0	0	0	2
Improper Backing	0	0	0	0	0	0	0
Improper Passing	0	0	0	0	0	0	0
Wrong Way	0	0	0	0	0	0	0
Followed Too Closely	13	1	0	0	0	0	14
Failed to Keep in Proper Lane	0	1	0	0	0	0	1
Operated Motor Vehicle in Erratic, Reckless, Careless, Negligent or Aggressive Manner	0	0	0	0	0	0	0
Swerved or Avoided Due to Wind, Slippery Surface, Motor Vehicle, Object, Non-Motorist in Roadway	2	0	0	0	0	0	2
Over-Correcting/Over-Steering	0	0	0	0	0	0	0
Other Contributing Action	4	1	0	0	0	0	5
Unknown	3	2	0	0	0	0	5
Total	75	43	2	1	0	0	121

Crashes by Apparent Physical Condition And Driver

Apparent Physical Condition	Dr 1	Dr 2	Dr 3	Dr 4	Dr 5	Other	Total
Apparently Normal	71	43	2	1	0	0	117
Physically Impaired	1	0	0	0	0	0	1
Emotional(Depressed, Angry, Disturbed, etc.)	0	0	0	0	0	0	0
Ill (Sick)	0	0	0	0	0	0	0
Asleep or Fatigued	1	0	0	0	0	0	1
Under the Influence of Medications/Drugs/Alcohol	1	0	0	0	0	0	1
Other	1	0	0	0	0	0	1
Total	75	43	2	1	0	0	121

Driver Age by Unit Type

Age	Driver	Bicycle	SnowMobile	Pedestrian	ATV	Total
09-Under	0	0	0	0	0	0
10-14	0	0	0	0	0	0
15-19	16	0	0	0	0	16
20-24	17	0	0	0	0	17
25-29	12	0	0	0	0	12
30-39	22	0	0	0	0	22
40-49	16	0	0	0	0	16
50-59	18	0	0	0	0	18
60-69	13	0	0	0	0	13
70-79	7	0	0	0	0	7
80-Over	2	0	0	0	0	2
Unknown	1	0	0	0	0	1
Total	124	0	0	0	0	124

Maine Department Of Transportation - Office of Safety, Crash Records Section

Crash Summary II - Characteristics

Most Harmful Event			
Most Harmful Event	Total	Most Harmful Event	Total
1-Overturn / Rollover	0	38-Other Fixed Object (wall, building, tunnel, etc.)	0
2-Fire / Explosion	0	39-Unknown	0
3-Immersion	0	40-Gate or Cable	0
4-Jackknife	0	41-Pressure Ridge	0
5-Cargo / Equipment Loss Or Shift	0	Total	123
6-Fell / Jumped from Motor Vehicle	0		
7-Thrown or Falling Object	0		
8-Other Non-Collision	0		
9-Pedestrian	0		
10-Pedalcycle	0		
11-Railway Vehicle - Train, Engine	0		
12-Animal	19		
13-Motor Vehicle in Transport	96		
14-Parked Motor Vehicle	1		
15-Struck by Falling, Shifting Cargo or Anything Set in Motion by Motor Vehicle	0		
16-Work Zone / Maintenance Equipment	0		
17-Other Non-Fixed Object	0		
18-Impact Attenuator / Crash Cushion	0		
19-Bridge Overhead Structure	0		
20-Bridge Pier or Support	0		
21-Bridge Rail	0		
22-Cable Barrier	0		
23-Culvert	0		
24-Curb	0		
25-Ditch	3		
26-Embankment	0		
27-Guardrail Face	0		
28-Guardrail End	0		
29-Concrete Traffic Barrier	0		
30-Other Traffic Barrier	0		
31-Tree (Standing)	2		
32-Utility Pole / Light Support	2		
33-Traffic Sign Support	0		
34-Traffic Signal Support	0		
35-Fence	0		
36-Mailbox	0		
37-Other Post, Pole, or Support	0		

Traffic Control Devices		
Traffic Control Device	Total	
1-Traffic Signals (Stop & Go)	16	
2-Traffic Signals (Flashing)	4	
3-Advisory/Warning Sign	0	
4-Stop Signs - All Approaches	1	
5-Stop Signs - Other	10	
6-Yield Sign	0	
7-Curve Warning Sign	0	
8-Officer, Flagman, School Patrol	1	
9-School Bus Stop Arm	0	
10-School Zone Sign	0	
11-R.R. Crossing Device	0	
12-No Passing Zone	0	
13-None	43	
14-Other	1	
Total	76	

Injury Data		
Severity Code	Injury Crashes	Number Of Injuries
K	0	0
A	0	0
B	6	6
C	12	14
PD	58	0
Total	76	20

Road Character	
Road Grade	Total
1-Level	64
2-On Grade	9
3-Top of Hill	2
4-Bottom of Hill	1
5-Other	0
Total	76

Light	
Light Condition	Total
1-Daylight	44
2-Dawn	1
3-Dusk	3
4-Dark - Lighted	9
5-Dark - Not Lighted	19
6-Dark - Unknown Lighting	0
7-Unknown	0
Total	76

Crash Summary II - Characteristics**Crashes by Year and Month**

Month	2023	2024	2025	Total
JANUARY	2	0	3	5
FEBRUARY	3	5	5	13
MARCH	1	4	2	7
APRIL	3	0	1	4
MAY	0	0	3	3
JUNE	2	1	1	4
JULY	1	0	1	2
AUGUST	0	4	1	5
SEPTEMBER	0	2	3	5
OCTOBER	5	3	1	9
NOVEMBER	2	5	3	10
DECEMBER	3	0	6	9
Total	22	24	30	76

Report is limited to the last 10 years of data.

Crash Summary II - Characteristics

Crashes by Crash Type and Type of Location

Crash Type	Straight Road	Curved Road	Three Leg Intersection	Four Leg Intersection	Five or More Leg Intersection	Driveways	Bridges	Interchanges	Other	Parking Lot	Private Way	Cross Over	Railroad Crossing	Traffic Circle-Roundabout	Total
Object in Road	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Rear End - Sideswipe	3	0	1	12	0	6	0	0	0	0	0	0	0	0	22
Head-on - Sideswipe	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Intersection Movement	0	0	2	19	0	1	0	0	0	0	0	0	0	0	22
Pedestrians	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Train	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Went Off Road	7	1	2	0	0	0	0	0	0	0	0	0	0	0	10
All Other Animal	1	0	0	0	0	0	0	0	0	0	0	0	0	0	1
Bicycle	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Other	0	0	0	1	0	0	0	0	0	0	0	0	0	0	1
Jackknife	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Rollover	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Fire	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Submersion	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Thrown or Falling Object	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Bear	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Deer	19	1	0	0	0	0	0	0	0	0	0	0	0	0	20
Moose	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Turkey	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Total	30	2	5	32	0	7	0	0	0	0	0	0	0	0	76

Maine Department Of Transportation - Office of Safety, Crash Records Section

Crash Summary II - Characteristics**Crashes by Weather, Light Condition and Road Surface**

Weather Light	Dry	Ice/Frost	Mud, Dirt, Gravel	Oil	Other	Sand	Slush	Snow	Unknown	Water (Standing, Moving)	Wet	Total
Blowing Sand, Soil, Dirt												
Dark - Lighted	0	0	0	0	0	0	0	0	0	0	0	0
Dark - Not Lighted	0	0	0	0	0	0	0	0	0	0	0	0
Dark - Unknown Lighting	0	0	0	0	0	0	0	0	0	0	0	0
Dawn	0	0	0	0	0	0	0	0	0	0	0	0
Daylight	0	0	0	0	0	0	0	0	0	0	0	0
Dusk	0	0	0	0	0	0	0	0	0	0	0	0
Unknown	0	0	0	0	0	0	0	0	0	0	0	0
Blowing Snow												
Dark - Lighted	0	0	0	0	0	0	0	0	0	0	0	0
Dark - Not Lighted	0	0	0	0	0	0	0	0	0	0	0	0
Dark - Unknown Lighting	0	0	0	0	0	0	0	0	0	0	0	0
Dawn	0	0	0	0	0	0	0	0	0	0	0	0
Daylight	0	0	0	0	0	0	0	0	0	0	0	0
Dusk	0	0	0	0	0	0	0	0	0	0	0	0
Unknown	0	0	0	0	0	0	0	0	0	0	0	0
Clear												
Dark - Lighted	7	0	0	0	0	0	0	0	0	0	0	7
Dark - Not Lighted	14	0	0	0	0	0	0	0	0	0	1	15
Dark - Unknown Lighting	0	0	0	0	0	0	0	0	0	0	0	0
Dawn	0	0	0	0	0	0	0	0	0	0	0	0
Daylight	26	2	0	0	0	0	0	0	0	0	2	30
Dusk	3	0	0	0	0	0	0	0	0	0	0	3
Unknown	0	0	0	0	0	0	0	0	0	0	0	0
Cloudy												
Dark - Lighted	0	0	0	0	0	0	0	0	0	0	0	0
Dark - Not Lighted	1	0	0	0	0	0	0	0	0	0	0	1
Dark - Unknown Lighting	0	0	0	0	0	0	0	0	0	0	0	0
Dawn	0	0	0	0	0	0	0	0	0	0	0	0
Daylight	7	0	0	0	0	0	0	0	0	0	1	8
Dusk	0	0	0	0	0	0	0	0	0	0	0	0
Unknown	0	0	0	0	0	0	0	0	0	0	0	0

Maine Department Of Transportation - Office of Safety, Crash Records Section

Crash Summary II - Characteristics

Crashes by Weather, Light Condition and Road Surface

Weather Light	Dry	Ice/Frost	Mud, Dirt, Gravel	Oil	Other	Sand	Slush	Snow	Unknown	Water (Standing, Moving)	Wet	Total
Fog, Smog, Smoke												
Dark - Lighted	0	0	0	0	0	0	0	0	0	0	0	0
Dark - Not Lighted	2	0	0	0	0	0	0	0	0	0	0	2
Dark - Unknown Lighting	0	0	0	0	0	0	0	0	0	0	0	0
Dawn	0	0	0	0	0	0	0	0	0	0	1	1
Daylight	0	0	0	0	0	0	0	0	0	0	0	0
Dusk	0	0	0	0	0	0	0	0	0	0	0	0
Unknown	0	0	0	0	0	0	0	0	0	0	0	0
Other												
Dark - Lighted	0	0	0	0	0	0	0	0	0	0	0	0
Dark - Not Lighted	0	0	0	0	0	0	0	0	0	0	0	0
Dark - Unknown Lighting	0	0	0	0	0	0	0	0	0	0	0	0
Dawn	0	0	0	0	0	0	0	0	0	0	0	0
Daylight	0	0	0	0	0	0	0	0	0	0	0	0
Dusk	0	0	0	0	0	0	0	0	0	0	0	0
Unknown	0	0	0	0	0	0	0	0	0	0	0	0
Rain												
Dark - Lighted	0	0	0	0	0	0	0	0	0	0	0	0
Dark - Not Lighted	0	0	0	0	0	0	0	0	0	0	1	1
Dark - Unknown Lighting	0	0	0	0	0	0	0	0	0	0	0	0
Dawn	0	0	0	0	0	0	0	0	0	0	0	0
Daylight	0	0	0	0	0	0	0	0	0	0	3	3
Dusk	0	0	0	0	0	0	0	0	0	0	0	0
Unknown	0	0	0	0	0	0	0	0	0	0	0	0
Severe Crosswinds												
Dark - Lighted	0	0	0	0	0	0	0	0	0	0	0	0
Dark - Not Lighted	0	0	0	0	0	0	0	0	0	0	0	0
Dark - Unknown Lighting	0	0	0	0	0	0	0	0	0	0	0	0
Dawn	0	0	0	0	0	0	0	0	0	0	0	0
Daylight	0	0	0	0	0	0	0	0	0	0	0	0
Dusk	0	0	0	0	0	0	0	0	0	0	0	0
Unknown	0	0	0	0	0	0	0	0	0	0	0	0

Crash Summary II - Characteristics**Crashes by Weather, Light Condition and Road Surface**

Weather Light	Dry	Ice/Frost	Mud, Dirt, Gravel	Oil	Other	Sand	Slush	Snow	Unknown	Water (Standing, Moving)	Wet	Total
Sleet, Hail (Freezing Rain or Drizzle)												
Dark - Lighted	0	0	0	0	0	0	0	0	0	0	1	1
Dark - Not Lighted	0	0	0	0	0	0	0	0	0	0	0	0
Dark - Unknown Lighting	0	0	0	0	0	0	0	0	0	0	0	0
Dawn	0	0	0	0	0	0	0	0	0	0	0	0
Daylight	0	0	0	0	0	0	0	0	0	0	0	0
Dusk	0	0	0	0	0	0	0	0	0	0	0	0
Unknown	0	0	0	0	0	0	0	0	0	0	0	0
Snow												
Dark - Lighted	0	0	0	0	0	0	0	1	0	0	0	1
Dark - Not Lighted	0	0	0	0	0	0	0	0	0	0	0	0
Dark - Unknown Lighting	0	0	0	0	0	0	0	0	0	0	0	0
Dawn	0	0	0	0	0	0	0	0	0	0	0	0
Daylight	0	0	0	0	0	0	0	2	0	0	1	3
Dusk	0	0	0	0	0	0	0	0	0	0	0	0
Unknown	0	0	0	0	0	0	0	0	0	0	0	0
TOTAL	60	2	0	0	0	0	0	3	0	0	11	76

H. C. L. CRASH COLLISION DIAGRAM DATA PACKAGE

COUNTY: CUMBERLAND

TOWN: WINDHAM

LOW NODE: 15960 HIGH NODE: 0000

REGION: 1

U/R: URBAN

DESCRIPTION: Int of River Rd, Chute Rd, and Depot St

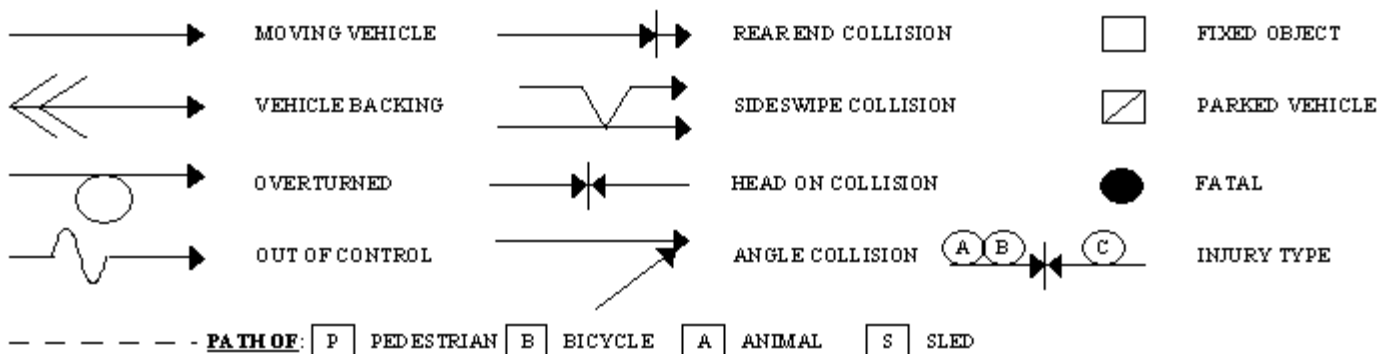
RTE # / RD #: 0500711 DATE DRAWN: 7/22/2026 DRAWN BY: Duncan

STUDY FROM: 1/1/2023

STUDY TO: 12/31/2025

CRASH RATE: 1.84 CRF: 4.75 % INJURY: 31.3 TOTAL CRASHES: 16

LEGEND

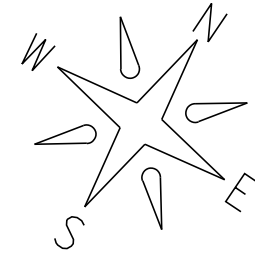


PAVEMENT: D - DRY, I - ICY, W - WET, S - SNOW

WEATHER: C - CLEAR, F - FOG, R - RAIN, SL - SLEET, S - SNOW, CL - CLOUDY

TIME: A - AM, P - PM

River Rd



Stop

Depot St

3708 2-3-25 3:28P W/C Fail to Yield

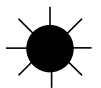
11555 3-24-24 7:49A I/C Fail to Yield

22185 8-7-24 6:04P D/C Follow too Close

3352 2-1-23 3:47P D/C Fail to Yield

5836 2-19-25 11:10A D/C Fail to Yield

Stop



= Flashing Light

River Rd

31700 10-31-25 1:30P D/C Fail to Yield
38035 12-16-25 1:54P D/C Fail to Yield
37951 12-13-23 7:07A D/C Fail to Yield

23406 8-24-24 2:58P D/C Fail to Yield

(B)

38486 12-19-23 6:02P D/C OUI

(C) 21632 8-7-24 5:45P D/C Fail to Yield
(B) 1128 1-12-23 12:23P W/S Fail to Yield
966 1-11-25 3:50P S/S Fail to Yield
5778 2-19-25 5:36P D/C Fail to Yield
5834 2-18-25 2:37P D/C Hit & Run
(C) 10495 4-8-25 2:06P W/R Fail to Yield

Chute Rd

Windham

Node: 15960

Study Period: 2023-2025

of Crashes: 16 / CRF: 4.75

Prepared by Office of Safety & Mobility

(DS 7/22/26)



Crash Summary Report

Report Selections and Input Parameters

REPORT SELECTIONS

☒ Crash Summary I - Single Node ☐ Section Detail ☒ Crash Summary II ☐ 1320 Public ☐ 1320 Private ☐ 1320 Summary

REPORT DESCRIPTION

Windham
Int of River Rd, Chute Rd, and Depot St

REPORT PARAMETERS

Year 2023, Start Month 1 through Year 2025 End Month: 12

Route: 0500711	Start Node: 15960	Start Offset: 0	☐ Exclude First Node
	End Node: 15960	End Offset: 0	☐ Exclude Last Node

Crash Summary I

Nodes

Node	Route - MP	Node Description	U/R	Total Crashes	K	Injury A	Crashes B	C	PD	Percent Annual M Injury	Ent-Veh	Crash Rate	Critical Rate	CRF
15960	0500711 - 2.44	Int of CHUTE RD DEPOT ST RIVER RD	2	16	0	0	2	3	11	31.3	2.904	1.84	0.39	4.74
				Statewide Crash Rate: 0.13										
Study Years: 3.00				NODE TOTALS:										
				16	0	0	2	3	11	31.3	2.904	1.84	0.39	4.75

Crash Summary II - Characteristics

Crashes by Day and Hour

Day Of Week	AM											Hour of Day											PM											Un	Tot
	12	1	2	3	4	5	6	7	8	9	10	11	12	1	2	3	4	5	6	7	8	9	10	11											
SUNDAY	0	0	0	0	0	0	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1								
MONDAY	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0	0	0	0	0	0	0	0	0	0	1								
TUESDAY	0	0	0	0	0	0	0	0	0	0	0	0	0	1	2	0	0	0	1	0	0	0	0	0	0	0	4								
WEDNESDAY	0	0	0	0	0	0	0	1	0	0	0	1	0	0	0	1	0	2	1	0	0	0	0	0	0	0	6								
THURSDAY	0	0	0	0	0	0	0	0	0	0	0	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0	1								
FRIDAY	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0	0	0	0	0	0	0	0	0	0	0	0	1								
SATURDAY	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	1	0	0	0	0	0	0	0	0	0	0	2								
Totals	0	0	0	0	0	0	0	2	0	0	0	1	1	2	3	3	0	2	2	0	0	0	0	0	0	0	16								

Vehicle Counts by Type

Unit Type	Total	Unit Type	Total
1-Passenger Car	9	23-Bicyclist	0
2-(Sport) Utility Vehicle	12	24-Witness	5
3-Passenger Van	1	25-Other	0
4-Cargo Van (10K lbs or Less)	0	26-Construction	0
5-Pickup	11	27-Farm Vehicle	0
6-Motor Home	0	28-Horse and Buggy	0
7-School Bus	0	Total	38
8-Transit Bus	0		
9-Motor Coach	0		
10-Other Bus	0		
11-Motorcycle	0		
12-Moped	0		
13-Low Speed Vehicle	0		
14-Autocycle	0		
15-Experimental	0		
16-Other Light Trucks (10,000 lbs or Less)	0		
17-Medium/Heavy Trucks (More than 10,000 lbs)	0		
18-ATV - (4 wheel)	0		
20-ATV - (2 wheel)	0		
21-Snowmobile	0		
22-Pedestrian	0		

