

4 Blanchard Road, P.O. Box 85A Cumberland, ME 04021 Tel: 207.829.5016 • Fax: 207.829.5692 info@smemaine.com smemaine.com

April 6, 2020

Ms. Jennifer Curtis, Planner Town of Windham 8 School Road Windham, ME 04062

Subject: Bangor Savings Bank Windham Branch/Office Building

745 &747 Roosevelt Trail, Windham, Maine

**Response to Staff Review Comments** 

Dear Ms. Curtis,

On behalf of Bangor Savings Bank (BSB), Sevee & Maher Engineers, Inc. (SME) is pleased to submit this comment response letter and supporting documentation for the Bangor Savings Bank Branch/Office Building project at 745 &747 Roosevelt Trail in Windham. The drawings have been revised in response to staff review comments received in an email dated March 13, 2020 and Gorrill-Palmer traffic review comments received in an email dated 4/1/2020. SME is providing this letter to address review comments prior to the Planning Board meeting scheduled for April 13, 2020.

#### **TOWN PLANNER:**

 Evidence meeting the requirements of 811.1.(d)(2)(ii): "The location and dimensions of all provisions for water supply and wastewater disposal, and evidence of their adequacy for the proposed use, including soils test pit data if on-site sewage disposal is proposed." (We usually accept an HHE-200)

<u>SME Response</u>: SME submitted an electronic copy of a completed HHE-200 form to the Planning Office via email on April 1, 2020. A copy of the completed HHE-200 form is attached to this letter for reference.

2. Evidence of coordinating with PWD for public water hookup (Ability to Serve or equivalent)

<u>SME Response</u>: A letter from PWD outlining their capacity to serve the project is included in the application package as Attachment E.

3. Ground floor elevations of existing buildings

<u>SME Response:</u> Door sill elevations for existing buildings are included in the ALTA survey completed by Jones Associates. A copy of the ALTA survey is included in the project plan set.



4. Location, front view, materials and dimensions of proposed signs with method for securing signs. (Also show existing signs, and indicate if they will stay, or indicate otherwise)

<u>SME Response</u>: Building mounted signs are outlined on the architectural elevations included in the Application package as Attachment H. Design sheets from Neokraft Signs, Bangor Savings Bank's sign consultant, are attached to outline the location, front view, and dimensions for proposed free-standing signs for this project. All existing signs on the property will be removed before project completion.

5. Show location and type of exterior lighting (show light poles on plan, and indicate type in details)

<u>SME Response</u>: Light pole locations are outlined on plan sheet C-104. Cut sheets for exterior pole mounted light fixtures are included in the Application package as Attachment G.

6. It is not clear from the plan that the designated right-turn-only entrance from northbound 302 is going to prohibit traffic from turning left from southbound 302 across northbound 302, to enter the site. Will the applicant please clarify what prohibits this movement and if it is adequate?

<u>SME Response</u>: The geometry of the entrance island has been modified to further discourage entrance across the northbound travel lane from southbound US-302. Project plans have been updated to reflect this change. Copies of the updated plan sheets are attached for reference. We believe these modifications will keep alert, responsible drivers from using the entrance inappropriately.

7. I see the recommendation for the intersection of Abby Road on the Traffic Analysis. I think it would be helpful if the applicant provided a diagram or plan and details showing the proposed pavement markings and sign

<u>SME Response</u>: Project plans have been updated to include the pavement striping and signage recommendations outlined in the traffic analysis. Copies of the updated plan sheets are attached for reference.

#### **TOWN ENGINEER:**

1. For infiltration Basin 2 (Pond 1CP1) the peak elevation for the water level in the basin calculated by HydroCad is 309.35' for the 25-yr storm compared to the top of the basin at 309.50'. Overflow, if/when it occurs, will likely flow onto the entrance to the drive-through on Route 115. The 0.15' of freeboard does not seem to be sufficient considering the overflow would go onto Rte. 115. It is recommended that the basin design be modified to provide at least 1 foot of freeboard.