Crash Summary II - Characteristics

Crashes by Driver Action at Time of Crash

Driver Action at Time of Crash	Dr 1	Dr 2	Dr 3	Dr 4	Dr 5	Other	Total
No Contributing Action	2	12	1	0	0	0	15
Ran Off Roadway	0	0	0	0	0	0	0
Failed to Yield Right-of-Way	11	4	0	0	0	0	15
Ran Red Light	0	0	0	0	0	0	0
Ran Stop Sign	0	0	0	0	0	0	0
Disregarded Other Traffic Sign	0	0	0	0	0	0	0
Disregarded Other Road Markings	0	0	0	0	0	0	0
Exceeded Posted Speed Limit	0	0	0	0	0	0	0
Drove Too Fast For Conditions	0	0	0	0	0	0	0
Improper Turn	0	0	0	0	0	0	0
Improper Backing	0	0	0	0	0	0	0
Improper Passing	0	0	0	0	0	0	0
Wrong Way	0	0	0	0	0	0	0
Followed Too Closely	1	0	0	0	0	0	1
Failed to Keep in Proper Lane	0	0	0	0	0	0	0
Operated Motor Vehicle in Erratic, Reckless, Careless, Negligent or Aggressive Manner	0	0	0	0	0	0	0
Swerved or Avoided Due to Wind, Slippery Surface, Motor Vehicle, Object, Non-Motorist in Roadway	0	0	0	0	0	0	0
Over-Correcting/Over-Steering	0	0	0	0	0	0	0
Other Contributing Action	0	0	0	0	0	0	0
Unknown	1	0	0	0	0	0	1
Total	15	16	1	0	0	0	32

Crashes by Apparent Physical Condition And Driver

Apparent Physical Condition	Dr 1	Dr 2	Dr 3	Dr 4	Dr 5	Other	Total
Apparently Normal	14	16	1	0	0	0	31
Physically Impaired	0	0	0	0	0	0	0
Emotional(Depressed, Angry, Disturbed, etc.)	0	0	0	0	0	0	0
Ill (Sick)	0	0	0	0	0	0	0
Asleep or Fatigued	0	0	0	0	0	0	0
Under the Influence of Medications/Drugs/Alcohol	1	0	0	0	0	0	1
Other	0	0	0	0	0	0	0
Total	15	16	1	0	0	0	32

Driver Age by Unit Type

Age	Driver	Bicycle	SnowMobile	Pedestrian	ATV	Total
09-Under	0	0	0	0	0	0
10-14	0	0	0	0	0	0
15-19	3	0	0	0	0	3
20-24	2	0	0	0	0	2
25-29	3	0	0	0	0	3
30-39	8	0	0	0	0	8
40-49	4	0	0	0	0	4
50-59	5	0	0	0	0	5
60-69	4	0	0	0	0	4
70-79	2	0	0	0	0	2
80-Over	1	0	0	0	0	1
Unknown	1	0	0	0	0	1
Total	33	0	0	0	0	33

Crash Summary II - Characteristics

Most Harmful Event			
Most Harmful Event	Total	Most Harmful Event	Total
1-Overturn / Rollover	0	38-Other Fixed Object (wall, building, tunnel, etc.)	0
2-Fire / Explosion	0	39-Unknown	0
3-Immersion	0	40-Gate or Cable	0
4-Jackknife	0	41-Pressure Ridge	0
5-Cargo / Equipment Loss Or Shift	0	Total	32
6-Fell / Jumped from Motor Vehicle	0		
7-Thrown or Falling Object	0		
8-Other Non-Collision	0		
9-Pedestrian	0		
10-Pedalcycle	0		
11-Railway Vehicle - Train, Engine	0		
12-Animal	0		
13-Motor Vehicle in Transport	32		
14-Parked Motor Vehicle	0		
15-Struck by Falling, Shifting Cargo or Anything Set in Motion by Motor Vehicle	0		
16-Work Zone / Maintenance Equipment	0		
17-Other Non-Fixed Object	0		
18-Impact Attenuator / Crash Cushion	0		
19-Bridge Overhead Structure	0		
20-Bridge Pier or Support	0		
21-Bridge Rail	0		
22-Cable Barrier	0		
23-Culvert	0		
24-Curb	0		
25-Ditch	0		
26-Embankment	0		
27-Guardrail Face	0		
28-Guardrail End	0		
29-Concrete Traffic Barrier	0		
30-Other Traffic Barrier	0		
31-Tree (Standing)	0		
32-Utility Pole / Light Support	0		
33-Traffic Sign Support	0		
34-Traffic Signal Support	0		
35-Fence	0		
36-Mailbox	0		
37-Other Post, Pole, or Support	0		

Traffic Control Devices		
Traffic Control Device	Total	
1-Traffic Signals (Stop & Go)	2	
2-Traffic Signals (Flashing)	4	
3-Advisory/Warning Sign	0	
4-Stop Signs - All Approaches	0	
5-Stop Signs - Other	7	
6-Yield Sign	0	
7-Curve Warning Sign	0	
8-Officer, Flagman, School Patrol	1	
9-School Bus Stop Arm	0	
10-School Zone Sign	0	
11-R.R. Crossing Device	0	
12-No Passing Zone	0	
13-None	1	
14-Other	1	
Total	16	

Injury Data		
Severity Code	Injury Crashes	Number Of Injuries
K	0	0
A	0	0
B	2	2
C	3	4
PD	11	0
Total	16	6

Road Character	
Road Grade	Total
1-Level	14
2-On Grade	2
3-Top of Hill	0
4-Bottom of Hill	0
5-Other	0
Total	16

Light	
Light Condition	Total
1-Daylight	13
2-Dawn	0
3-Dusk	0
4-Dark - Lighted	1
5-Dark - Not Lighted	2
6-Dark - Unknown Lighting	0
7-Unknown	0
Total	16

Crash Summary II - Characteristics

Crashes by Year and Month

Month	2023	2024	2025	Total
JANUARY	1	0	1	2
FEBRUARY	1	0	4	5
MARCH	0	1	0	1
APRIL	0	0	1	1
MAY	0	0	0	0
JUNE	0	0	0	0
JULY	0	0	0	0
AUGUST	0	3	0	3
SEPTEMBER	0	0	0	0
OCTOBER	0	0	1	1
NOVEMBER	0	0	0	0
DECEMBER	2	0	1	3
Total	4	4	8	16

Report is limited to the last 10 years of data.

Crash Summary II - Characteristics

Crashes by Crash Type and Type of Location

Crash Type	Straight Road	Curved Road	Three Leg Intersection	Four Leg Intersection	Five or More Leg Intersection	Driveways	Bridges	Interchanges	Other	Parking Lot	Private Way	Cross Over	Railroad Crossing	Traffic Circle-Roundabout	Total
Object in Road	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Rear End - Sideswipe	0	0	0	2	0	0	0	0	0	0	0	0	0	0	2
Head-on - Sideswipe	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Intersection Movement	0	0	0	14	0	0	0	0	0	0	0	0	0	0	14
Pedestrians	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Train	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Went Off Road	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
All Other Animal	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Bicycle	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Other	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Jackknife	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Rollover	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Fire	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Submersion	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Thrown or Falling Object	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Bear	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Deer	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Moose	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Turkey	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Total	0	0	0	16	0	0	0	0	0	0	0	0	0	0	16

Crash Summary II - Characteristics

Crashes by Weather, Light Condition and Road Surface

Weather Light	Dry	Ice/Frost	Mud, Dirt, Gravel	Oil	Other	Sand	Slush	Snow	Unknown	Water (Standing, Moving)	Wet	Total
Blowing Sand, Soil, Dirt												
Dark - Lighted	0	0	0	0	0	0	0	0	0	0	0	0
Dark - Not Lighted	0	0	0	0	0	0	0	0	0	0	0	0
Dark - Unknown Lighting	0	0	0	0	0	0	0	0	0	0	0	0
Dawn	0	0	0	0	0	0	0	0	0	0	0	0
Daylight	0	0	0	0	0	0	0	0	0	0	0	0
Dusk	0	0	0	0	0	0	0	0	0	0	0	0
Unknown	0	0	0	0	0	0	0	0	0	0	0	0
Blowing Snow												
Dark - Lighted	0	0	0	0	0	0	0	0	0	0	0	0
Dark - Not Lighted	0	0	0	0	0	0	0	0	0	0	0	0
Dark - Unknown Lighting	0	0	0	0	0	0	0	0	0	0	0	0
Dawn	0	0	0	0	0	0	0	0	0	0	0	0
Daylight	0	0	0	0	0	0	0	0	0	0	0	0
Dusk	0	0	0	0	0	0	0	0	0	0	0	0
Unknown	0	0	0	0	0	0	0	0	0	0	0	0
Clear												
Dark - Lighted	0	0	0	0	0	0	0	0	0	0	0	0
Dark - Not Lighted	2	0	0	0	0	0	0	0	0	0	0	2
Dark - Unknown Lighting	0	0	0	0	0	0	0	0	0	0	0	0
Dawn	0	0	0	0	0	0	0	0	0	0	0	0
Daylight	9	1	0	0	0	0	0	0	0	0	1	11
Dusk	0	0	0	0	0	0	0	0	0	0	0	0
Unknown	0	0	0	0	0	0	0	0	0	0	0	0
Cloudy												
Dark - Lighted	0	0	0	0	0	0	0	0	0	0	0	0
Dark - Not Lighted	0	0	0	0	0	0	0	0	0	0	0	0
Dark - Unknown Lighting	0	0	0	0	0	0	0	0	0	0	0	0
Dawn	0	0	0	0	0	0	0	0	0	0	0	0
Daylight	0	0	0	0	0	0	0	0	0	0	0	0
Dusk	0	0	0	0	0	0	0	0	0	0	0	0
Unknown	0	0	0	0	0	0	0	0	0	0	0	0

Crash Summary II - Characteristics

Crashes by Weather, Light Condition and Road Surface

Weather Light	Dry	Ice/Frost	Mud, Dirt, Gravel	Oil	Other	Sand	Slush	Snow	Unknown	Water (Standing, Moving)	Wet	Total
Fog, Smog, Smoke												
Dark - Lighted	0	0	0	0	0	0	0	0	0	0	0	0
Dark - Not Lighted	0	0	0	0	0	0	0	0	0	0	0	0
Dark - Unknown Lighting	0	0	0	0	0	0	0	0	0	0	0	0
Dawn	0	0	0	0	0	0	0	0	0	0	0	0
Daylight	0	0	0	0	0	0	0	0	0	0	0	0
Dusk	0	0	0	0	0	0	0	0	0	0	0	0
Unknown	0	0	0	0	0	0	0	0	0	0	0	0
Other												
Dark - Lighted	0	0	0	0	0	0	0	0	0	0	0	0
Dark - Not Lighted	0	0	0	0	0	0	0	0	0	0	0	0
Dark - Unknown Lighting	0	0	0	0	0	0	0	0	0	0	0	0
Dawn	0	0	0	0	0	0	0	0	0	0	0	0
Daylight	0	0	0	0	0	0	0	0	0	0	0	0
Dusk	0	0	0	0	0	0	0	0	0	0	0	0
Unknown	0	0	0	0	0	0	0	0	0	0	0	0
Rain												
Dark - Lighted	0	0	0	0	0	0	0	0	0	0	0	0
Dark - Not Lighted	0	0	0	0	0	0	0	0	0	0	0	0
Dark - Unknown Lighting	0	0	0	0	0	0	0	0	0	0	0	0
Dawn	0	0	0	0	0	0	0	0	0	0	0	0
Daylight	0	0	0	0	0	0	0	0	0	0	1	1
Dusk	0	0	0	0	0	0	0	0	0	0	0	0
Unknown	0	0	0	0	0	0	0	0	0	0	0	0
Severe Crosswinds												
Dark - Lighted	0	0	0	0	0	0	0	0	0	0	0	0
Dark - Not Lighted	0	0	0	0	0	0	0	0	0	0	0	0
Dark - Unknown Lighting	0	0	0	0	0	0	0	0	0	0	0	0
Dawn	0	0	0	0	0	0	0	0	0	0	0	0
Daylight	0	0	0	0	0	0	0	0	0	0	0	0
Dusk	0	0	0	0	0	0	0	0	0	0	0	0
Unknown	0	0	0	0	0	0	0	0	0	0	0	0

Crash Summary II - Characteristics

Crashes by Weather, Light Condition and Road Surface

Weather Light	Dry	Ice/Frost	Mud, Dirt, Gravel	Oil	Other	Sand	Slush	Snow	Unknown	Water (Standing, Moving)	Wet	Total
Sleet, Hail (Freezing Rain or Drizzle)												
Dark - Lighted	0	0	0	0	0	0	0	0	0	0	0	0
Dark - Not Lighted	0	0	0	0	0	0	0	0	0	0	0	0
Dark - Unknown Lighting	0	0	0	0	0	0	0	0	0	0	0	0
Dawn	0	0	0	0	0	0	0	0	0	0	0	0
Daylight	0	0	0	0	0	0	0	0	0	0	0	0
Dusk	0	0	0	0	0	0	0	0	0	0	0	0
Unknown	0	0	0	0	0	0	0	0	0	0	0	0
Snow												
Dark - Lighted	0	0	0	0	0	0	0	1	0	0	0	1
Dark - Not Lighted	0	0	0	0	0	0	0	0	0	0	0	0
Dark - Unknown Lighting	0	0	0	0	0	0	0	0	0	0	0	0
Dawn	0	0	0	0	0	0	0	0	0	0	0	0
Daylight	0	0	0	0	0	0	0	0	0	0	1	1
Dusk	0	0	0	0	0	0	0	0	0	0	0	0
Unknown	0	0	0	0	0	0	0	0	0	0	0	0
TOTAL	11	1	0	0	0	0	0	1	0	0	3	16

Janet T. Mills
Governor

Sara Gagné-Holmes
Commissioner



Maine Department of Health and Human Services
Maine Center for Disease Control and Prevention
11 State House Station
286 Water Street
Augusta, Maine 04333-0011
Tel; (207) 287-8016; Fax (207) 287-2887
TTY: Dial 711 (Maine Relay)

July 22, 2026

Robie Holdings
PO Box 1508
Windham, ME 04062
c/o Mr. Jayson Haskell, P.E.

Subject: Approval, proposed SWW for Legacy Village Retirement Community, Webb Road, Windham, ME

Dear Mr. Haskell:

The Division of Environmental and Community Health has completed a review of a design for an engineered subsurface wastewater disposal system design, to serve this proposed 75-bedroom retirement facility. The HHE-200 Form dated July 13, 2026, was prepared by Scott Dixon, S.E. The system was designed by Main Land Development Consultants, Inc., with plans signed and stamped by Scott Dixon, P.E.

Hereinafter, the term "design engineer" shall refer collectively to Main Land Development Consultants, Inc., its staff, and its representatives unless otherwise specified; and the term "owner" shall refer collectively to Robie Holdings, its staff, and its representatives unless otherwise specified.

Design Flow

The design flow is 6,750 gallons per day (gpd), based upon Table 5C of the Maine State Plumbing Code, Subsurface Wastewater Disposal Rules (Rules). The design flow of 6,750 gpd is approved with the notation that the suitability of the design flow is the responsibility of the design engineer.

Treatment Tank(s)

Wastewater from the residences is collected in two tank-treatment locations. At one location near the northern end of the line of cottages, two 1,500-gallon septic tanks in series feed two FujiClean CEN 14 Advanced Wastewater Treatment Units in parallel before the pump station and force main pumps the effluent to the disposal area. At the southern end of the row of cottages, two 2,000-gallon septic tanks in series feed three FujiClean CEN 14 Advanced Wastewater Treatment Units in parallel before the pump station and force main transports the effluent to the disposal area.

Disposal Areas

A 1,000-gallon septic tank stills the flow from the force main. The water then distributed between two beds of 70 4-foot by 8-foot concrete chambers (140 chambers total). The chambered portion of each bed is 40 feet wide by 56 feet long. The fill extension is reported to be 38 feet long and the lower third is designed to be composed of a loamy material.

Soils

The soils have been identified as 4C per the Rules by Scott Dixon, S.E. Reduced conditions were observed near the base of the thin ablation till layer. Seasonal high groundwater was therefore assumed to occur within the weathered bedrock.

Mounding Analysis

The proposed system has been designed such that the calculated groundwater mounding will not result in a compromise of the separation specified in Table 5F of the Rules, according to the report dated July 15, 2026, by Scott Dixon, L.G.

Site Transmission Analysis

The proposed system design demonstrates that the native soil and/or fill material will have sufficient capacity to prevent wastewater from surfacing downgradient of the disposal field, according to the report dated July 15, 2026, by Scott Dixon, L.G.

Well Setback

There are no potable water supply wells reported within 300 feet of the proposal. The HHE-200 reports that the project is served by public water.

Interagency Review

This project was reviewed by The Maine Department of Environmental Protection (MDEP) pursuant to the Site Memorandum of Understanding between DHHS and DEP, dated in May 2023. Review of the proposed on-site engineered subsurface wastewater disposal system included: (1) the geology of the project area and vicinity, (2) effects of the project on groundwater and surface water quality, and (3) public and private uses of groundwater and surface water resources in the project area and vicinity. The review found no reason to believe that normal operation of the proposed engineered subsurface wastewater disposal system will result in unreasonable adverse impact on the natural environment or other uses of groundwater and surface water, and provided that the system is properly constructed and maintained.

The DEP reviewer made the following comments:

- The project site is *not* located on a significant sand and gravel aquifer (MGS), in a watershed of a waterbody most at risk from development (Chapter 502, DEP Regulations), *or* within a flood zone as mapped by FEMA.
- The nearest wetlands are more than 500 feet to the southwest of the proposed disposal field as mapped by the National Wetlands Inventory (NWI).

Miscellaneous

No variance to the Subsurface Wastewater Rules is required.

The design engineer and the Division met and discussed the proposal on October 9, 2025, pursuant to Section 11.2.a of the Rules.

Findings

The system meets the Rules, unless otherwise noted. Therefore, the design is approved with the following conditions and comments:

1. The owner must retain the design engineer to oversee construction. The constructed system may not be used unless all pertinent requirements of the Rules have been met.
2. Construction must not commence until the owner has obtained the necessary plumbing permit from the Local Plumbing Inspector (LPI).
3. The design engineer must provide sufficient supervision to assure that the system is constructed as designed and in accordance with the code and other regulations. Attention must be given to site preparation, fill selection and placement, installation of pipes, mechanical and electrical systems.
4. The design engineer must provide the owner and this office with a brief report on the construction including any unexpected conditions encountered and any changes made to the approved drawings. The LPI must not issue the Certificate of Approval until the LPI has received the aforementioned report from the design engineer.
5. The design engineer must test all systems prior to acceptance by the owner. The testing must determine whether the components were correctly installed and whether they function as designed. This includes confirmation that flow dividing devices or configurations function as intended.
6. The design engineer, with the concurrence of the LPI must determine when the site conditions are suitable for construction.
7. Construction must cease whenever the design engineer determines that the site conditions, or workmanship, or materials are unacceptable.
8. The owner and design engineer must inform the LPI of the proposed construction schedule and must also inform the LPI of the progress of construction. They must cooperate fully with the LPI in scheduling any inspections and providing any equipment necessary for the inspection.
9. The design engineer must provide the owner with an Operations and Maintenance Manual containing written recommendations for the operation and maintenance of the system including inspection and pumping schedules and record keeping procedures.
10. The owner must operate the system within the requirements of the Rules and the limitations of this design.
11. The owner must inform the LPI and the design engineer of any operational problem and/or malfunction.
12. The Local Plumbing Inspector must inspect the engineered disposal system in accordance with Section 11 Letter I of the Rules. In addition, the property owner must retain the design engineer to inspect the construction of the system. The inspection must be sufficient for the design engineer to determine that the system was installed as designed.

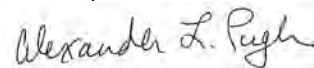
13. The five FujiClean CEN 14 Advanced Treatment Units are to be installed and maintained by the appropriate professionals according to the manufacturer's recommendations. Biannual inspections of these units are to include laboratory analysis of the effluent for at least Nitrate Nitrogen, TKN, BOD and TSS. These concentrations are to be compared with the manufacturer's claims of performance. Both the Department of Health and Human Services and the Department of Environmental Protection must be notified within five business days if any effluent quality data fail to meet a wastewater strength of 30 mg/l, or if either the nitrate-nitrogen or TKN concentrations in the effluent exceed 15 mg/L. All records of the sampling and all effluent quality data must be maintained on site and must be provided to the Town of Winham, the Department of Health and Human Services and the Department of Environmental Protection on demand. This requirement should be added to the Operations and Maintenance Manual for the System. A revised copy of the manual including the effluent sampling, data retention and notification requirements should be sent in PDF form to the Department and used by the maintenance staff.
14. This approval is only for the rules administered by this office, and it does not consider other federal, state or local regulations. The owner is responsible for compliance with any other pertinent regulations.
15. By accepting this approval and the associated plumbing permit, the owner agrees to comply fully with the conditions of approval and the Subsurface Wastewater Disposal Rules.