SME Response: Infiltration basin 2 (Pond 1CP1) is designed to provide 0.5 feet of freeboard above the emergency spillway elevation. Spot grades have been added to the grading plan for



clarity. Overflow is intended to travel overland to the municipal storm drain system in the rightof-way based on initial design recommendations from Town staff. Copies of the updated plan sheets, an updated stormwater quantity analysis, and updated post-development stormwater modeling calculations are attached for reference.

2. Although the amount of runoff flowing into the public right-of-way is being largely reduced, there are still about 5,000 - 6,000 SF flowing into Route 302 at the entrance to the project in this area. Other options to minimize the amount flowing onto Rte. 302 in this area should be considered.

<u>SME Response:</u> Proposed improvements to site grading stormwater management will significantly reduce the peak flow and volume of stormwater runoff leaving the property and reduce the load on the existing municipal storm drain system. Further reductions in surface runoff from the property will require costly structural stormwater management devices that will burden the Applicant with long-term maintenance and potential replacement costs.

3. The entrance to the drive-through off of Route 115 appears to provide minimal room for queuing. The distance from the sidewalk on Route 115 is only about 80', which is room for about 4 vehicles. A traffic study has not yet been submitted, but when submitted, should evaluate whether the queuing distance is sufficient to prevent baking up onto Rte. 115.

<u>SME Response</u>: The drive through is designed with two lanes to provide quick service and adequate queueing for bank patrons. The drive through is also equipped with a slip lane to minimize congestion. The site is also designed with open sight lines, which will allow patrons approaching the Bank to bypass the ME-115 site access, if necessary and enter the site from US-302 to queue internally. Based on historical use at other branches, the Bank views this as an extreme condition not typically experienced during normal operations.

#### Gorrill-Palmer Traffic Peer Review:

1. GP agrees with the use of the 10th edition of the Institute of Transportation Engineers' (ITE) Trip Generation manual. GP agrees that the most representative Land Use Codes (LUC) were used for the existing/proposed office area (LUC 710 – General Office) and proposed bank area (LUC 912 – Drive-In Bank). As mentioned in the report, there is not a representative land use code for retail. The LUC used (820 – Shopping Center) for the existing 938 SF retail building (iPhone repair store), in our opinion, does not accurately represent the use; however, based on the size of the retail building and potential other options that may have been used, changing this trip generation would not be expected to change any of the conclusions of the study.

SME Response: No response necessary.

2. GP agrees with the existing trip generation for office and retail space.

<u>SME Response</u>: No response necessary.



3. GP agrees with the proposed trip generation for office and bank development, with the exception of the PM Peak Hour of the Generator for the Bank, which we could not reproduce. Since the adjacent street trip generation is used for the remainder of the study and not the trip generation of the generator, the conclusions of the study would not change.

SME Response: No response necessary.

4. GP agrees with the methods used to seasonally and annually adjust the traffic counts to a 2021 no-build condition.

SME Response: No response necessary.

5. The Trip Assignments provided on Figure 4 do not appear to add from a roadway network perspective. The volumes entering and exiting the site appear correct, but the volumes flowing through the rest of the system do not appear to agree. Resulting changes to other figures or capacity analysis should be revisited.

SME Response: Sewall has addressed this comment in a response letter attached for reference.

6. The results of the traffic analysis for level of service are correctly identified from the simulation to the report (see above comment for possible changes). The applicant has noted that the level of service of one approach does change from an "E" to an "F". Per the Town of Windham Ordinance, if the level of service of an intersection is an "E" or worse, the level of service should not decrease because of the additional traffic. The overall intersection level of service is not provided. The applicants traffic engineer should provide a response to this item. This criteria can be waived by the Planning Board.

SME Response: Sewall has addressed this comment in a response letter attached for reference.

7. It should be noted that the results of the capacity analysis provided in the study are most likely not accurate due to the impacts on traffic flow from the adjacent signalized intersection. However, the results provided in the study can be used as an indicator of the level of impact of the project on the intersection.