Based upon this approval of the design, the LPI may issue the permit required for an engineered system.

Because installation and owner maintenance have a significant effect on the working order of onsite sewage disposal systems, including their components, the Division makes no representation or guarantee as to the efficiency and/or operation of the system.

Should you have any questions, please feel free to contact me at (207) 592-2086, or by e-mail at alex.l.pugh@maine.gov.

Sincerely,



Alexander L. Pugh
Senior Environmental Hydrogeologist
Division of Environmental and Community Health
Drinking Water Program

Electronic copies to:

Jon Rioux, L.P.I.
Scott Dixon, P.E.
William Noble, MDEP



APPLICATION FOR ENGINEERED SEPTIC SYSTEM

SERVING THE PROPOSED LEGACY VILLAGE
RETIREMENT COMMUNITY
WEBB ROAD, WINDHAM, MAINE

PREPARED FOR: ROBIE HOLDINGS, LLC

MAIN-LAND DEVELOPMENT CONSULTANTS, INC.
PO BOX Q, 69 MAIN STREET, LIVERMORE FALLS, MAINE 04254
367 U.S. ROUTE 1, N. BUILDING, FALMOUTH, MAINE 04105
182A MOOSEHEAD TRAIL, NEWPORT, ME 04953
(207) 897-6752



MAIN-LAND

DEVELOPMENT
CONSULTANTS, INC.

ENGINEERS, SURVEYORS, SCIENTISTS

P.O. BOX Q LIVERMORE FALLS, ME 04254
367 US ROUTE 1, N. BUILDING, FALMOUTH, ME 04105
182A MOOSEHEAD TRAIL, NEWPORT, ME 04953
TEL: (207) 897-6752/FAX: (207) 897-5404
WWW.MAIN-LANDDCI.COM

July 13, 2026

Division of Environmental and Community Health
286 Water Street, 3rd Floor
11 State House Station
Augusta, Maine 04333-0011

SUBJECT: Engineered Wastewater Disposal System Design
Serving the Proposed Legacy Village Retirement Community
Webb Road, Windham, Maine

Dear Engineering and Water Resources Team,

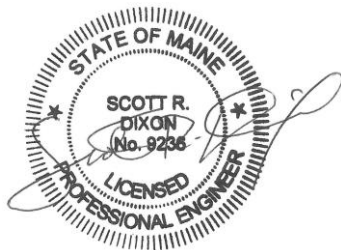
Enclosed please find one copy of the application package for the proposed Engineered Leachfield serving the proposed Woodlands residential development in Standish, Maine. The \$100 application fee has been sent via regular mail along with two copies of the full-size project drawings.

The package follows the requirements of the HHE-220 form, which is also enclosed as part of this application. Please do not hesitate to contact Main-Land if we can provide additional information relevant to your review of this application.

As discussed during our Pre-Application meeting on 10/9/25, the Owner, Site Civil Engineer, and Main-Land appreciate your review of this submittal. Please note that the design flow for the current project (6,750 gpd) is lower than the design flow discussed during our 10/9/25 pre-app meeting (9,810 gpd).

Sincerely,

Main-Land Development Consultants, Inc.



Scott R. Dixon, P.E., C.G., L.S.E.
Senior Chief Environmental Scientist

Attachment: Application

DATE: July 13, 2026

PROJECT:

Application for Engineered Subsurface Wastewater Disposal System
Serving the Proposed Legacy Village Retirement Community
Webb Road, Windham, Maine

TABLE OF CONTENTS

TAB NUMBER	ITEM
1	Application Form – HHE 220
2	Exhibit A – USGS Site Plan
3	Exhibit B and C – Combined Mounding and Transmissivity Report
4	Exhibit D – HHE 200 form
5	Exhibit E – Operations and Maintenance Manual
6	Exhibit F – Soil Logs
7	Exhibit G – Design Plan

Janet T. Mills
Governor

Jeanne M. Lambrew, Ph.D.
Commissioner



Maine Department of Health and Human Services
Maine Center for Disease Control and Prevention
11 State House Station
286 Water Street
Augusta, Maine 04333-0011
Tel; (207) 287-8016; Fax (207) 287-9058
TTY: Dial 711 (Maine Relay)

APPLICATION FOR ENGINEERED
SUBSURFACE WASTEWATER DISPOSAL SYSTEM

Please complete the following Sections. Please print or type.

Applicant/Owner

Company Name: Robie Holdings
Contact Person: c/o Mr. Jayson Haskell, P.E. (DM Roma Engineers)
Address: (Robie Holdings) P.O. Box 1508
Town/City: Windham State/Province: ME Zip/Postal Code: 04062
Country: U.S.
Telephone: c/o Mr. Haskell 207-591-5055 Fax: _____
e-mail: jayson@dmroma.com

Design Engineer

Company Name: Main-Land Development Consultants, Inc.
Contact Person: Scott R. Dixon
Address: P.O. Box Q
Town/City: Livermore Falls State: ME Zip Code: 04254
Telephone: 207-897-6752 Fax: _____
e-mail: scott@main-landdci.com

1. Property Location

Town/City: Windham, ME County: Cumberland

Tax Map and Lot Number: Map 6 Lot 33 (21.4+/- acres)

Attach as "Exhibit A" a copy of the relevant section of the USGS 7.5' topographic map, if available, or 15' topographic map showing the location of the proposed engineered disposal system.

2. Project Description

Provide a brief written description of the proposal. Use a separate sheet if necessary.

The proposed engineered leachfield will serve up to 75 bedrooms within the development. The leachfield will consist of two
separate beds of 70 concrete chambers each, for 140 total units. Five FujiClean CEN 14 Advanced Treatment Units will be employed to
allow a 50% reduction in the leachfield size/number of chamber units.

3. Design Flow

The design flow for this project is: 6,750 gpd gallons per day. Provide design flow calculations and assumptions used in the calculations. Use a separate sheet if necessary.

75 bedrooms x 90 gpd/bedroom = 6,750 gpd

4. Mounding Analysis

Submit as "Exhibit B" an analysis of the proposed system design showing that there is adequate vertical separation between the bottom of the disposal field and any mounded water table. Include all calculations and assumptions used.

5. Transmissivity Analysis

Submit as "Exhibit C" an analysis of the proposed system design showing that there are sufficient suitable soils down-gradient to prevent the effluent from surfacing within 50 feet of the disposal field. Include all calculations and assumptions used.

6. HHE-200 and Variance Form(s)

Submit as "Exhibit D" a complete HHE-200 Form, and variance forms if applicable, signed by a Professional Engineer. The design engineer may reference associated plans and soil test pit logs on pages 2 and 3 of the HHE-200 Form.

This project requires:

- ☐ a First Time System Variance to the Maine Subsurface Wastewater Disposal Rules.
- ☐ a Replacement System Variance to the Maine Subsurface Wastewater Disposal Rules.
- ☒ no variance to the Maine Subsurface Wastewater Disposal Rules.

7. Operations and Maintenance Manual

Submit as "Exhibit E" an operations and maintenance manual for the owner with written recommendations for the operation and maintenance of the system, including inspection schedules, pumping schedules, and record keeping procedures.

8. Soil and Site Conditions

Submit as "Exhibit F" soil test pit logs prepared by a licensed Site Evaluator. The test pits shall be of sufficient number to accurately describe the site conditions under the proposed disposal area and the down gradient fill extension.

9. Plans

Submit as "Exhibit G" plans for the proposed engineered disposal system meeting provisions of Section 1102 of the Maine Subsurface Wastewater Disposal Rules. Two sets of plans are required, or one set of plans and one set of copies no larger than 11" x 17". Plans may be submitted for review purposes in digital format.

The plans must specify the latitude and longitude of the center of the disposal area(s), expressed as degrees, minutes, and seconds. If this data is obtained from an electronic GIS device, provide the device's margin of error.

10. Review Fee

Submit a check or money order in the amount of \$100.00 U.S. made payable to the Treasurer of the State of Maine.

I, Scott R. Dixon, am the design engineer for the subject design.
(print name)

I state that the information submitted is correct to the best of my knowledge and understand that any falsification is reason for the Department to deny the project.


Signature of Design Engineer

PE 9236

P.E. License Number

7 /13/26

Date

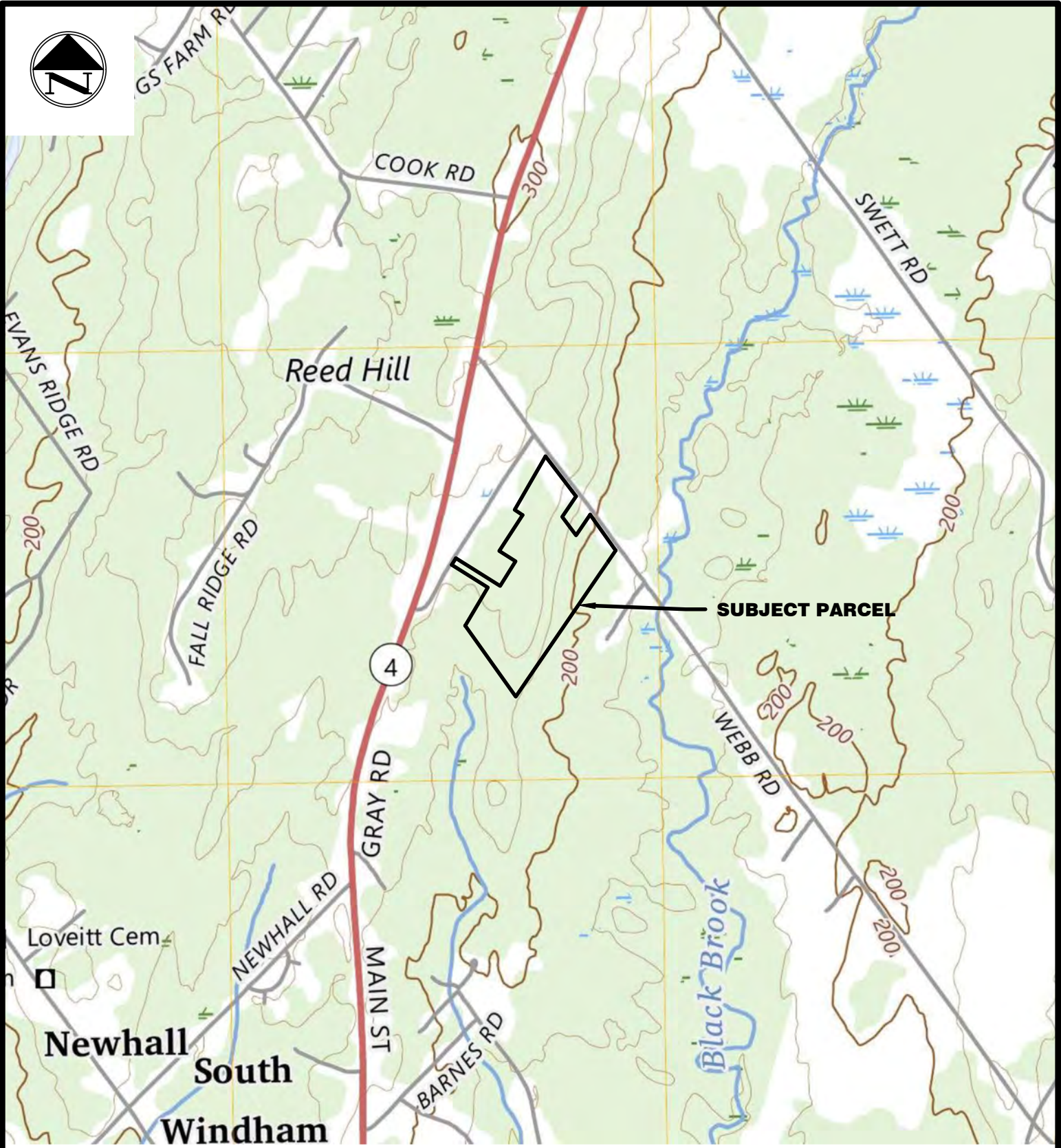


HHE-220
04/2019

EXHIBIT A

USGS Site Plan





- NOTES
1. TOWN OF WINDHAM: TAX MAP 6, LOT 33.
 2. TOPOGRAPHY SHOWN IS BASED ON MAP DOWNLOADED FROM USGS "TOPOVIEW" AND DEPICTS MAP ENTITLED "NORTH WINDHAM, ME" DATED 2024.

NOT FOR CONSTRUCTION

PROJECT:	ENGINEERED SYSTEM WEBB ROAD, WINDHAM, ME
DRAWING:	USGS SITE MAP

MLDC NO.	25-328
PROJ. MGR:	SRD
DRAWN BY:	HRD
CHECKED BY:	SRD
REVISION NO.	N/A
ISSUE DATE:	2026-07-13
ISSUED FOR:	APPLICATION

MAIN-LAND DEVELOPMENT CONSULTANTS, INC. 69 MAIN ST. LIVERMORE FALLS, MAINE 367 US ROUTE 1 FALMOUTH, MAINE PH: (207) 897-6752 FAX: (207) 897-5404 WWW.MAIN-LANDDCI.COM	
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EXHIBIT B and C

Combined Mounding and Transmissivity Report





MAIN-LAND

DEVELOPMENT
CONSULTANTS, INC.

ENGINEERS, SURVEYORS, SCIENTISTS

P.O. BOX Q LIVERMORE FALLS, ME 04254
367 US ROUTE 1, N. BUILDING, FALMOUTH, ME 04105
182A MOOSEHEAD TRAIL, NEWPORT, ME 04953
TEL: (207) 897-6752/FAX: (207) 897-5404
WWW.MAIN-LANDDCI.COM

July 13, 2026

Robie Holdings, LLC
c/o Mr. Jayson Haskell, P.E.
D.M. Roma Consulting Engineers
P.O. Box 1116, Windham, ME 04062

SUBJECT: Mounding and Transmissivity Analyses
Engineered Wastewater Disposal System Design
Serving the Proposed Legacy Village Retirement Community
Webb Road, Windham, Maine

Dear Jayson,

As part of the application for Engineered Subsurface Wastewater Disposal System permitting for the subject project, Main-Land Development Consultants, Inc. (Main-Land) is pleased to provide the following analyses of wastewater Mounding and Transmissivity. These analyses are for the proposed new Engineered Leachfield to serve the proposed Legacy Village Retirement Community development located off Webb Road in Windham, Maine. These analyses are provided as combined Exhibits B and C of the Engineered System permit application.

INTRODUCTION

The proposed Engineered Leachfield is to serve up to 75 bedrooms within the single-family housing development. Per the Maine Subsurface Wastewater Disposal Rules, updated 9/23/23 (i.e., the *Rules*), the design flow is:

$$90 \text{ gpd/bedroom} \times 75 \text{ bedrooms} = 6,750 \text{ gpd}$$

The site will be served by private water supply wells; site civil and infrastructure design is by DM Roma Consulting Engineers.

Based on the above design flow, the proposed system design must meet current engineered system design and permitting standards. Main-Land provides the following evaluation of site hydrogeology, as well as mounding and transmissivity analyses, in support of engineered system design and permitting.

SITE AND LOCAL HYDROGEOLOGY

Characteristics of the groundwater aquifer underlying the project site are based on Main-Land's evaluation of project test pits and other site observations, and laboratory grain size analysis. Main-Land performed laboratory grain size analysis by ASTM D422 on a representative sample of native ablation glacial till soils collected from Test Pit TP-3 on the project site. The grain size analysis sheet and

permeability estimate are attached (see Attachment B). The grain size distributions were evaluated using the Kozeny-Carmen approach to estimate soil permeability, as summarized in the following table:

Soil sample	Estimated permeability, k
TP-3, 2'-3' depth	20 feet/day

The project site is located in a moderately sloping area off the southeastern side of Webb Road. The ablation glacial till soils observed in the test pits suggest the general upland character of the geographic setting. Weathered bedrock was encountered underlying ablation till soils at depths of about 3 to 4 feet. Owing to the shallower bedrock and the location along the crest of a gentle ridge (at the top of the local watershed), free groundwater was not observed in the test pits at the time of the explorations (8/27/25). Reduced conditions were observed near the base of the till layer and extending down into the underlying weathered rock zone. Therefore, seasonal high groundwater was taken as occurring within the weathered rock zone near below the base of the ablation till soil layer.

Based on site observations and available data, Main-Land estimated the aquifer thickness beneath the leachfield area as about 3.5-feet thick, which includes soil deposits and the upper zone of fractured and permeable weathered rock above the harder bedrock surface. Reduced conditions were typically observed in the bottom 6 inches of this profile above the harder bedrock. Therefore, seasonal high groundwater has been taken as occurring at 3 feet deep in the soil/weathered rock profile underlying the leachfield bed footprints.

GROUNDWATER MOUNDING AND TRANSMISSIVITY ANALYSIS

Based on the underlying 4 soil profile (ablation glacial till with about 36% gravel, 42% sand, and 22% silt – 2.6 ft²/gpd sizing factor) identified by Main-Land's Licensed Site Evaluator, the leachfield would need to be a minimum of 2.6 x 6,750 effective gpd = 17,550 ft² in total treatment area needed.

To reduce the footprint size and reduce nitrates for property line considerations, five FujiClean Tertiary Advanced Treatment Units (CEN 14 ATUs) are proposed to treat the domestic wastewater and allow a 50% reduction in leachfield treatment area. Therefore, this results in:

17,550 ft² total treatment area/2 for 50% ATU reduction = 8,775 ft² treatment area

18,775 ft² total treatment area/64 ft² per concrete chamber in cluster = 137 chambers, minimum (use 140 units)

The chambers will be arranged in two beds (Bed 1 and Bed 2) of 70 units each, with a configuration of 40-feet wide by 56-feet long per bed; this results in 5 rows of 14 side-feed chambers per bed (i.e., 70 units per bed x 2 beds = 140 units). It is noted that, without pretreatment, the 4 profile soils/AIII bedrock condition requires a minimum of 24 inches vertical separation between base of leachfield and predicted groundwater mound. Per FujiClean Modified Approval for General Use, CEN Series (dated 10/12/16), with the FujiClean pretreatment the minimum separation distance above bedrock can be reduced to 12 inches.

Mounding - Wastewater mounding analysis was performed for the proposed Engineered Leachfield. The purpose of the mounding analysis is to determine the potential rise in the groundwater level due to

wastewater infiltration through the unsaturated zone to the groundwater surface or base of aquifer below the leachfield.

The mounding analysis used was developed by M.S. Hantush in 1967 to predict rises in groundwater from external recharge sources. The model incorporates assumptions including infinite aquifer area with homogeneous and isotropic conditions over a horizontal impermeable base, constant formation coefficients, and constant recharge rate and uniform distribution over the leachfield footprint, to simplify the model. Required input includes leachfield area, recharge rate, time of interest, and aquifer characteristics (hydraulic conductivity and specific yield). Main-Land used a mounding calculator for the Hantush equation created by Glenn M. Duffield and found on Hydrosolve, Inc.'s website.

Based on review of available hydrogeologic data, Main-Land selected the following input to model conditions for the analysis of mounding beneath each bed:

$h_i = 0.5 \text{ feet}^*$ = initial height of water surface above base of aquifer (based on review of Main-Land test pit information)

*equivalent to 6" of seasonal high groundwater occurring in the reduced soil/weathered rock zone above harder bedrock; note that the groundwater height is low due to leachfield's location near top of local watershed.

$W = \text{recharge rate} = ((3,375 \text{ gpd/bed}) / 7.48 \text{ ft}^3 \text{ per gallon}) / ((40 \times 56) = 451.2 \text{ ft}^3 / 2,240 \text{ ft}^2 = 0.201 \text{ ft./day/bed}$

$S_y = \text{Specific Yield} = 0.25^*$

*Value derived for coarse to fine sand soil from Domenico & Schwartz, 1990.