SME Response: Sewall has addressed this comment in a response letter attached for reference.

8. GP agrees with the safety analysis for High Crash Locations and mitigation tactics to improve these locations. This includes additional striping and signage to not block the intersection.

SME Response: No response necessary.

9. It should be noted that the proposed access management measures (reduction of driveways and restriction of movements) to this corner should have a net positive impact to the overall area, reducing potential conflicts and improving safety. However, the applicant should



address the Town's double frontage requirements. We recommend the applicant revisit the channelization of the proposed driveways to improve the enforcement of right turn movements only. As currently shown at both driveways, the restrictions do not appear to be prohibitive enough.

SME Response: Municipal Ordinance Section 812(B) (2)(e) outlines where a lot has frontage on two (2) or more streets, the primary access to and egress from the lot shall be provided from the street where there is less potential for traffic congestion and for traffic and pedestrians hazards. Access from other streets may be allowed if it is safe and does not promote shortcutting through the site.

SME believes the current design adheres to this standard. The main site entrance is located on Abby Road, which is the street where there is less potential for traffic congestion and for traffic and pedestrian hazards. Access from ME-115 and US-302 are designed to be safe. Internal vehicular circulation routes do not promote shortcutting through the site.

SME has updated entrance geometry at the US-302 and ME-115 site entrances to improve access management and access drive channelization. Copies of the updated plan sheets are attached for reference. We believe these modifications will encourage alert, responsible drivers to follow proposed circulation routes on the property and at entrances and exits to the public right of way.

If you have any questions or comments, please do not hesitate to contact me.

Sincerely,

SEVEE & MAHER-ENGINEERS. IN

Jeffrey Read P.E. **Project Manager** 

cc: Mark Arienti, P.E, Town Engineer David Latulippe, CJ Developers

Jason Donovan, Bangor Savings Bank

**Attachments** 

#### SUBSURFACE WASTEWATER DISPOSAL SYSTEM APPLICATION Div of Environmental Health, 11 SHS (207) 287-2070 Fax: (207) 287-4172 PROPERTY LOCATION >> CAUTION: LPI APPROVAL REQUIRED << City, Town, Windham or Plantation Permit # Street or Road 745 Roosevelt Trail Date Permit Issued \_\_\_/\_\_/\_\_ Fee: \$\_\_\_\_\_ Double Fee Charged [ ] Subdivision Lot # \_\_\_ L.P.I. #\_\_ Local Plumbing Inspector Signature OWNER/APPLICANT INFORMATION □ Owner □ Town □ State Name (last, first, MI) ✓ Owner Donovan, Jason (for Bangor Savings Bank) The Subsurface Wastewater Disposal System shall not be installed until a ■ Applicant Permit is issued by the Local Plumbing Inspector. The Permit shall Mailing Address of ' authorize the owner or installer to install the disposal system in accordance Owner/Applicant with this application and the Maine Subsurface Wastewater Disposal Rules. Daytime Tel. # Municipal Tax Map # Lot # CAUTION: INSPECTION REQUIRED OWNER OR APPLICANT STATEMENT I state and acknowledge that the information submitted is correct to the best of I have inspected the installation authorized above and found it to be in compliance with the Subsurface Wastewater Disposal Rules Application. my knowledge and understand that any falsification is reason for the Department and/or Local Plumbing Inspector to deny a Permit. (1st) date approved Signature of Owner or Applicant Date Local Plumbing Inspector Signature (2nd) date approved PERMIT INFORMATION **TYPE OF APPLICATION** THIS APPLICATION REQUIRES **DISPOSAL SYSTEM COMPONENTS** 1. Complete Non-engineered System √ 1. No Rule Variance 1. First Time System ☐ 2. Primitive System (graywater & alt. toilet) 2. Replacement System 2. First Time System Variance 3. Alternative Toilet, specify:\_\_\_ ☐ a. Local Plumbing Inspector Approval b. State & Local Plumbing Inspector Approval 4. Non-engineered Treatment Tank (only) 5. Holding Tank, \_\_\_\_\_ gallons 6. Non-engineered Disposal Field (only) Type replaced: Year installed: 3. Replacement System Variance 3. Expanded System a. Local Plumbing Inspector Approval b. State & Local Plumbing Inspector Approval ☐ 7. Separated Laundry System a. <25% Expansion b. ≥25% Expansion 8. Complete Engineered System (2000 gpd or more) ☐ 4. Experimental System 9. Engineered Treatment Tank (only) 4. Minimum Lot Size Variance 10. Engineered Disposal Field (only) 5. Seasonal Conversion 5. Seasonal Conversion Permit 11. Pre-treatment, specify: SIZE OF PROPERTY DISPOSAL SYSTEM TO SERVE ☐12. Miscellaneous Components 1. Single Family Dwelling Unit, No. of Bedrooms: \_\_\_\_\_ 0.9 + / -SQ. FT. TYPE OF WATER SUPPLY 2. Multiple Family Dwelling, No. of Units: \_\_\_\_\_ ✓ ACRES √ 3. Other: Bank and Insurance Company 1. Drilled Well 2. Dug Well 3. Private SHORELAND ZONING (specify) 4. Public 5. Other Yes Current Use Seasonal Year Round Undeveloped **DESIGN DETAILS (SYSTEM LAYOUT SHOWN ON PAGE 3) DISPOSAL FIELD TYPE & SIZE GARBAGE DISPOSAL UNIT** TREATMENT TANK **DESIGN FLOW** ✓ 1. Concrete 1. Stone Bed 2. Stone Trench √ 1. No ☐ 2. Yes ☐ 3. Maybe ☑a. Regular □b. Low Profile √ 3. Proprietary Device gallons per day If Yes or Maybe, specify one below: BASED ON: ☐ a. cluster array ☐ c. Linear ☐ b. regular load ☐ d. H-20 load a. multi-compartment tank ☑ 1. Table 4A (dwelling unit(s)) 2. Plastic b. \_\_\_ tanks in series 3. Other: ☐ 2. Table 4C(other facilities) SHOW CALCULATIONS for other facilites 24 employees w/no showers at 12 gpd each (288 gpd) 4. Other: CAPACITY: 1.000 c. increase in tank capacity d. Filter on Tank Outlet **SOIL DATA & DESIGN CLASS DISPOSAL FIELD SIZING** EFFLUENT/EJECTOR PUMP ☐ 3. Section 4G (meter readings) PROFILE CONDITION . Not Required depends on ATTACH WATER METER DATA level of 5 / B May Be Required plumbing in proposed bank √ 1. Medium---2.6 sq. ft. / gpd LATITUDE AND LONGITUDE at Observation Hole # TP-1 2. Medium---Large 3.3 sq. f.t / gpd at center of disposal area . Required \_\_d 50 \_\_d 26 Depth >65 " 3. Large---4.1 sq. ft. / gpd Specify only for engineered systems: Lon. W 70 \_m 16.4 of Most Limiting Soil Factor DOSE: \_\_\_\_\_ gallons 4. Extra Large---5.0 sq. ft. / gpd if g.p.s, state margin of error: SITE EVALUATOR STATEMENT I certify that on 3/25/2020 (date) I completed a site evaluation on this property and state that the data reported are accurate and that the proposed system is in compliance with the State of Maine Subsurface Wastewater Disposal Rules (10-144A CMR 241). #370 Site Evaluator Signature 3/30/2020 SE# Date Andrew Gobeil (207) 829-5016 apg@smemaine.com Site Evaluator Name Printed Telephone Number E-mail Address