$K, \text{ composite hydraulic conductivity} = 35 \text{ ft/day}^*$

*composite of 20 ft/day for native soil from Kozeny-Carmen analysis and estimated 60 ft/day for clean gravelly sand backfill constituting fill below and around chambers

$*K_{\text{composite}} = ([20 \text{ ft/day} \times 3.5' \text{ stratum thickness}] + [60 \text{ ft/day} \times 2' \text{ backfill average thickness}]) / 5.5 \text{ feet total thickness of transmitting medium} = 35 \text{ ft/day}$

For an individual leachfield bed with base dimensions: $x = 40'$, leachfield width and $y = 56'$, leachfield length

Time = days of interest (modeled 365 days)

The estimated mound height calculated below the center of the leachfield beds is on the order of 3.5 feet (see Attachment B). The estimated base of aquifer/top of hard bedrock beneath the centers of each leachfield is about El. 237 feet existing grade – 3.5 feet thick aquifer = El. 233.5 feet. With an estimated seasonal high groundwater height of 6" above top of hard bedrock based on reduced conditions observed, the seasonal high groundwater would then occur near El. 234 feet. With this, the mound is estimated to occur up to about $\text{El. } 234 + 3.5 = \text{El. } 237.5 \text{ feet}$ beneath the centers of the beds, or about 0.5 foot above existing grade of El. 237 feet at the centers of the beds. The bottom of the 3-inch thick stone layer elevation

is designed as El. 239 feet and bottom of chamber as El. 239.3 feet (Note: Bottom of stone El. 239 – Existing Grade El. 237 = 2 feet of fill beneath center of bed, which is the average fill thickness in the $K_{\text{composite}}$ calculation above). The bottom of stone elevation is roughly:

El. 239 feet bottom of stone – El 237.5 feet top of mound = 1.5 feet or

18” above the estimated mound, which meets the minimum 12” vertical separation for a 4-profile soil and/or an AIII bedrock condition with pretreatment. The estimated mounding is depicted on Drawing E1.1, attached to the overall application package.

Because the top of bedrock slopes gently southwestward with the ground surface, and the clustered chambers are placed flat, the elevation of the seasonal high groundwater limiting factor becomes deeper in the downgradient direction. The separation between the limiting factor and the bottom of the flat chamber layout also increases, which in turn increases the depth and subsequent infiltration/treatment time for the wastewater to the limiting factor. In addition, the wastewater is being pre-treated by the tertiary FujiClean ATUs, and impacts to groundwater are anticipated to be minimal due to the near runoff quality of the ATU effluent.

Transmissivity - The estimated mound elevation beneath the center of the leachfield beds is on the order of 0.5 foot above existing grade, and in the general direction of groundwater flow southwestward. Based on the mounding data, approximately 40 feet from the centers of the beds and southwestward in the direction of groundwater flow, the mound degrades in height to about 3.5 feet above the limiting factor. Since the soil/weathered rock zone is on the order of 3.5 feet thick, then the mound is anticipated to be at or below ground surface about 40 feet from the centers of the beds; this distance equates to about 20 feet beyond the downslope edges of the beds. Since the downslope fill extensions are on the order of 38 feet long, then break out above ground surface within the 50 feet of interest downgradient of the leachfield is not anticipated, i.e., the mound is anticipated to be below ground surface beneath the fill extension length of approximately 38 feet.

ATUs AND SEPTIC TANK VOLUME

It has been indicated by the FujiClean ATU design and distribution team that the volume of septic tanks upstream of the ATUs should not exceed the equivalent of 1-day of liquid retention time. In other words, for this project, the septic tank volume should not exceed 7,000 gallons for the 6,750 gpd design flow. This design requirement is based on FujiClean not wanting excessive liquid retention time whereby ammonization can begin to take place in the wastewater with longer retention; excess ammonization of nitrates impacts the effectiveness of treatment within the ATUs.

This ATU Manufacturer’s tank volume requirement differs from what the *Rules* would call for, which is a minimum total tank volume of 1.5 times the daily design flow. For this project, that would equate to about 10,000 gallons of septic tanks. Main-Land and the State have discussed and addressed this Manufacturer’s requirement on previous engineered system projects requiring FujiClean ATUs. Main-Land’s design for the subject project includes 7,000 gallons of septic tank volume upstream of the ATUs, as depicted conceptually on attached Drawing E1.1.



SUMMARY

Based on aquifer characteristics evaluated from field observations and laboratory grain size analysis, Main-Land selected representative values to model groundwater mounding and transmissivity beneath the proposed replacement engineered leachfield. Groundwater mounding is anticipated to meet the minimum 1-foot vertical separation from the proposed base of leachfield, and our review of transmissivity characteristics indicates that effluent will not surface within 50 feet downgradient of the leachfield.

Please do not hesitate to contact Main-Land if we can provide additional information relevant to mounding and transmissivity for the proposed engineered leachfield.

Sincerely,

Main-Land Development Consultants, Inc.



Scott R. Dixon, P.E., C.G., L.S.E.
Senior Chief Environmental Scientist

Attachments: Attachment A. Grain Size Analysis for TP-3 sample of native ablation glacial till
and Kozeny-Carmen Hydraulic Conductivity Estimate

Attachment B. Mounding Results

REFERENCES

Department of Health and Human Services, et al., *State of Maine Subsurface Wastewater Disposal Rules*, 1-144, Chapter 241 (Effective Date 9/23/23).

Domenico, P., and Schwartz, F., *Physical and Chemical Hydrogeology*, John Wiley & Sons, 1990, page 118.



ATTACHMENT A

Grain Size Analysis for test pit sample of native ablation glacial till
and Kozeny-Carmen Hydraulic Conductivity Estimate



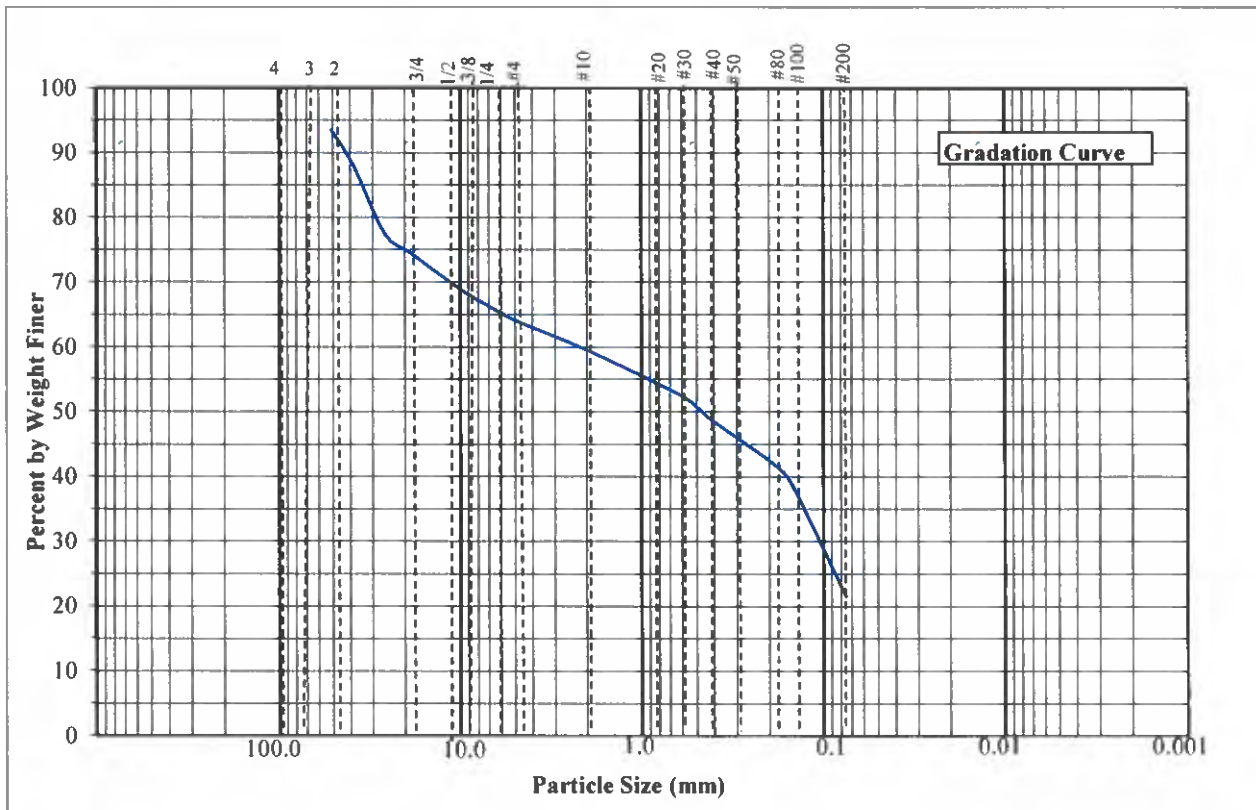
GRAIN SIZE ANALYSIS - ASTM D422

PROJECT NAME: Windham Eng. System
CLIENT: DM Roma
M-L SOIL DES:
SOURCE: TP-3, 2'-3'
DATE: September 3, 2025

PROJECT #: 25-320
MAIN LAND SAMPLE N/A
INTENDED USE: Gradation
SPECIFICATION: N/A
TECHNICIAN: TLB

DATA

<u>PARTICLE SIZE mm</u>	<u>% BY WT FINER</u>	<u>STRUCTURAL FILL SPECIFICATION</u>	<u>COMMENTS</u>
50.80 (2 in)	93.6	N/A	N/A
38.10 (1-1/2 in)	88		
25.40 (1 in)	77.3		
19.05 (3/4 in)	74.8		
12.70 (1/2 in)	71.1		
9.53 (3/8 in)	68.6		
6.35 (1/4 in)	65.7		
4.75 (No. 4)	63.9		
2.00 (No. 10)	59.6		
0.60 (No. 30)	52.5		
0.43 (No. 40)	49.2		
0.30 (No. 50)	46.1		
0.18 (No. 80)	41.6		
0.15 (No. 100)	39.1		
0.075 (No. 200)	21.6		



REMARKS:

Reviewed Scott R. Dixon, P.E.
Date 9/3/25

For TP3 at Webb Rd./Windham

Sieve Sizes		
Sieve size I.S. Standar	D _{ave}	
metric Sieve No.	cm	
10	4	
7.5	3	8.407395
5	2	5.880468
3.75	1.5	4.206612
2.5	1	2.942273
1.9	3/4	2.121418
1.25	1/2	1.480055
0.95	3/8	1.061444
0.63	1/4	0.74406
0.475	#4	0.532803
0.2	#10	0.284117
0.085	#20	0.120398
0.0425	#40	0.056413
0.018	#80	0.025572
0.0106	#140	0.013188
0.0075	#200	0.008667
0.00325	hyd #1	0.004582
0.00207	Hyd#2	0.002499
0.0012	Hyd#3	0.001506
0.00085	hyd#4	0.000984
0.0006	hyd#5	0.000696
0.0003	hyd#6	0.0004
0.00012	hyd#7	0.000175

Gradation Results

% Pass	Fi	Fi/D _{ave}
100		
100	0	0
93.6	6.4	1.088349
88	5.6	1.331237
77.3	10.7	3.636644
74.8	2.5	1.178457
71.1	3.7	2.499907
68.6	2.5	2.355281
65.7	2.9	3.897535
63.9	1.8	3.378362
59.6	4.3	15.13462
54.5	5.1	42.3594
49.2	5.3	93.95052
42	7.2	281.5634
29	13	985.7261
21.6	7.4	853.7814
0	21.6	4713.662
	0	0
	0	0
	0	0
	0	0
	0	0
0	21.6	3272.872

D_o est (cm)

0.006

Sum= 10278.41

porosity, n= 0.39

void ratio, e= 0.639344

Shape Factor	
Shape	SF
Spherical	6
Rounded	6.1
Worn	6.4
Sharp	7.4
Angular	7.7

k=	0.008325 cm/sec	k=	23.59703 feet/day
k=	0.008054 cm/sec	k=	22.8297 feet/day
k=	0.007316 cm/sec	k=	20.73958 feet/day
k=	0.005473 cm/sec	k=	15.51302 feet/day
k=	0.005055 cm/sec	k=	14.32776 feet/day

use 20 ft/day

Backfill K at Webb Rd./Windham

Sieve Sizes		
Sieve size I.S. Standar		D _{avg}
metric Sieve No.		cm
10	4	
7.5	3	8.407395
5	2	5.880468
3.75	1.5	4.206612
2.5	1	2.942273
1.9	3/4	2.121418
1.25	1/2	1.480055
0.95	3/8	1.061444
0.63	1/4	0.74406
0.475	#4	0.532803
0.2	#10	0.284117
0.085	#20	0.120398
0.0425	#40	0.056413
0.018	#80	0.025572
0.0106	#140	0.013188
0.0075	#200	0.008667
0.00325	hyd #1	0.004582
0.00207	Hyd#2	0.002499
0.0012	Hyd#3	0.001506
0.00085	hyd#4	0.000984
0.0006	hyd#5	0.000696
0.0003	hyd#6	0.0004
0.00012	hyd#7	0.000175

Gradation Results

% Pass	Fi	Fi/D _{avg}
100		
100	0	0
100	0	0
98	2	0.475442
96	2	0.679747
95	1	0.471383
94	1	0.67565
92	2	1.884225
89	3	4.031933
87	2	3.753736
75	12	42.23614
55	20	166.1153
29	26	460.8894
13	16	625.6965
7	6	454.9505
5	2	230.7517
0	5	1091.125
	0	0
	0	0
	0	0
	0	0
	0	0
0	5	1144.348

D_o est (cm)
0.003

Sum= 4228.085
porosity, n= 0.38
void ratio, e= 0.612903

Shape Factor	
Shape	SF
Spherical	6
Rounded	6.1
Worn	6.4
Sharp	7.4
Angular	7.7

k=	0.044051 cm/sec	k=	124.8693 feet/day
k=	0.042619 cm/sec	k=	120.8087 feet/day
k=	0.038717 cm/sec	k=	109.7484 feet/day
k=	0.02896 cm/sec	k=	82.09082 feet/day
k=	0.026747 cm/sec	k=	75.81874 feet/day

use 110 ft/day

(used 60 ft/d in
K_{composite})

ATTACHMENT B

Mounding Results



This spreadsheet will calculate the height of a groundwater mound beneath a stormwater infiltration basin. More information can be found in the U.S. Geological Survey Scientific Investigations Report 2010-5102 "Simulation of groundwater mounding beneath hypothetical stormwater infiltration basins".

The user must specify infiltration rate (R), specific yield (Sy), horizontal hydraulic conductivity (Kh), basin dimensions (x, y), duration of infiltration period (t), and the initial thickness of the saturated zone (hi(0)). height of the water table if the bottom of the aquifer is the datum). For a square basin the half width equals the half length (x = y). For a rectangular basin, if the user wants the water-table changes perpendicular to the long side, specify x as the short dimension and y as the long dimension. Conversely, if the user wants the values perpendicular to the short side, specify y as the short dimension, x as the long dimension. All distances are from the center of the basin. Users can change the distances from the center of the basin at which water-table aquifer thickness are calculated.

Cells highlighted in yellow are values that can be changed by the user. Cells highlighted in red are output values based on user-specified inputs. **The user MUST click the blue "Re-Calculate Now" button each time ANY of the user specified inputs are changed** otherwise necessary iterations to converge on the correct solution will not be done and values shown will be incorrect. Use consistent units for all input values (for example, feet and days)

Input Values

R	0.2010
Sy	0.250
K	35.00
x	20.000
y	28.000
t	365.000
hi(0)	0.500

h(max)

3.25

Δh(max)

3.25

Ground-water Mounding, in feet

Distance from center of basin in x direction, in feet

Recharge (infiltration) rate (feet/day)

Specific yield, Sy (dimensionless, between 0 and 1)

Horizontal hydraulic conductivity, Kh (feet/day)*

1/2 length of basin (x direction, in feet)

1/2 width of basin (y direction, in feet)

duration of infiltration period (days)

initial thickness of saturated zone (feet)

maximum thickness of saturated zone (beneath center of basin at end of infiltration period)

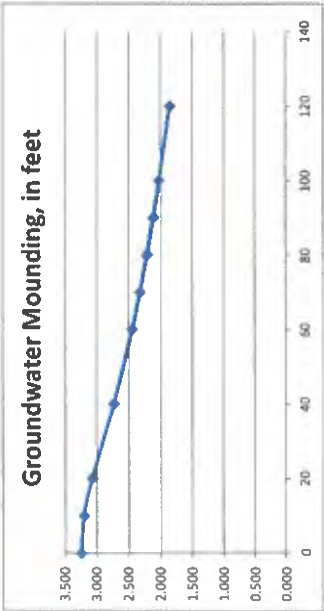
maximum groundwater mounding (beneath center of basin at end of infiltration period)

Conversion Table

inch/hour	0.67	feet/day	1.33
hours	2.00	days	4.00
36		1.50	hydraulic conductivity (ft/d).

In the report accompanying this spreadsheet (USGS SIR 2010-5102), vertical soil permeability (ft/d) is assumed to be one-tenth horizontal

Re-Calculate Now



Disclaimer

This spreadsheet solving the Hantush (1967) equation for ground-water mounding beneath an infiltration basin is made available to the general public as a convenience for those wishing to replicate values documented in the USGS Scientific Investigations Report 2010-5102 "Groundwater mounding beneath hypothetical stormwater infiltration basins" or to calculate values based on user-specified site conditions. Any changes made to the spreadsheet (other than values identified as user-specified) after transmission from the USGS could have unintended, undesirable consequences. These consequences could include, but may not be limited to: erroneous output, numerical instabilities, and violations of underlying assumptions that are inherent in results presented in the accompanying USGS published report. The USGS assumes no responsibility for the consequences of any changes made to the spreadsheet. If changes are made to the spreadsheet, the user is responsible for documenting the changes and justifying the results and conclusions.

EXHIBIT D

HHE 200 Form



UNSUBSURFACE WASTEWATER DISPOSAL

Maine Dept. Health & Human Services
Div. Environmental Health, 115115
207) 287-2070 Fax (207) 287-4172

PROPERTY LOCATION

>> CAUTION: LPI APPROVAL REQUIRED <<

City, Town, or Plantation	Windham, Maine
Street or Road	Webb Road
Subdivision, Lot #	"Webb Road Property"
OWNER/APPLICANT INFORMATION	
Name (last, first, MI)	Robbie Holdings, LLC
Mailing Address of Owner/Applicant	P.O. Box 1508 Windham, ME 04062
Daytime Tel. #	40 DM Roma Engineers 207-591-5055

Town/City	Permit #	
Date Permit Issued	Fee: \$	Double Fee Charged ☐
Local Plumbing Inspector Signature		
Fee: \$	state min fee \$	Locally adopted fee
Copy: ☐ Owner ☐ Town ☐ State		
The Subsurface Wastewater Disposal System shall not be installed until a Permit is issued by the Local Plumbing Inspector. The Permit shall authorize the owner or installer to install the disposal system in accordance with this application and the Maine Subsurface Wastewater Disposal Rules		
Municipal Tax Map #	Lot #	

I state and acknowledge that the information submitted is correct to the best of my knowledge and understand that any falsification is reason for the Department and/or Local Plumbing Inspector to deny a permit.

Agent 7-10-2026

Signature of Owner or Applicant

CAUTION: INSPECTION REQUIRED

I have inspected the installation authorized above and found it to be in compliance with the Subsurface Wastewater Disposal Rules Application.