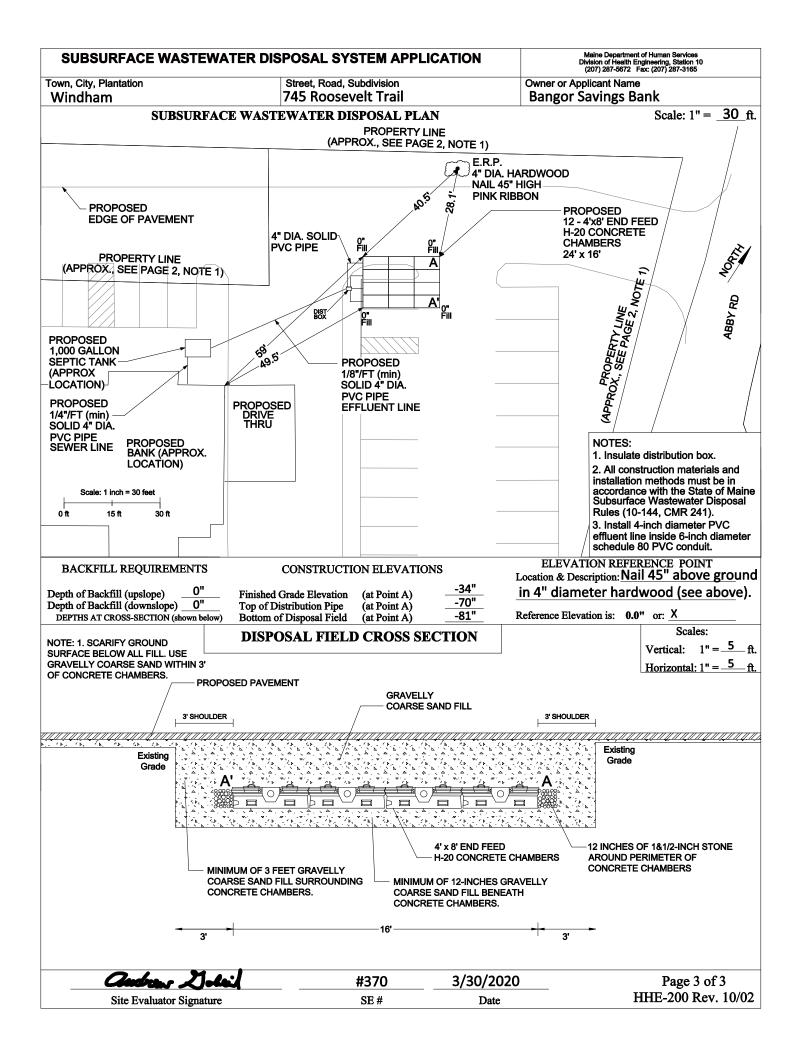
Note: Changes to or deviations from the design should be confirmed with the Site Evaluator.

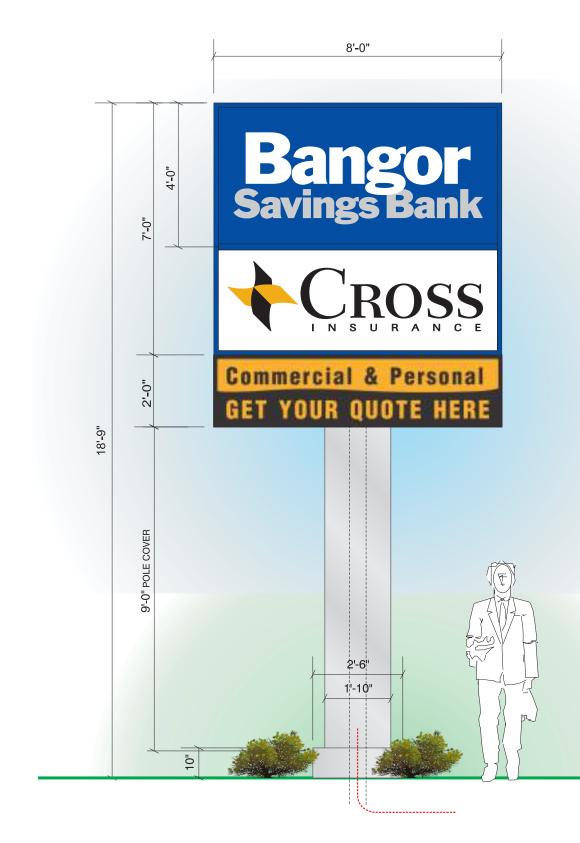
Maine Dept.Health & Human Services

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HHE-200 Rev. 08/2011

#### Maine Department of Human Service SUBSURFACE WASTEWATER DISPOSAL SYSTEM APPLICATION Division of Health Engineering, Station 10 (207) 287-5672 Fax: (207) 287-3165 Town, City, Plantation Street, Road, Subdivision Owner or Applicant Name **Bangor Savings Bank** Windham 745 Roosevelt Trail SITE LOCATION PLAN SITE PLAN Scale 1'' = 80ft. (map from Maine Atlas recommended) **PROPOSED** 1,000 GALLON SEPTIC TANK (APPROX EXISTING BUILDING (APPROX. 115 LOCATION) LOCATION) **PROPOSED** PROPERTY LINE 12 - 4'x8' END FEED (APPROX., SEE NOTE 1) H-20 CONCRETE 4" DIA. HARDWOOD **CHAMBERS** NAIL 45" HIGH PINK RIBBON 24' x 16' 10 is 50 ROOSEVELT TRAIL Ø5.66.41 Sketc NOTES: 38.81 1. Property boundaries shown are approximate. Disposal field is located at least 10 feet from property line based on information provided by the owner. PROPOSED BANK (APPROX. 2. Proposed septic tank must be located at least 8 feet from 3 BUILDING (\* LOCATION) LOCATION) proposed full-foundation. 3. Area served by public water supply. 8 4. Proposed foundation must be at least 20 feet from proposed disposal field. 5. It is the responsibility of the contractor/excavator to confirm that there are no underground utilities Scale: 1 inch = 80 feet (e.g., electric, gas, water) in areas TANDBERG TRAIL 40 ft 0 ft required to be excavated. 6. Proposed stormwater detention basin must be located at least 50 feet from proposed septic tank and disposal field. SOIL PROFILE DESCRIPTION AND CLASSIFICATION (Location of Observation Holes Shown Above) Test Pit ☐ Boring Observation Hole # \_ TP-1 X Test Pit Boring Observation Hole # Depth of organic horizon above mineral soil Depth of organic horizon above mineral soil 0 Mottling Consistency Color Mottling Texture Consistency Color Texture 0 Fine Sandy Friable 10YR 6/6 Loam (fill) 6 6 surface (inches) surface (inches) 12 12 10YR 8/6 Gravelly Fine to 18 18 Course Depth below mineral soil <u>S</u> Sand (fill) 24 mineral ~~~~~ ^^^^ 30 30 Loamy Fine 10YR 4/3 below Sand 36 36 Depth **Gravelly Fine** 42 42 10YR 8/6 None to Loose to Course Sand to 65"+ 65"+ to 65"+ 48 48 Classificatioin Slope Limiting Factor Soil Classificatioin Slope Limiting Factor ☐ Groundwater ☐ Groundwater ☐ Restrictive Lave □ Restrictive Layer >65" ☐ Bedrock □ Bedrock Condition Profile Percent Depth Profile Condition Percent Depth Page 2 of 3 audrens . 3/30/2020 #370 HHE-200 Rev. 10/02 SE# Date Site Evaluator Signature





SIGNCOMP WIDEBODY [#2005] ALUMINUM EXTRUDED CABINET, 1½" RETAINER, TOP AND BOTTOM AND 1½" DUAL FRAME AND COVER ON SIDES, PAINTED 'AKZO' SIGN 4402, WHITE 'LED' ILLUMINATION,

'BANGOR' - 3/16" THICK TRANS WHITE SG ACRYLIC FACES WITH GSP TRANS COBALT BLUE [230-157] VINYL BACKGROUND AND KNOCKED OUT TRANS WHITE COPY; GSP TRANS SILVER OVERLAY ON "SAVINGS BANK",