(1st) date approved

(2nd) date approved

PERMIT INFORMATION

TYPE OF APPLICATION	THIS APPLICATION REQUIRES
☒ 1. First Time System	☒ 1. No Rule Variance
☐ 2. Replacement System	☐ 2. First Time System Variance
Type replaced:	☐ a. Local Plumbing Inspector Approval
Year installed	☐ b. State & Local Plumbing Inspector Approval
☐ 3. Expanded System	☐ 3. Replacement System Variance
☐ a. <25% Expansion	☐ a. Local Plumbing Inspector Approval
☐ b. ≥25% Expansion	☐ b. State & Local Plumbing Inspector Approval
☐ 4. Experimental System	☐ 4. Minimum Lot Size Variance
☐ 5. Seasonal Conversion	☐ 5. Seasonal Conversion Permit
SIZE OF PROPERTY	DISPOSAL SYSTEM TO SERVE
21.4±	☐ 1. Single Family Dwelling Unit, No. of Bedrooms:
☐ SQ. FT.	☐ 2. Multiple Family Dwelling, No. of Units.
☒ ACRES	☒ 3. Other: Multiple Dwellings - 75 BR total
SHORELAND ZONING	(specify)
☐ Yes	Current Use ☐ Seasonal ☐ Year Round ☒ Undeveloped
☒ No	

DISPOSAL SYSTEM COMPONENTS

- ☐ 1. Complete Non-engineered System
- ☐ 2. Primitive System (graywater & alt. toilet)
- ☐ 3. Alternative Toilet, specify:
- ☐ 4. Non-engineered Treatment Tank (only)
- ☐ 5. Holding Tank, gallons
- ☐ 6. Non-engineered Disposal Field (only)
- ☐ 7. Separated Laundry System
- ☒ 8. Complete Engineered System (2000 gpd or more)
- ☐ 9. Engineered Treatment Tank (only)
- ☐ 10. Engineered Disposal Field (only)
- ☒ 11. Pre-treatment, specify: (5) Fujiclean CEN 14ATUs
- ☐ 12. Miscellaneous Components

TYPE OF WATER SUPPLY

- ☐ 1. Drilled Well
- ☐ 2. Dug Well
- ☐ 3. Private
- ☒ 4. Public
- ☐ 5. Other

DESIGN DETAILS (SYSTEM LAYOUT SHOWN ON PAGE 3)

TREATMENT TANK	DISPOSAL FIELD TYPE & SIZE	GARBAGE DISPOSAL UNIT	DESIGN FLOW
☒ 1. Concrete	☐ 1. Stone Bed ☐ 2. Stone Trench	☐ 1. No ☐ 2. Yes ☒ 3. Maybe	6,750 gallons per day *
☐ a. Regular	☒ 3. Proprietary Device	If Yes or Maybe, specify one below:	BASED ON:
☐ b. Low Profile	☒ a. cluster array ☐ c. Linear	☐ a. multi-compartment tank	☒ 1. Table 5A (dwelling unit(s))
☐ 2. Plastic	☒ b. regular load ☐ d. H-20 load	☐ b. tanks in series	☐ 2. Table 5C (other facilities)
☒ 3. Others: See Dr. E.J.I.	☐ 4. Other:	☐ c. increase in tank capacity	SHOW CALCULATIONS for other facilities
CAPACITY 7,000 GAL	SIZE: sq. ft. lin. ft.	☐ d. Filter on Tank Outlet	* 75 BR x 90 gpd/BR = 6,750 gpd
* 1-day retention time	DISPOSAL FIELD SIZING	EFFLUENT/EJECTOR PUMP	☐ 3. Section 5G (meter readings)
SOIL DATA & DESIGN CLASS	☒ 1. Medium---2.6 sq. ft. / gpd	☐ 1. Not Required	ATTACH WATER METER DATA
PROFILE CONDITION	☐ 2. Medium---Large 3.3 sq. ft. / gpd	☐ 2. May Be Required	LATITUDE AND LONGITUDE
4 / C	☐ 3. Large---4.1 sq. ft. / gpd	☒ 3. Required	at center of disposal area
a) Observation Hole # TP-6	☐ 4. Extra Large---5.0 sq. ft. / gpd	Specify only for engineered systems	Lat. 43° d 45' m 37.52" N
Depth varies		DOSE gallons	Lon. 70° d 25' m 16.02" W
of Most Limiting Soil Factor			if g.p.s. state margin of error.

SITE EVALUATOR STATEMENT

I certify that on 8/27/25 (date) I completed a site evaluation on this property and state that the data reported are accurate and that the proposed system is in compliance with the State of Maine Subsurface Wastewater Disposal Rules (10-144A CMR 241)

Site Evaluator Signature: Scott R. Dixon

Site Evaluator Name Printed: Scott R. Dixon

SE #: 406

Date: 7/13/26

Telephone Number: 207-877-6752

E-mail Address: scott@main-landdci.com

Note: Changes to or deviations from the design shall be confirmed with the Site Evaluator.

Department of Health & Human Services
Division of Environmental Health
(207) 287-5672 Fax: (207) 287-3165

Owner's Name

Webb Road

Robie Holdings, LLC

Scale 1" = _____ ft. or as shown

NSITE LOCATION PLAN

See Drawing E1.1 attached
for Site Plan

Site location plan showing the intersection of Rt. 4/202 and Webb Rd. A dashed line indicates the location of the 'SITE'.

Observation Hole TP-1 ☒ Test Pit ☐ Boring
3 " Depth of Organic Horizon Above Mineral Soil

Ex. Grade 3 E. 236

Hand-drawn soil profile diagram showing depth (0 to 50 inches) and soil characteristics (Texture, Consistency, Color, Mottling). The profile shows a topsoil layer (0-10 inches) with loamy sand and gravel, friable consistency, brown and strong brown color, and no mottling. A subsoil layer (10-36 inches) is labeled 'weathered/fractured rock' with reduced mottling. Harder bedrock is noted at 36 inches.

Depth Below Mineral Soil Surface (inches)	Texture	Consistency	Color	Mottling
0 - 10	Loamy Sand, with angular gravel	Friable	Brown and strong brown	None
10 - 36			Light brown	Reduced
36	Harder bedrock at 36"			

Observation Hole TP-2 ☒ Test Pit ☐ Boring
3 " Depth of Organic Horizon Above Mineral Soil

Texture	Consistency	Color	Mottling

Hand-drawn soil profile diagram showing depth (0 to 50 inches) and soil characteristics (Texture, Consistency, Color, Moisture). The profile shows loamy sand with angular gravel in the top 30 inches, followed by weathered/fractured rock, and harder bedrock at 40 inches.

Depth Below Mineral Soil Surface (inches)	Texture	Consistency	Color	Moisture
0	Loamy sand, with angular gravel	Friable	Brown	None
10			Light brown	
20				
30	Weathered/fractured rock			
40	Harder bedrock at 40"			
50				

Soil Classification	Slope	Limiting Factor	☒ Ground Water
<u>4C</u> <u>AIII</u>	<u>4-6</u> %	<u>30</u> "	☐ Restrictive Layer
Profile Condition			☐ Bedrock
			☐ Pit Depth

Soil Classification	Slope	Limiting Factor	☒ Ground Water
4C AIII	3-5 %		☐ Restrictive Layer
Profile Condition		36 "	☐ Bedrock
			☐ Pit Depth

Site Evaluator Signature

4060

7/13/26

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SUBSURFACE WASTEWATER DISPOSAL SYSTEM APPLICATION

Maine Dept. Health & Human Services
Division of Environmental Health
(207) 287-5672 Fax: (207) 287-3165

Town, City, Plantation

Windham, ME

Street, Road, Subdivision

Webb Road

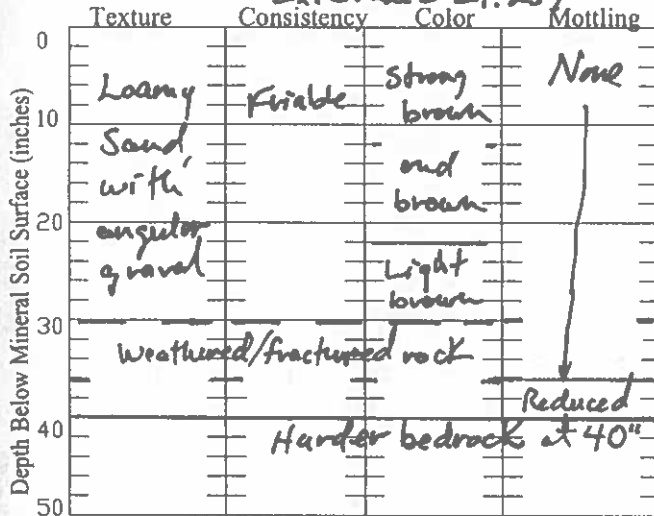
Owner's Name

Robie Holdings, LLC

SOIL DESCRIPTION AND CLASSIFICATION (Location of Observation Holes Shown Above)

Observation Hole TP-3 ☒ Test Pit ☐ Boring
" Depth of Organic Horizon Above Mineral Soil

Ex. Grade El. 237'



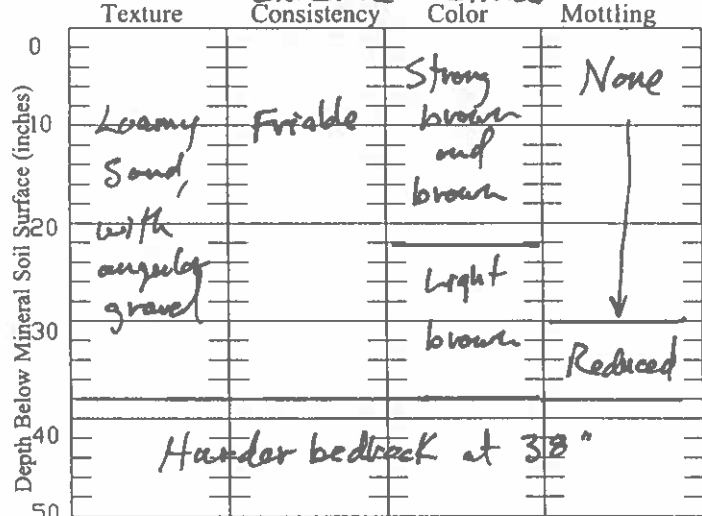
Soil Classification
4C AIII
Profile Condition

Slope
3-5 %

Limiting Factor
36 "
☒ Ground Water
☐ Restrictive Layer
☐ Bedrock
☐ Pit Depth

Observation Hole TP-4 ☒ Test Pit ☐ Boring
" Depth of Organic Horizon Above Mineral Soil

Ex. Grade El. 236'



Soil Classification
4C AIII
Profile Condition

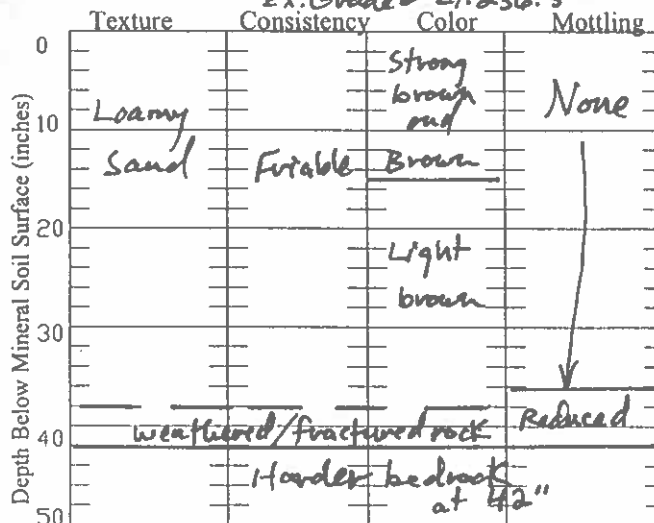
Slope
2-4 %

Limiting Factor
30 "
☒ Ground Water
☐ Restrictive Layer
☐ Bedrock
☐ Pit Depth

SOIL DESCRIPTION AND CLASSIFICATION (Location of Observation Holes Shown Above)

Observation Hole TP-5 ☒ Test Pit ☐ Boring
" Depth of Organic Horizon Above Mineral Soil

Ex. Grade El. 236.5'



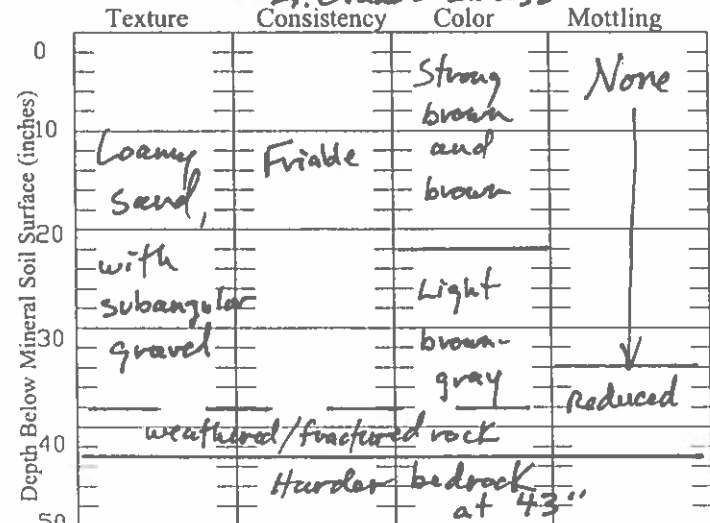
Soil Classification
4C AIII
Profile Condition

Slope
3-5 %

Limiting Factor
36 "
☒ Ground Water
☐ Restrictive Layer
☐ Bedrock
☐ Pit Depth

Observation Hole TP-6 ☒ Test Pit ☐ Boring
" Depth of Organic Horizon Above Mineral Soil

Ex. Grade El. 238'



Soil Classification
4C AIII
Profile Condition

Slope
4-6 %

Limiting Factor
34 "
☒ Ground Water
☐ Restrictive Layer
☐ Bedrock
☐ Pit Depth

Scott R. D.

Site Evaluator Signature

406

SF #

7/13/24

Date

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HHE-200 Rev. 05/08

SUBSURFACE WASTEWATER DISPOSAL SYSTEM APPLICATION

Maine Dept. Health & Human Services
Division of Environmental Health
(207) 287-5672 Fax: (207) 287-3165

Town, City, Plantation

Windham, ME

Street, Road, Subdivision

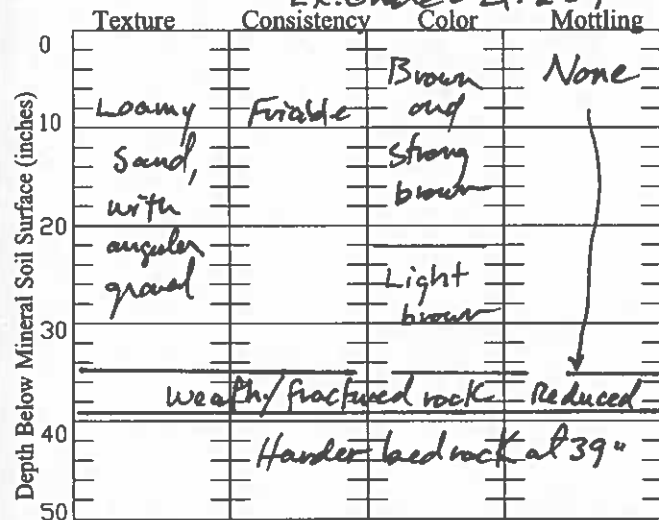
Webb Road

Owner's Name

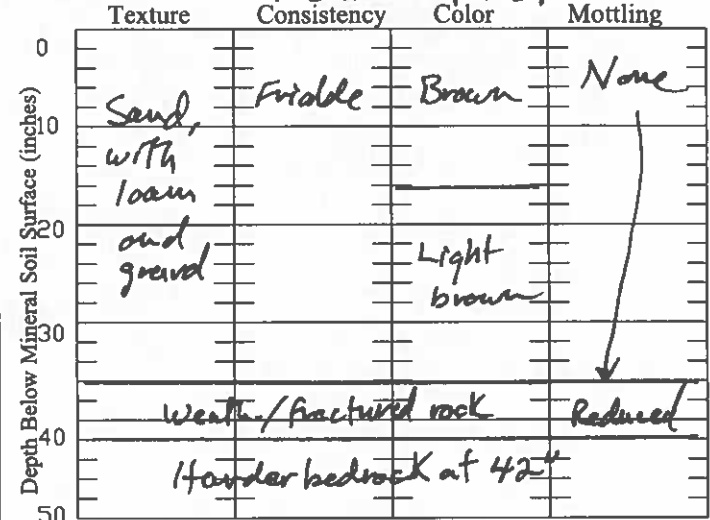
Robie Holdings, LLC

SOIL DESCRIPTION AND CLASSIFICATION (Location of Observation Holes Shown Above)

Observation Hole TP-7 ☒ Test Pit ☐ Boring
3 " Depth of Organic Horizon Above Mineral Soil
Ex. Grade El. 237



Observation Hole TP-8 ☒ Test Pit ☐ Boring
2 " Depth of Organic Horizon Above Mineral Soil
Ex. Grade El. 237

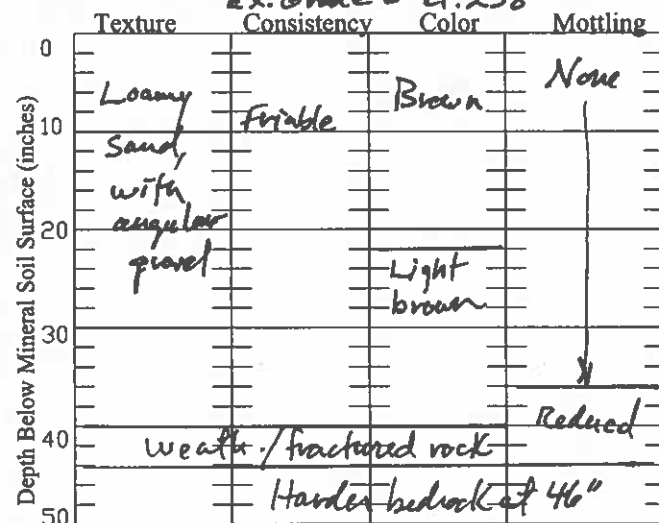


Soil Classification: 4C ATII
Profile Condition
Slope: 3-5 %
Limiting Factor: 35 "
☒ Ground Water
☐ Restrictive Layer
☐ Bedrock
☐ Pit Depth

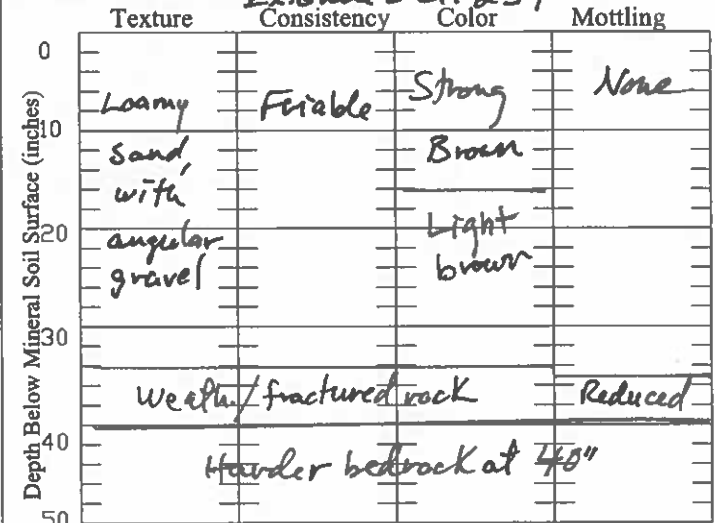
Soil Classification: 4C ATII
Profile Condition
Slope: 4-6 %
Limiting Factor: 36 "
☐ Ground Water
☐ Restrictive Layer
☐ Bedrock
☐ Pit Depth

SOIL DESCRIPTION AND CLASSIFICATION (Location of Observation Holes Shown Above)

Observation Hole TP-9 ☒ Test Pit ☐ Boring
3 " Depth of Organic Horizon Above Mineral Soil
Ex. Grade El. 238



Observation Hole TP-10 ☒ Test Pit ☐ Boring
3 " Depth of Organic Horizon Above Mineral Soil
Ex. Grade El. 237



Soil Classification: 4C ATII
Profile Condition
Slope: 3-5 %
Limiting Factor: 36 "
☒ Ground Water
☐ Restrictive Layer
☐ Bedrock
☐ Pit Depth

Soil Classification: 4C ATII
Profile Condition
Slope: 3-5 %
Limiting Factor: 35 "
☒ Ground Water
☐ Restrictive Layer
☐ Bedrock
☐ Pit Depth

7/13/26

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Site Evaluator Signature

SE #

Date

SUBSURFACE WASTEWATER DISPOSAL SYSTEM APPLICATION

Department of Health & Human Services
Division of Environmental Health
(207) 287-5672 Fax: (207) 287-3165

Town, City, Plantation

Windham, ME

Street, Road, Subdivision

Webb Road

Owner's Name

Robie Holdings, LLC

SUBSURFACE WASTEWATER DISPOSAL PLAN

SCALE: 1" = _____ FT.

See Drawing E1.1 attached
for Disposal Plan

FILL REQUIREMENTS

Depth of Fill (Upslope) _____

Depth of Fill (Downslope) _____

CONSTRUCTION ELEVATIONS

(SEE DRAWING E1.1)
Finished Grade Elevation _____

Top of Distribution Pipe or Proprietary Device _____

Bottom of Disposal Area _____

ELEVATION REFERENCE POINT

Location & Description: _____

Reference Elevation: _____

DISPOSAL AREA CROSS SECTION

Scale

Horizontal 1" = _____ ft.

Vertical 1" = _____ ft.

See Drawing E1.1 attached
for Cross Section

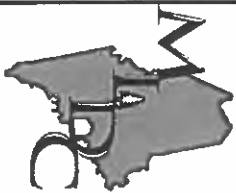

Site Evaluator Signature

406

SE #

7/13/26

Date



MAIN-LAND
DEVELOPMENT
CONSULTANTS, INC.