'CROSS' - 3/16" THICK TRANS WHITE SG ACRYLIC FACES WITH MANGO TRANSL (230-125) AND MATTE BLACK,

'EMC' - FULL COLOR

FABRICATED .080 CLEAR ANODIZED ALUMINUM POLE COVER AND PEDESTAL

STEEL POLES, SET IN CONCRETE, ELECTRICAL TO SIGN LOCATION BY OWNER

**DOUBLE-FACE INTERNALLY ILLUMINATED PYLON - RT 302** 

SCALE: 3/8"=1'-0"

(1) REQUIRED



**SEE SITE PLAN, PAGE 3** 

# NEOKRAFT

#### Neokraft Signs, Inc.

647 Pleasant Street Lewiston, Maine 04240 207.782.9654 | 800.339.2258 neokraft.com

#### Custom Sign Fabrication

These plans are the exclusive property of Neokraft Signs, Inc. and are the result of the original work of its employees. They are submitted to Neokraft's client for the sole purpose of consideration of whether to purchase these plans or to purchase from Neokraft a sign manufactured according to these plans.

Distribution or exhibition of these plans to anyone other than employees of said client, or use of these plans to construct a sign similar to the one embodied herein, is expressly forbidden. In the event that such exhibition or construction occurs, Neokraft expects to be reimbursed \$1500 in compensation for time and effort entailed in creating these plans.

#### PRESENTATION

#### BANGOR SAVINGS BANK

@8338-3

ACCT ID: 012022

LOCATION: 745 ROOSEVELT TRAIL

WINDHAM, MAINE

DRAWING NO: 1 OF 3

DRAWN BY: BK REP.: MM

DATE: 03.23.2020 QUOTE: @8338-2

GEN REF: 18/367

EF: 18/3677.1, 19/5224.3,

16/1116-1.1

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1'-6"

10"

**END VIEW** 

1'-3"



SIGNCOMP WIDEBODY [#2005] ALUMINUM EXTRUDED CABINET, 1½" RETAINER, TOP AND BOTTOM AND 1½" DUAL FRAME AND COVER ON SIDES, PAINTED 'AKZO' SIGN 4402, WHITE 'LED' ILLUMINATION,

'BANGOR' - 3/16" THICK TRANS WHITE SG ACRYLIC FACES WITH GSP TRANS COBALT BLUE [230-157] VINYL BACKGROUND AND KNOCKED OUT TRANS WHITE COPY; GSP TRANS SILVER OVERLAY ON "SAVINGS BANK",

'CROSS' - 3/16" THICK TRANS WHITE SG ACRYLIC FACES WITH MANGO TRANSL (230-125) AND MATTE BLACK,

FABRICATED .080 CLEAR ANODIZED ALUMINUM POLE COVER AND PEDESTAL

STEEL POLES, SET IN CONCRETE, ELECTRICAL TO SIGN LOCATION BY OWNER

**DOUBLE-FACE INTERNALLY ILLUMINATED PYLON - RT 115** 

SCALE: 3/8"=1'-0"