69 MAIN ST. LINTHROP, PA 15460
152 MAIN ST. LINTHROP, PA 15460
TEL: (717) 877-4321 FAX: (717) 877-5404
WWW.MAINLANDDC.COM

**ENGINEERED
WASTEWATER
DISPOSAL SYSTEM**

OWNER OF RECORD
WEBB ROAD
METHUEN, ME

**ROBIE HOLDINGS,
LLC**

MADE FOR
**D.M. ROMA
CONSULTING
ENGINEERS**
PO BOX 116
METHUEN, ME 04062

DRAWING SCALE:
VARIES

SUBMISSION NOTES:
SUBMISSION 1: 2006-07-13 ERL
THIS SUBMISSION IS FOR
APPLICATION

ROLL USE:
DRAWN BY: DMR/MS
CHECKED BY: SRO
SUBMISSION DATE: 2006-07-13
SUBMITTED FOR: APPLICATION

NOT FOR CONSTRUCTION
**WASTEWATER
DISPOSAL
DESIGN**

SCALE:

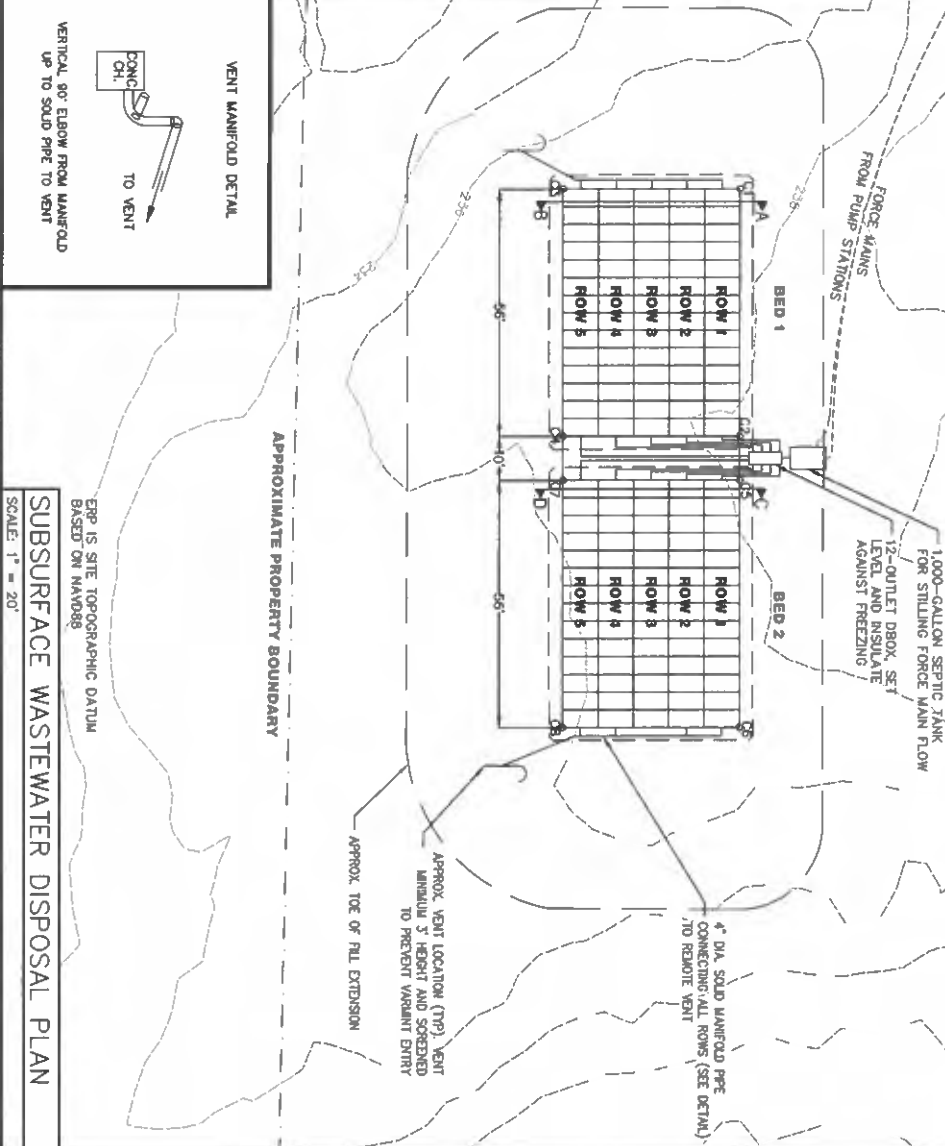


E1.1

DATE: 06-25-2006

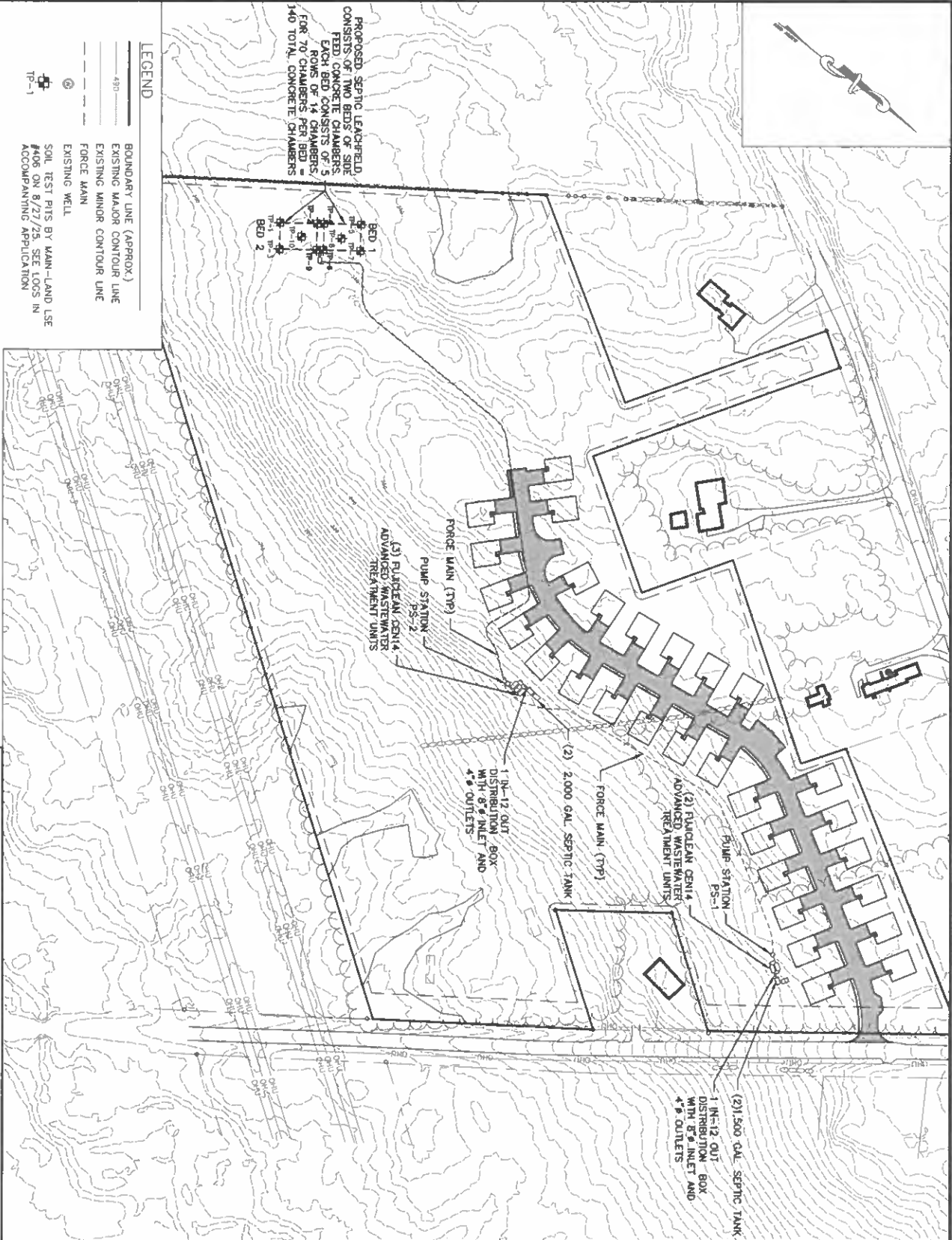
BED 1 EXISTING GRADE ELEVATIONS AT CORNERS	
C1	237.0
C2	238.0
C3	236.0
C4	226.5

BED 2 EXISTING GRADE ELEVATIONS AT CORNERS	
C5	238.0
C6	237.0
C7	236.0
C8	236.0

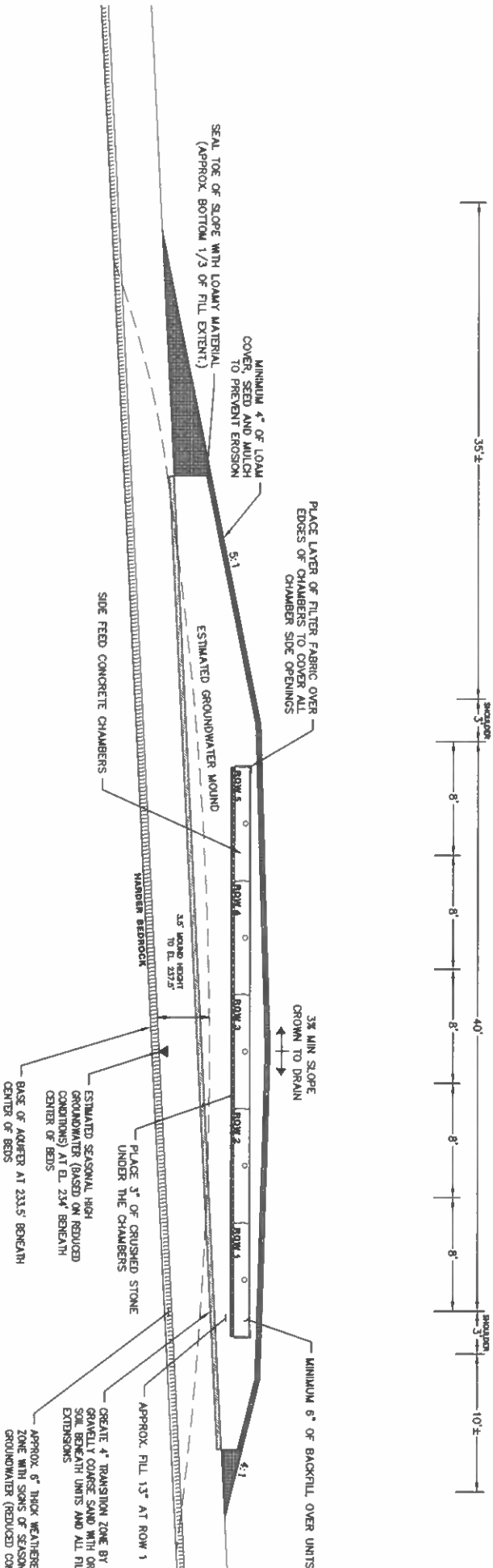


SUBSURFACE WASTEWATER DISPOSAL PLAN
SCALE: 1" = 20'

SITE PLAN
SCALE: 1" = 100'



- LEGEND**
- BOUNDARY LINE (APPROX.)
 - EXISTING MAJOR CONTOUR LINE
 - EXISTING MINOR CONTOUR LINE
 - FORCE MAIN
 - EXISTING WELL
 - SOIL TEST PITS BY MAIN-LAND LSE #406 ON 8/27/25. SEE LOGS IN ACCOMPANYING APPLICATION
 - TP-1



**NOTE: CROSS-SECTION
DEPICTS BOTH
BEDS 1 AND 2**

EXISTING ELEVATIONS (BOTH BEDS)	
FINAL GRADE	241.2± (AT ROW 3)
TOP OF CHAMBER	240.4'
BOTTOM OF CHAMBER	239.3'
BOTTOM OF STONE	239.0'
BOTTOM OF BACKFILL	VARIES. EXTENDS DOWN TO TRANSITION ZONE NEAR EXISTING GRADE

NOTE: BACKFILL MEANS GRAVELLY COARSE SAND

CROSS-SECTION (A-B AND C-D)
SCALE: 1" = 5'

EXHIBIT E

Operations and Maintenance Manual



OPERATIONS AND MAINTENANCE

ENGINEERED LEACHFIELD

Serving the Proposed Legacy Village Retirement Community
Webb Road, Windham, Maine

INTRODUCTION:

The proposed engineered leachfield for the proposed residential development is designed to dispose of a maximum of approximately 6,750 gallons per day of domestic wastewater. This wastewater is comprised of discharge from up to 75 bedrooms. The system includes 7,000 gallons of regular septic tanks and a Tertiary Advanced Treatment Unit (five Fujiclean CEN 14 units planned) for wastewater treatment prior to the leachfield.

OPERATION:

Operation of the system is the responsibility of the Project Owner.

The most important Operation item is ensuring that no unauthorized wastes enter the system. No harsh chemicals should be allowed into the system, particularly those chemicals that kill bacteria, such as chlorine, at high concentrations above those associated with normal household use. Cleaning products should be used in moderation and should be diluted when entering the system.

MAINTENANCE:

Maintenance of the system, including inspection and pumping of the individual septic tanks and the ATUs, is the responsibility of the Owner.

The septic system does require periodic maintenance. First, all water fixtures shall be kept in working order. Leaky toilets, showers, and sinks can overtax a septic system.

Second, the septic tanks should be inspected annually. Septic tanks should be cleaned when the sludge and scum occupies ***no more than one-third*** the tank liquid capacity, or once every two to three years, whichever comes first. Cleaning means the removal of all contents in the tanks.

Records of all tank pumping should be kept in the event an issue arises. Records should include volumes pumped and the frequency of the pumping.

The ATUs should be inspected per the Manufacturer's instructions. Records should include inspection results and results of water quality testing, when performed.

Third, the ground around the leachfield should also be inspected for wet spots, or for odors on an on-going basis. If odors or wet spots are apparent, the Design Engineer shall be contacted immediately.

The area for a distance of 30 feet around the leachfield should be inspected at least twice annually and woody vegetation in this area removed to prevent roots from growing into the system.

If, at any time, any portion of this system does not appear to be functioning as designed, notify the Design Engineer as soon as possible.

EXHIBIT F

Soil Logs



Department of Health & Human Services
Division of Environmental Health
(207) 287-5672 Fax: (207) 287-3165

Owner's Name
Robie Holdings, LLC

NSITE LOCATION PLAN

See Drawing E1.1 attached
for Site Plan

True

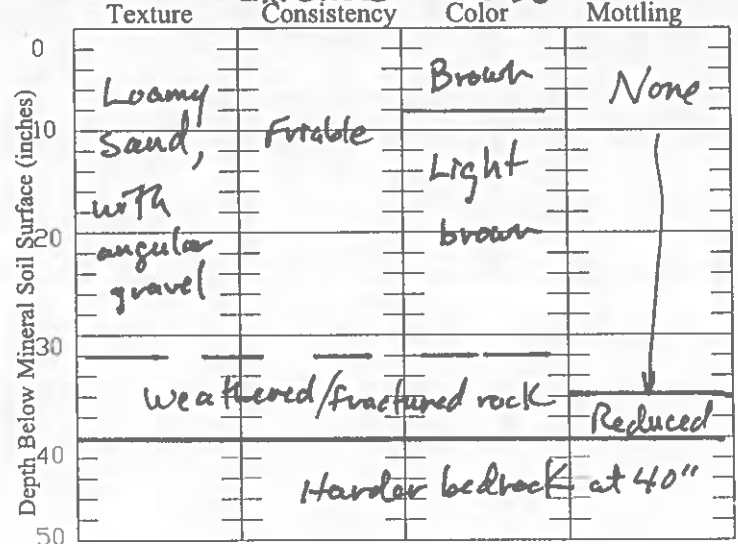
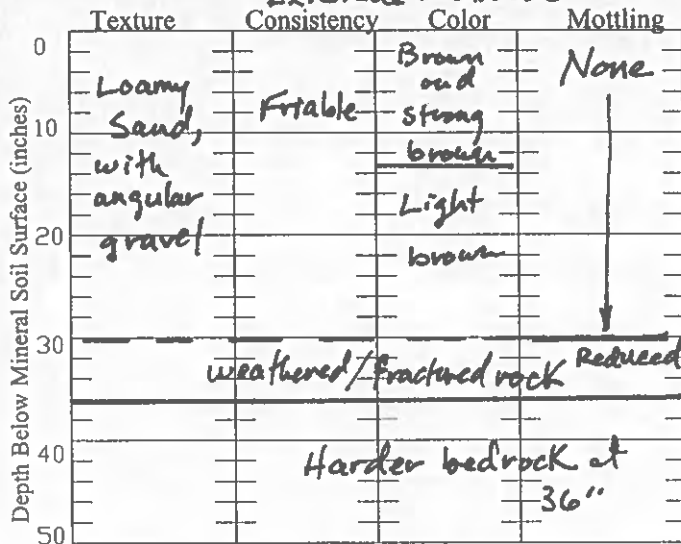
N

RT. 4/202

Webb Rd.

SITE

Observation Hole TP-2 ☒ Test Pit ☐ Boring
3 " Depth of Organic Horizon Above Mineral Soil
Ex. Grade El. 236'



Soil Classification	Slope	Limiting Factor	☒ Ground Water
<u>4C</u> <u>AIII</u>	<u>3-5</u> %	<u>36</u> "	☐ Restrictive Layer
Profile	Condition		☐ Bedrock
			☐ Pit Depth

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SUBSURFACE WASTEWATER DISPOSAL SYSTEM APPLICATION

Maine Dept. Health & Human Services
Division of Environmental Health
(207) 287-5672 Fax: (207) 287-3165

Town, City, Plantation

Windham, ME

Street, Road, Subdivision

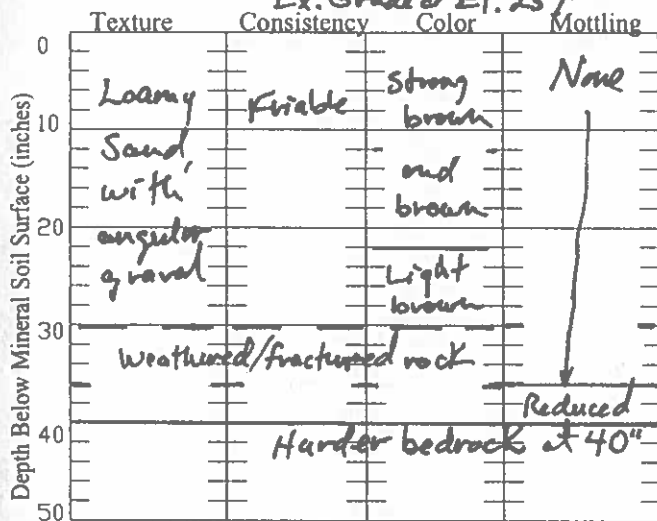
Webb Road

Owner's Name

Robie Holdings, LLC

SOIL DESCRIPTION AND CLASSIFICATION (Location of Observation Holes Shown Above)

Observation Hole TP-3 ☒ Test Pit ☐ Boring
" Depth of Organic Horizon Above Mineral Soil
Ex. Grade El. 237'



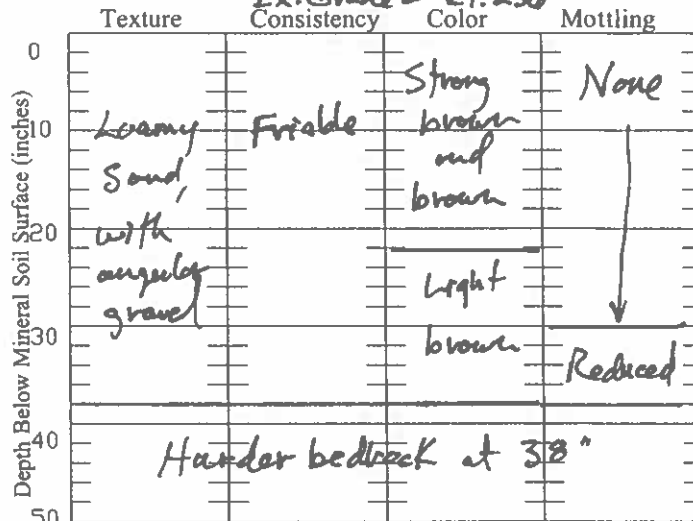
Soil Classification
4C AIII
Profile Condition

Slope
3-5 %

Limiting Factor
36 "

☒ Ground Water
☐ Restrictive Layer
☐ Bedrock
☐ Pit Depth

Observation Hole TP-4 ☒ Test Pit ☐ Boring
" Depth of Organic Horizon Above Mineral Soil
Ex. Grade El. 236'



Soil Classification
4C AIII
Profile Condition

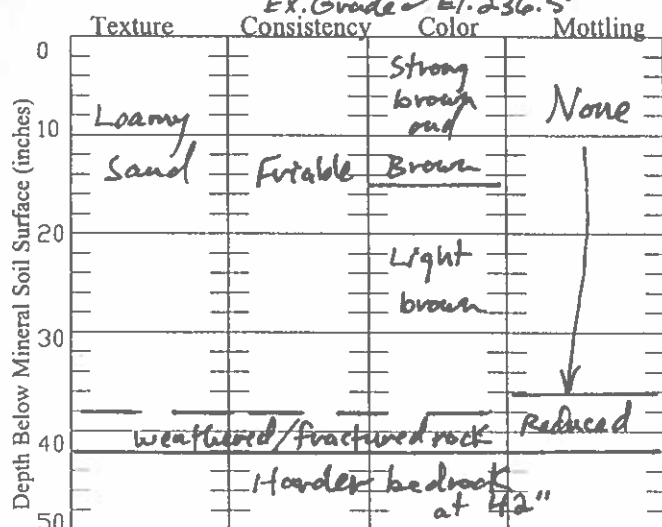
Slope
2-4 %

Limiting Factor
30 "

☒ Ground Water
☐ Restrictive Layer
☐ Bedrock
☐ Pit Depth

SOIL DESCRIPTION AND CLASSIFICATION (Location of Observation Holes Shown Above)

Observation Hole TP-5 ☒ Test Pit ☐ Boring
" Depth of Organic Horizon Above Mineral Soil
Ex. Grade El. 236.5'



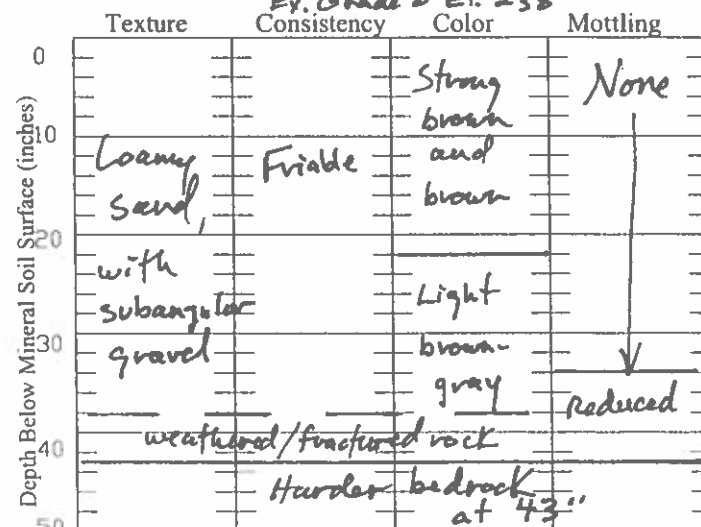
Soil Classification
4C AIII
Profile Condition

Slope
3-5 %

Limiting Factor
36 "

☒ Ground Water
☐ Restrictive Layer
☐ Bedrock
☐ Pit Depth

Observation Hole TP-6 ☒ Test Pit ☐ Boring
" Depth of Organic Horizon Above Mineral Soil
Ex. Grade El. 238'



Soil Classification
4C AIII
Profile Condition

Slope
4-6 %

Limiting Factor
34 "

☒ Ground Water
☐ Restrictive Layer
☐ Bedrock
☐ Pit Depth

Scott R. D.
Site Evaluator Signature

406

SE #

7/13/24

Date

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HHE-200 Rev. 05/08

SUBSURFACE WASTEWATER DISPOSAL SYSTEM APPLICATION

Maine Dept. Health & Human Services
Division of Environmental Health
(207) 287-5672 Fax: (207) 287-3165

Town, City, Plantation

Windham, ME

Street, Road, Subdivision

Webb Road

Owner's Name

Robie Holdings, LLC

SOIL DESCRIPTION AND CLASSIFICATION (Location of Observation Holes Shown Above)

Observation Hole TP-7 ☒ Test Pit ☐ Boring
3" Depth of Organic Horizon Above Mineral Soil
Ex. Grade 2 El. 237

Texture	Consistency	Color	Mottling
Loamy Sand, with angular gravel	Friable	Brown and strong brown	None
		Light brown	
		weath./fractured rock	Reduced
		Harder bedrock at 39"	

Observation Hole TP-8 ☒ Test Pit ☐ Boring
2" Depth of Organic Horizon Above Mineral Soil
Ex. Grade 2 El. 237

Texture	Consistency	Color	Mottling
Sand, with loam and gravel	Friable	Brown	None
		Light brown	
		weath./fractured rock	Reduced
		Harder bedrock at 42"	

Soil Classification 4C ATII Slope 3-5 % Limiting Factor 35"
Profile Condition

Soil Classification 4C ATII Slope 4-6 % Limiting Factor 36"
Profile Condition

SOIL DESCRIPTION AND CLASSIFICATION (Location of Observation Holes Shown Above)

Observation Hole TP-9 ☒ Test Pit ☐ Boring
3" Depth of Organic Horizon Above Mineral Soil
Ex. Grade 2 El. 238

Texture	Consistency	Color	Mottling
Loamy Sand, with angular gravel	Friable	Brown	None
		Light brown	
		weath./fractured rock	Reduced
		Harder bedrock at 46"	

Observation Hole TP-10 ☒ Test Pit ☐ Boring
3" Depth of Organic Horizon Above Mineral Soil
Ex. Grade 2 El. 237

Texture	Consistency	Color	Mottling
Loamy Sand, with angular gravel	Friable	Strong Brown	None
		Light brown	
		weath./fractured rock	Reduced
		Harder bedrock at 40"	

Soil Classification 4C ATII Slope 3-5 % Limiting Factor 36"
Profile Condition

Soil Classification 4C ATII Slope 3-5 % Limiting Factor 35"
Profile Condition

7/13/26

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Site Evaluator Signature

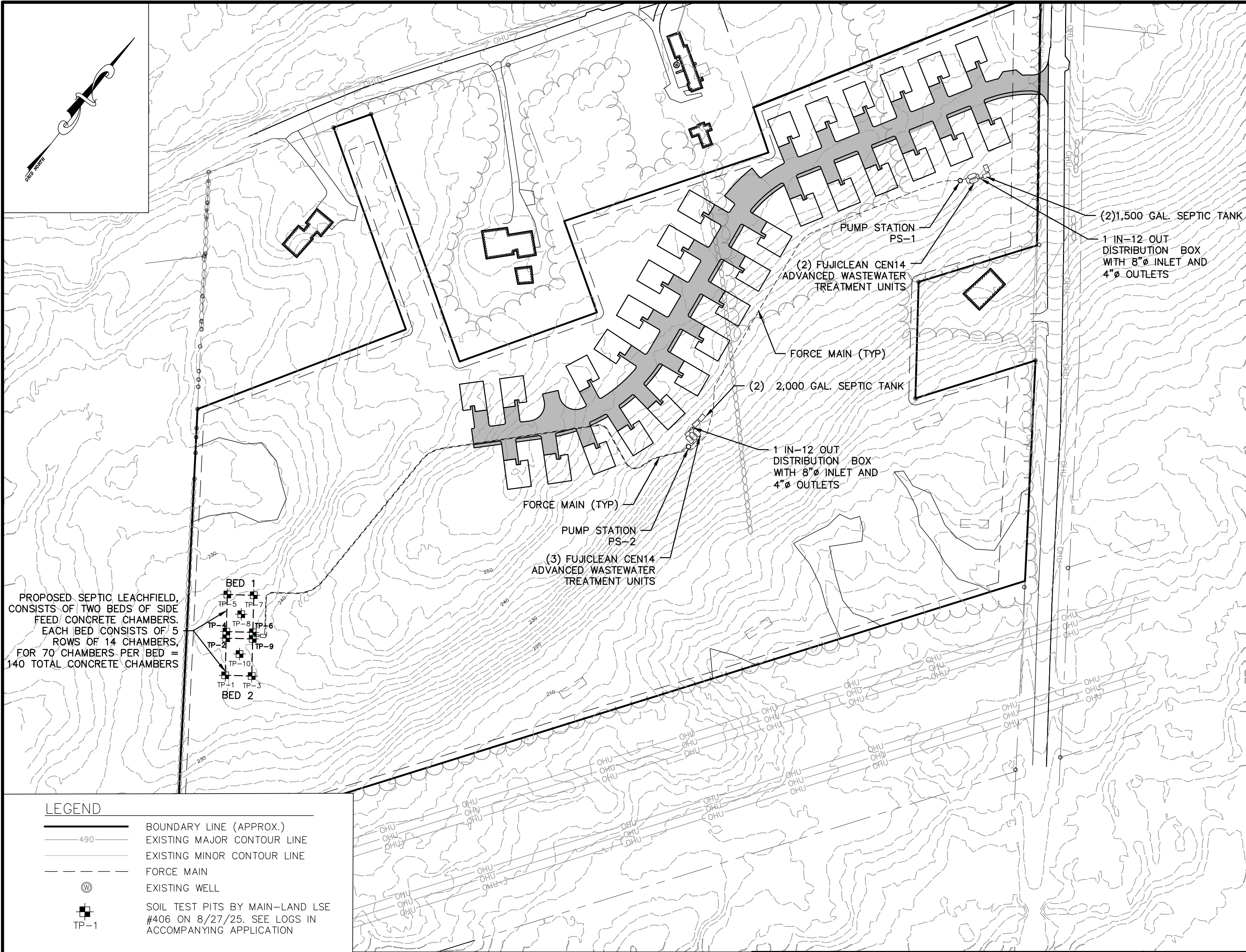
SE #

Date

EXHIBIT G

Design Plan





SITE PLAN

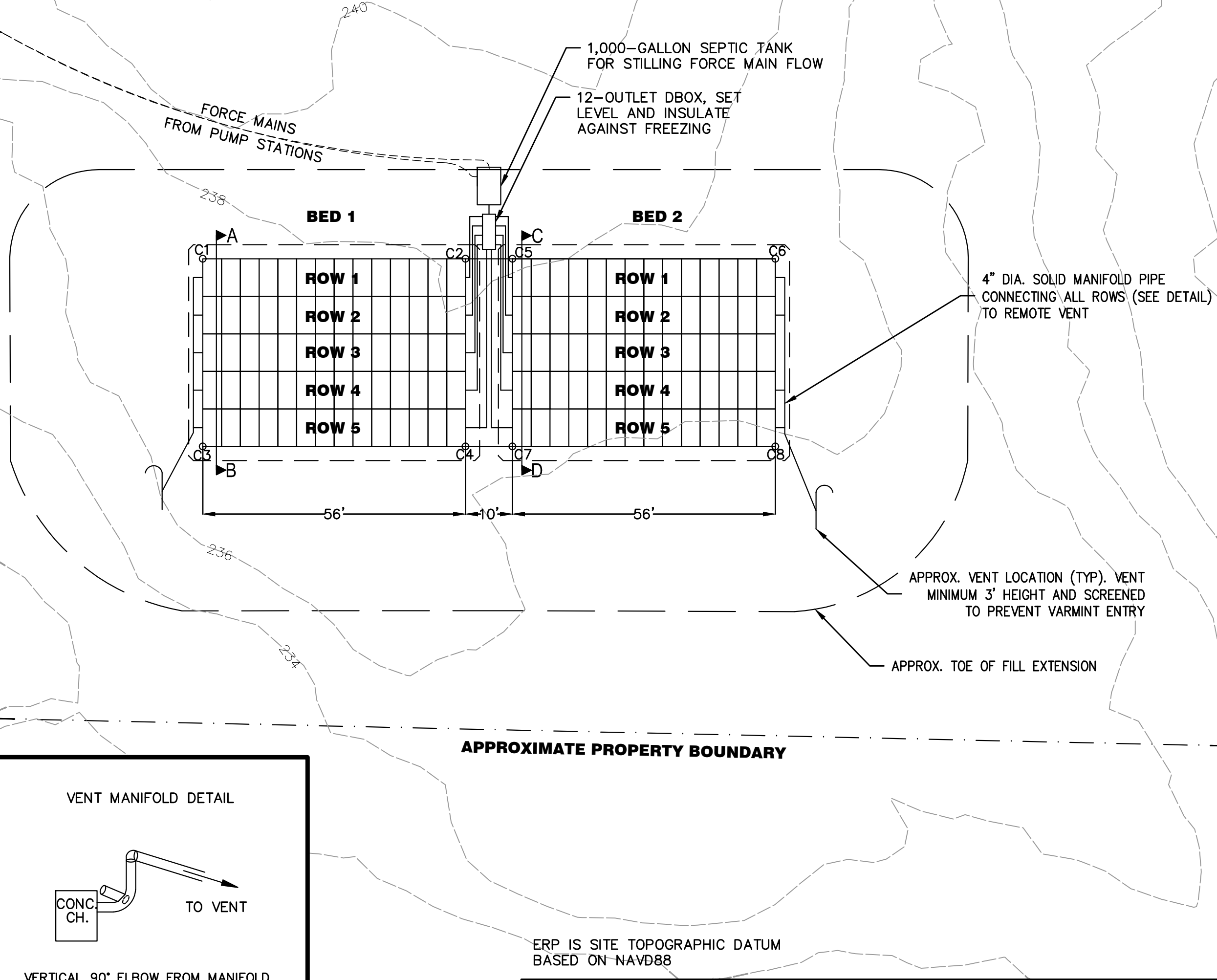
SCALE: 1" = 100'

BED 1 EXISTING GRADE ELEVATIONS AT CORNERS

C1	237.0
C2	238.0
C3	236.0
C4	236.5

BED 2 EXISTING GRADE ELEVATIONS AT CORNERS

C5	238.0
C6	237.0
C7	236.0
C8	236.0

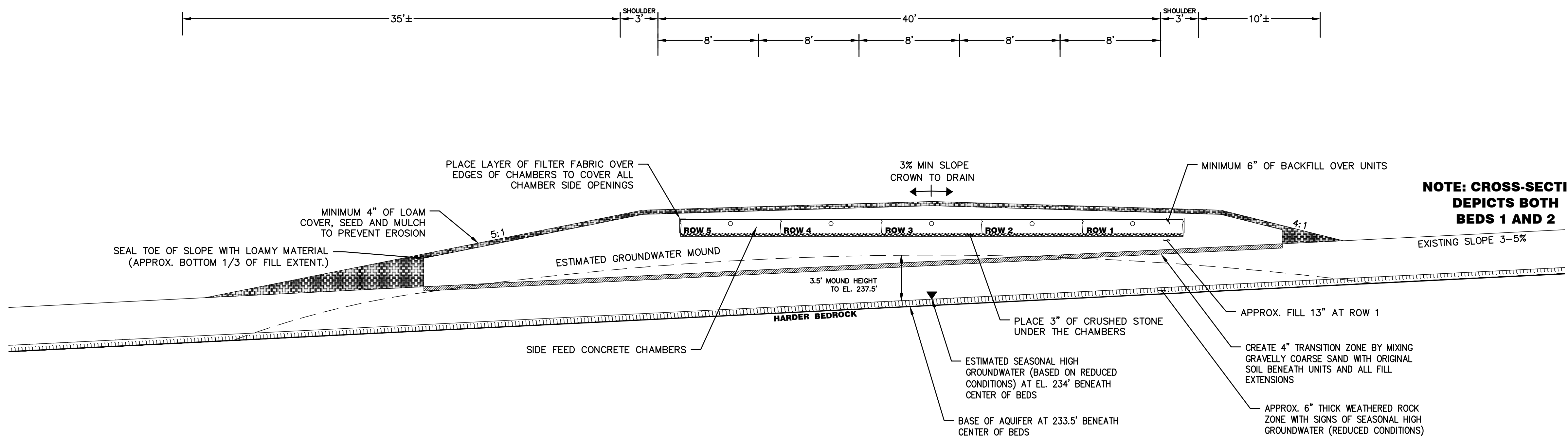


SUBSURFACE WASTEWATER DISPOSAL PLAN

SCALE: 1" = 20'

EXISTING ELEVATIONS (BOTH BEDS)

FINAL GRADE	241.2'±(AT ROW 3)
TOP OF CHAMBER	240.4'
BOTTOM OF CHAMBER	239.3'
BOTTOM OF STONE	239.0'
BOTTOM OF BACKFILL	VARIES, EXTENDS DOWN TO TRANSITION ZONE NEAR EXISTING GRADE



NOTE: CROSS-SECTION DEPICTS BOTH BEDS 1 AND 2

NOTE: BACKFILL MEANS GRAVELLY COARSE SAND

CROSS-SECTION (A-B AND C-D)

SCALE: 1" = 5'

MAIN-LAND DEVELOPMENT CONSULTANTS, INC.
69 MAIN ST. LIVERMORE FALLS, MAINE
367 US ROUTE 1 FALMOUTH, MAINE
182 MOOSEHEAD TRAIL, NEWPORT, MAINE
PH: (207) 897-6752 FAX: (207) 897-5404
WWW.MAIN-LANDDC.COM

PROJECT
ENGINEERED WASTEWATER DISPOSAL SYSTEM

WEBB ROAD
WINDHAM, ME

OWNER OF RECORD
ROBIE HOLDINGS, LLC

MADE FOR
D.M. ROMA CONSULTING ENGINEERS
PO BOX 1116
WINDHAM, ME 04062

DRAWING SCALE:
VARIES

SUBMISSION NOTES:
SUBMISSION 1: 2026-07-13 ERL
THIS SUBMISSION IS FOR APPLICATION.

PROJ. MGR: SRD
DRAWN BY: DRP/HRD
CHECKED BY: SRD
SUBMISSION NO. N/A
SUBMISSION DATE: 2026-07-13
SUBMITTED FOR: APPLICATION

NOT FOR CONSTRUCTION

WASTEWATER DISPOSAL DESIGN

SEAL:

SCOTT R. DIXON ME PE#9236

DRAWING NO.
E1.1

MLDC NO. 25-328 1 OF 1

VIPER Floodlight

VIPER LUMINAIRE

MICROSTRIKE | OPTICS STRIKE

FEATURES

- Low profile LED floodlighting luminaire with a variety of NEMA distributions for lighting applications such as accent lighting, sign lighting, distribution center, and general area lighting.
- Featuring two different optical technologies, Strike and Micro Strike Optics, which provide the best distribution patterns for retrofit or new construction
- Vibration rated for high vibration applications including bridges and overpasses. All housing sizes are rated for 1.5G
- Control options including photo control, occupancy sensing, NX Lighting Controls, Wiscap and 7-Pin with networked controls
- New customizable lumen output feature allows for the wattage and lumen output to be customized in the factory to meet whatever specification requirements may entail
- Field interchangeable mounting provides additional flexibility after the fixture has shipped



CONTROL TECHNOLOGY



LIGHTGRID⁺

SPECIFICATIONS

CONSTRUCTION

- Die-cast housing with hidden vertical heat fins are optimal for heat dissipation while keeping a clean smooth outer surface
- Corrosion resistant, die-cast aluminum housing with 1000 hour powder coat paint finish
- External hardware is corrosion resistant

OPTICS

- Micro Strike Optics (132, 264, 360, or 540 LED counts) maximize uniformity in retrofit applications and come standard with mid-power LEDs which evenly illuminate the entire luminous surface area to provide a low glare appearance. Catalog logic found on page 2
- Strike Optics (36, 72, 108, or 162 LED counts) provide best in class distributions and maximum pole spacing in new construction applications with high powered LEDs. Strike optics are held in place with a polycarbonate bezel to mimic the appearance of the Micro Strike Optics so both solutions can be combined on the same application. Catalog logic found on page 3
- One-piece silicone gasket ensures a weatherproof seal

INSTALLATION

- Mounting patterns for each arm can be found on page 8
- All mounting hardware included
- Knuckle arm fitter option available for 2-3/8" OD tenon
- Control options are only available on the knuckle mount option and must be installed on a vertical tenon
- Micro Strike flood configurations may be aimed up, but must have at least a 30° to allow for water to shed.

ELECTRICAL

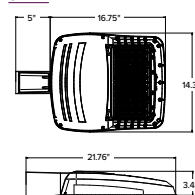
- Universal 120-277 VAC or 347-480 VAC input voltage, 50/60 Hz
- Ambient operating temperature -40°C to 40°C
- Drivers have greater than 90% power factor and less than 20% THD
- LED drivers have output power over-voltage, over-current protection and short circuit protection with auto recovery
- Field replaceable surge protection device provides 20kA protection meeting ANSI/IEEE C62.41.2 Category C High and Surge Location Category C3; Automatically takes fixture off-line for protection when device is compromised

CONTROLS

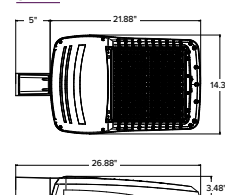
- Photo control, occupancy sensor programmable controls and Zigbee wireless controls available for complete on/off and dimming control
- Please consult brand or sales representative when combining control and electrical options as some combinations may not operate as anticipated depending on your application
- 7-pin ANSI C136.41-2013 photocontrol receptacle option available for twist lock photocontrols or wireless control modules (control accessories sold separately)
- 0-10V Dimming Drivers are standard and dimming leads are extended out of the luminaire unless control options require connection to the dimming leads. Must specify if wiring leads are to be greater than the 6" standard
- NX Lighting Controls™ available with in fixture wireless control module, features dimming and occupancy sensor
- LightGRID+ available with in fixture wireless control module, features dimming and occupancy sensor. Also available in 7-pin configuration



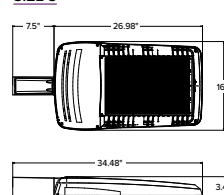
SIZE 1



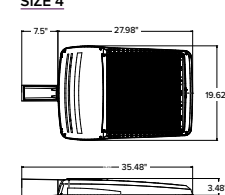
SIZE 2



SIZE 3



SIZE 4



	EPA			
	Size 1	Size 2	Size 3	Size 4
30°	0.827	1.023	1.423	1.850
60°	1.419	1.837	2.419	3.080

CERTIFICATIONS

- Listed to UL1598 and CSA C22.2#250.0-24 for wet locations and 40°C ambient temperatures
- 1.5 G rated for ANSI C136.31 high vibration applications
- Fixture is IP65 rated
- Meets IDA recommendations using 3K CCT configuration at 0 degrees of tilt
- This product meets federal procurement law requirements under the Buy American Act (FAR 52.225-9) and Trade Agreements Act (FAR 52.225-11). See Buy America(n) Solutions (link to <https://www.currentlighting.com/resources/america-solutions>)
- DLC® (DesignLights Consortium Qualified), with some Premium Qualified configurations. Please refer to the DLC website for specific product qualifications at www.designlights.org

WARRANTY

- 5 year warranty



VIPER Floodlight

VIPER LUMINAIRE

DATE:	LOCATION:
TYPE:	PROJECT:
CATALOG #:	

MICRO STRIKE OPTICS – ORDERING GUIDE

Example: VP-F-2-132L-39-3K8-4x4-UNV-AAU-BLT

CATALOG #

VP-F						
Series	Optic Platform	Size	Light Engine	CCT/CRI	Distribution	Voltage
VP-F Viper Flood	Microstrike	1 Size 1 ⁶	132L-39 5500 lumens 132L-55 7500 lumens 132L-75 10000 lumens 132L-100 12500 lumens 132L-120 15000 lumens 132L-135 18000 lumens	AP AP-Amber Phosphor Converted 27K8 2700K, 80 CRI 3K7 3000K, 70 CRI 3K8 3000K, 80 CRI 35K8 3500K, 80 CRI	2X2 Narrow Spot 4X4 Medium Spot 6X6 Wide Flood	UNV 120-277V 120 120V 208 208V 240 240V 277 277V 347 347V 480 480V
		2 Size 2	264L-130 18000 lumens 264L-155 21000 lumens 264L-175 24000 lumens 264L-205 27000 lumens 264L-235 30000 lumens 264L-260 33000 lumens	3K9 3000K, 90 CRI 4K7 4000K, 70 CRI 4K8 4000K, 80 CRI 4K9 4000K, 90 CRI 5K7 5000K, 70 CRI 5K8 5000K, 80 CRI		
		3 Size 3	360L-270 36000 lumens 360L-310 40000 lumens 360L-345 44000 lumens			
		4 Size 4	540L-350 48000 lumens 540L-390 52000 lumens 540L-415 55000 lumens 540L-460 60000 lumens ⁷ CLO Custom Lumen Output ¹			

Mounting	Color	Options	Network Control Options
AAU Adjustable Arm AA_U Adjustable arm mount for round pole ⁹ K Knuckle T Trunnion	BLT Black Matte Textured BLS Black Gloss Smooth DBT Dark Bronze Matte Textured DBS Dark Bronze Gloss Smooth GTT Graphite Matte Textured LGS Light Grey Gloss Smooth LGT Light Grey Gloss Textured PSS Platinum Silver Smooth WHT White Matte Textured WHS White Gloss Smooth VGT Verde Green Textured LEG Legacy Colors Color Option CC Custom Color	F Fusing 2PF Dual Power Feed ² 2DR Dual Driver TE Tooless Entry TB Terminal Block	NXWS16F NX Networked Wireless Enabled Integral NXSMP2-LMO PIR Occupancy Sensor with Automatic Dimming Photocell and Bluetooth Programming ^{1,3,4,8,10} NXWS40F NX Networked Wireless Enabled Integral NXSMP2-HMO PIR Occupancy Sensor with Automatic Dimming Photocell and Bluetooth Programming ^{1,3,4,8,10} NXW NX Networked Wireless Radio Module NXRM2 and Bluetooth Programming, without Sensor ^{3,4,8} WIR LightGRID+ In-Fixture Module ^{1,3,4,8}
			Stand Alone Sensors BTS-14F Bluetooth® Programmable, BTSMP-LMO PIR Occupancy Sensor with Automatic Dimming Photocell and 360° Lens ^{4,8,10} BTS-40F Bluetooth® Programmable, BTSMP-HMO PIR Occupancy Sensor with Automatic Dimming Photocell and 360° Lens ^{4,8,10} BTSO-12F Bluetooth® Programmable, BTSMP-OMNI-O PIR Occupancy Sensor with Automatic Dimming Photocell and 360° Lens ^{4,8,10}
			Stand Alone Sensors 7PR 7-Pin Receptacle ^{4,10} 7PR-SC 7-Pin Receptacle with shorting cap ^{4,10} 3PR 3-Pin twist lock ^{4,10} 3PR-SC 3-Pin receptacle with shorting cap ^{4,10} 3PR-TL 3-Pin PCR with photocontrol ^{4,10}
			Programmed Controls ADD AutoDim Timer Based Dimming ⁴ ADT AutoDim Time of Day Dimming ⁴

1 – Items with a grey background can be done as a custom order. Contact brand representative for more information
2 – Not available with trunnion mount
3 – Networked Controls cannot be combined with other control options and are limited based on mounting orientation
4 – Not available with 2PF option
5 – Not available with 480V
6 – Not available with Dual Driver option
7 – Some voltage restrictions may apply when combined with controls
8 – Control option not available in 130W or 155W configurations
9 – Replace “_” with “2” for 2.5”-3.4” OD pole, “3” for 3.5”-4.13” OD pole, “4” for 4.18”-5.25” OD pole, “5” for 5.5”-6.5” OD pole
10 – Occupancy sensor configurations only available with knuckle.
Should be mounted on a vertical tenon.
11 – PC only available on Size 1 and Size 2

VIPER Floodlight

VIPER LUMINAIRE

DATE:	LOCATION:
TYPE:	PROJECT:
CATALOG #:	

STRIKE OPTIC – ORDERING GUIDE

Example: VP-F-ST-1-36L-39-3K7-3x3-UNV-AAU-BLT

 CATALOG #

VP-F						
Series	Optic Platform	Size	Light Engine	CCT/CRI	Distribution	Voltage
VP-F Viper Flood	ST Strike	1 Size 1	36L-39 ⁷ 5500 lumens 36L-55 ⁷ 7500 lumens 36L-85 10000 lumens 36L-105 12500 lumens 36L-120 14000 lumens	AM monochromatic amber, 595nm 27K8 2700K, 80 CRI 3K7 3000K, 70 CRI 3K8 3000K, 80 CRI 3K9 3000K, 90 CRI 35K8 3500K, 80 CRI 4K7 4000K, 70 CRI 4K8 4000K, 80 CRI 4K9 4000K, 90 CRI 5K7 5000K, 70 CRI 5K8 5000K, 80 CRI	3X3 Narrow Flood 5X5 Medium Flood 4X6 Vertical Flood 6X4 Horizontal Flood	UNV 120-277V 120 120V 208 208V 240 240V 277 277V 347 347V 480 480V
		2 Size 2	72L-115 15000 lumens 72L-145 18000 lumens 72L-180 21000 lumens 72L-210 24000 lumens 72L-240 27000 lumens			
		3 Size 3	108L-215 ⁷ 27000 lumens 108L-250 30000 lumens 108L-280 33000 lumens 108L-325 36000 lumens 108L-365 40000 lumens			
		4 Size 4	162L-320 40000 lumens 162L-365 ⁹ 44000 lumens 162L-405 48000 lumens 162L-445 52000 lumens 162L-485 55000 lumens 162L-545 ⁷ 60000 lumens CLO Custom Lumen Output ¹			

Mounting	Color	Options	Network Control Options
AAU Adjustable Arm	BLT Black Matte Textured	F Fusing	NXWS16F NX Networked Wireless Enabled Integral NXSMP2-LMO PIR Occupancy Sensor with Automatic Dimming Photocell and Bluetooth Programming ^{1,3,4,11}
AA_U Adjustable arm mount for round pole ¹⁰	BLS Black Gloss Smooth	E Battery Backup ^{12,6,7,8}	NXWS40F NX Networked Wireless Enabled Integral NXSMP2-HMO PIR Occupancy Sensor with Automatic Dimming Photocell and Bluetooth Programming ^{1,3,4,11}
K Knuckle	DBT Dark Bronze Matte Textured	2PF Dual Power Feed ²	NXW NX Networked Wireless Radio Module NXRM2 and Bluetooth Programming, without Sensor ^{3,4}
T Trunnion	DBS Dark Bronze Gloss Smooth	2DR Dual Driver	WIR LightGRID+ In-Fixture Module ^{1,3,4,8}
	GTT Graphite Matte Textured	TE Toolless Entry	Stand Alone Sensors
	LGS Light Grey Gloss Smooth	TB Terminal Block	BTS-14F Bluetooth® Programmable, BTSMP-LMO PIR Occupancy Sensor with Automatic Dimming Photocell and 360° Lens ^{4,11}
	LGT Light Grey Gloss Textured		BTS-40F Bluetooth® Programmable, BTSMP-HMO PIR Occupancy Sensor with Automatic Dimming Photocell and 360° Lens ^{4,11}
	PSS Platinum Silver Smooth		BTSO-12F Bluetooth® Programmable, BTSMP-OMNI-O PIR Occupancy Sensor with Automatic Dimming Photocell and 360° Lens ^{4,11}
	WHT White Matte Textured		Stand Alone Sensors
	WHS White Gloss Smooth		7PR 7-Pin Receptacle ^{4,11}
	VGTT Verde Green Textured		7PR-SC 7-Pin Receptacle with shorting cap ^{4,11}
	LEG Legacy Colors		3PR 3-Pin twist lock ^{4,11}
	Color Option		3PR-SC 3-Pin receptacle with shorting cap ^{4,11}
	CC Custom Color		3PR-TL 3-Pin PCR with photocontrol ^{4,11}
			Programmed Controls
			ADD AutoDim Timer Based Dimming ⁴
			ADT AutoDim Time of Day Dimming ⁴

1 – Items with a grey background can be done as a custom order. Contact brand representative for more information

2 – Not available with trunnion mount

3 – Networked Controls cannot be combined with other control options and are limited based on mounting orientation

4 – Not available with 2PF option

5 – Not available with 480V

6 – Not available with 347 or 480V

7 – Not available with Dual Driver option

8 – Only available in Size 1 housing

9 – Some voltage restrictions may apply when combined with controls

10 – Replace “_” with “2” for 2.5”-3.4” OD pole, “3” for 3.5”-4.13” OD pole, “4” for 4.18”-5.25” OD pole, “5” for 5.5”-6.5” OD pole

11 – Occupancy sensor configurations only available with knuckle

VIPER Floodlight

VIPER LUMINAIRE

DATE:	LOCATION:
TYPE:	PROJECT:
CATALOG #:	

ORDERING GUIDE (CONTINUED)

CATALOG #			
Accessory Type	Size	Option	Color
SHD Shield	1 Size 1	VISOR Visor Accessory ¹	BLS Black Gloss Smooth
	2 Size 2		BLT Black Matte Textured
	3 Size 3		DBS Dark Bronze Gloss Smooth
	4 Size 4		DBT Dark Bronze Matte Textured
MTG Mounting		A Arm Mount for square pole/flat surface	GTT Graphite Matte Textured
		ASQU Universal Arm Mount for square pole	LGS Light Gray Gloss Smooth
		AAU Adjustable Arm for pole mounting	PSS Platinum Silver Smooth
		ADU Decorative upswept Arm	WHS White Gloss Smooth
		RPA Round Pole Adapter	WHT White Matte Textured
		MAF Mast Arm Fitter for 2-3/8" OD horizontal arm	VGT Verde Green Textured
		K Knuckle	LEG Legacy Colors
		T Trunnion	Color Option
		WB Wall Bracket (compatible with universal arm mounts)	CC Custom Color
Accessory Type	Option		
MSC Miscellaneous	BIRD SPK Bird Spike		

Current Control Solutions — Accessories (Sold Separately)

NX Lighting Controls

- ☐ **NXOFM2-1R1D-UNV** On-fixture Module (7-pin), On / Off / Dim, Daylight Sensor with NX Radio and Bluetooth® Radio, 120–480VAC

LightGRID+ Lighting Control

- ☐ **WIR-RME-L** On-fixture Module (7-pin or 5-pin), On / Off / Dim, Daylight Sensor with wiSCAPE Radio, 110–480VAC

For additional information related to these accessories please visit currentlighting.com/beacon. Options provided for use with integrated sensor, please view specification sheet ordering information table for details.

1 – Visor will block occupancy sensors

VP-F-ST-1-36L-85-3K7-3X3.ies

BEACON

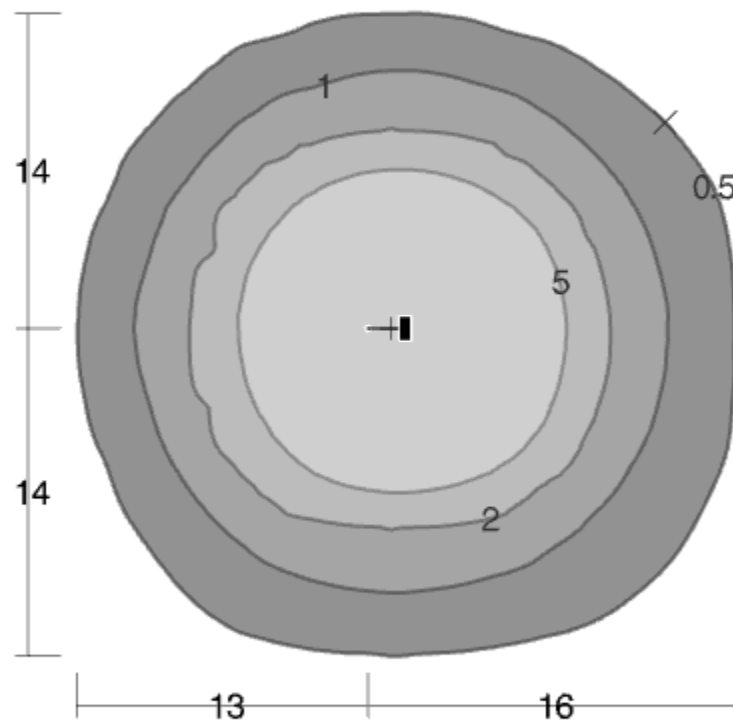
VP-F-ST-1-36L-85-3K7-3X3

Viper 2.0

Single (Arm)

Luminaire Watts	84	W
Ballast/Driver Factor	1.00	
Light Loss Factor	1.00	
Total Proration Factor	1.00	
Luminaire Lumens	9125	lms

 16 ft



Min: 0.50 fc 

Min/Avg: 20

Avg: 13 fc

Avg/Min: 20

Max: 294 fc 

 Max/Min: 587

Stormwater Treatment Table

	Total Watershed Area (SF)	New Roof Area (SF) **	New Paved/Gravel Area (SF)	New Landscaped Area (SF)	Existing/Offsite Impervious Area (SF)*	Existing/Offsite Landscaping Area (SF)*	Existing Undeveloped Area (SF)	Treatment Provided	New Impervious Area Treated (SF)	New Landscaped Area Treated (SF)	Treatment Device
WS-10	162,545	8,875	0	26,040	10,935	33,070	83,625	Dripedge	8,875	0	Dripedge Only
WS-11	28,060	0	16,490	11,570	0	0	0	Yes	16,490	11,570	FB-1
WS-12	25,580	0	1,185	3,050	3,190	2,940	15,215	No	0	0	None
WS-20	62,640	11,150	0	51,490	0	0	0	Yes	11,150	51,490	FB-1
WS-30	42,060	5,970	0	15,305	0	1,760	19,025	Yes	5,970	15,305	FB-2
WS-31	35,855	1,820	19,345	14,690	0	0	0	Yes	21,165	14,690	FB-2
WS-32	17,320	1,085	10,800	5,435	0	0	0	Yes	11,885	5,435	FB-2
WS-33	30,940	5,815	0	25,125	0	0	0	Yes	5,815	25,125	FB-2
WS-34	210,895	5,920	0	34,905	0	0	170,070	Dripedge	5,920	0	Dripedge Only
WS-40	73,990	2,960	4,315	22,800	2,595	13,110	28,210	Yes	7,275	22,800	FB-3
WS-41	132,425	795	0	15,370	0	0	116,260	Dripedge	795	0	Dripedge Only
Total		44,390	52,135	225,780					95,340	146,415	

* The project is not taking credit for the Existing / Offsite impervious and landscaped areas, but are included in the BMP sizing calculations for each treatment device.

** All buildings shall install a roofline drip edge to provide treatment for the rooftop impervious surface.

The building's impervious area is included in the watershed and overall treatment calculations below, but not included in the BMP sizing calculations for the underdrained filter basins.

New Impervious Area = 96,525
 New Impervious Area Requiring Treatment (90%) 86,873
 Provided New Impervious Treatment= 95,340
 99% New Impervious Area Treated

New Developed Area = 322,305
 New Developed Area Requiring Treatment (75%)= 241,729
 New Developed Area Treated= 241,755
 75% New Developed Area Treated

25007 - POST

Type III 24-hr 25-Year Rainfall=5.80"

Prepared by {enter your company name here}

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Summary for Pond FB1&2: Filter Basin

[62] Hint: Exceeded Reach R11 OUTLET depth by 0.79' @ 12.60 hrs

Inflow Area = 216,805 sf, 33.43% Impervious, Inflow Depth = 3.78" for 25-Year event
 Inflow = 17.86 cfs @ 12.12 hrs, Volume= 68,344 cf
 Outflow = 5.81 cfs @ 12.51 hrs, Volume= 68,353 cf, Atten= 67%, Lag= 23.9 min
 Primary = 5.81 cfs @ 12.51 hrs, Volume= 68,353 cf
 Secondary = 0.00 cfs @ 0.00 hrs, Volume= 0 cf

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.10 hrs
 Peak Elev= 235.04' @ 12.51 hrs Surf.Area= 13,679 sf Storage= 26,793 cf

Plug-Flow detention time= (not calculated: outflow precedes inflow)
 Center-of-Mass det. time= 263.0 min (1,074.6 - 811.6)

Volume	Invert	Avail.Storage	Storage Description
#1	232.00'	41,810 cf	Custom Stage Data (Prismatic) Listed below (Recalc)

Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
232.00	5,260	0	0
234.00	9,500	14,760	14,760
236.00	17,550	27,050	41,810

Device	Routing	Invert	Outlet Devices
#1	Primary	229.73'	10.0" Round Culvert L= 30.0' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 229.73' / 229.00' S= 0.0243 '/' Cc= 0.900 n= 0.013, Flow Area= 0.55 sf
#2	Device 1	229.83'	1.7" Vert. 1-3/4" Orifice C= 0.600
#3	Device 2	232.00'	2.410 in/hr Exfiltration over Surface area
#4	Device 1	233.50'	15.0" W x 11.0" H Vert. Orifice/Grate C= 0.600
#5	Device 1	234.45'	Neenah R4345 Beehive Grate Light Duty-req. structure Head (feet) 0.00 0.10 0.15 0.20 0.25 0.30 0.35 0.40 0.50 0.60 0.70 0.80 0.90 1.00 Disch. (cfs) 0.000 0.900 1.600 2.500 3.500 4.000 4.600 5.300 6.800 7.500 8.100 8.600 9.100 9.600
#6	Secondary	235.10'	10.0' long x 10.0' breadth Broad-Crested Rectangular Weir Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 Coef. (English) 2.49 2.56 2.70 2.69 2.68 2.69 2.67 2.64

Primary OutFlow Max=5.81 cfs @ 12.51 hrs HW=235.03' TW=229.11' (Dynamic Tailwater)

1=Culvert (Inlet Controls 5.81 cfs @ 10.65 fps)
 2=1-3/4" Orifice (Passes < 0.17 cfs potential flow)
 3=Exfiltration (Passes < 0.76 cfs potential flow)
 4=Orifice/Grate (Passes < 5.68 cfs potential flow)
 5=Neenah R4345 Beehive Grate Light Duty-req. structure(Passes < 7.39 cfs potential flow)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=232.00' TW=0.00' (Dynamic Tailwater)

6=Broad-Crested Rectangular Weir (Controls 0.00 cfs)