(1) REQUIRED



SEE SITE PLAN, PAGE 3

# NEOKRAFT

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#### PRESENTATION

#### BANGOR SAVINGS BANK

@8338-3

ACCT ID: 012022 LOCATION: 745 ROOSEVELT TRAIL

WINDHAM, MAINE

DRAWING NO: 2 OF 3

DRAWN BY: BK REP.: MM

DATE: 03.23.2020

QUOTE: @8338-2

GEN REF: 18/3677.1, 19/5224.3,

16/1116-1.1

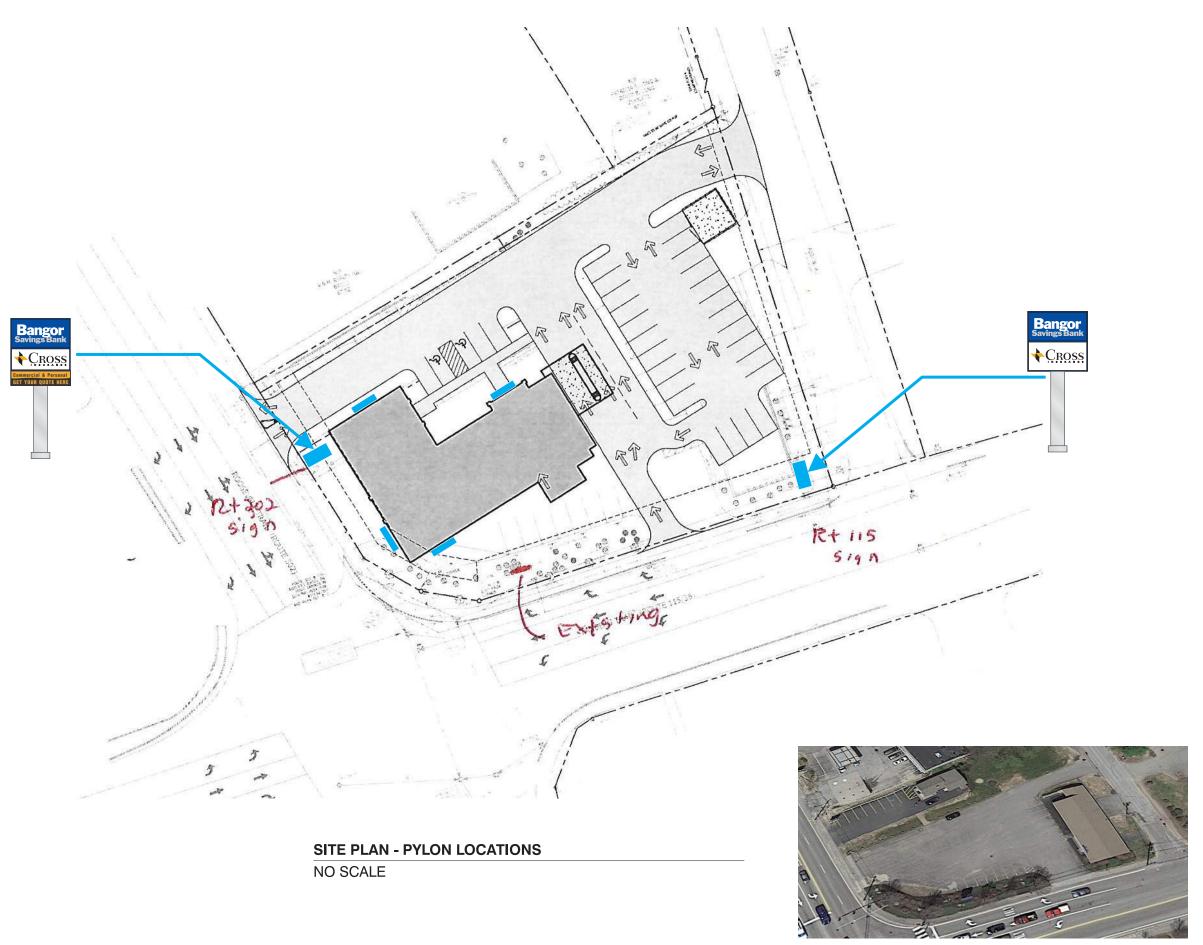
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1'-6"

10"

**END VIEW** 

1'-3"



## NEOKRAFT

### SIGNS

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#### PRESENTATION

#### **BANGOR SAVINGS BANK**

@8338-3

ACCT ID: 012022

LOCATION: 745 ROOSEVELT TRAIL

WINDHAM, MAINE

DRAWING NO: 3 OF 3

DRAWN BY: REP.: MM

DATE: 03.23.2020

@8338-2 QUOTE:

18/3677.1, 19/5224.3, GEN REF:

16/1116-1.1

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#### 5.0 STORMWATER QUANTITY ANALYSIS (Revised April 3, 2020)

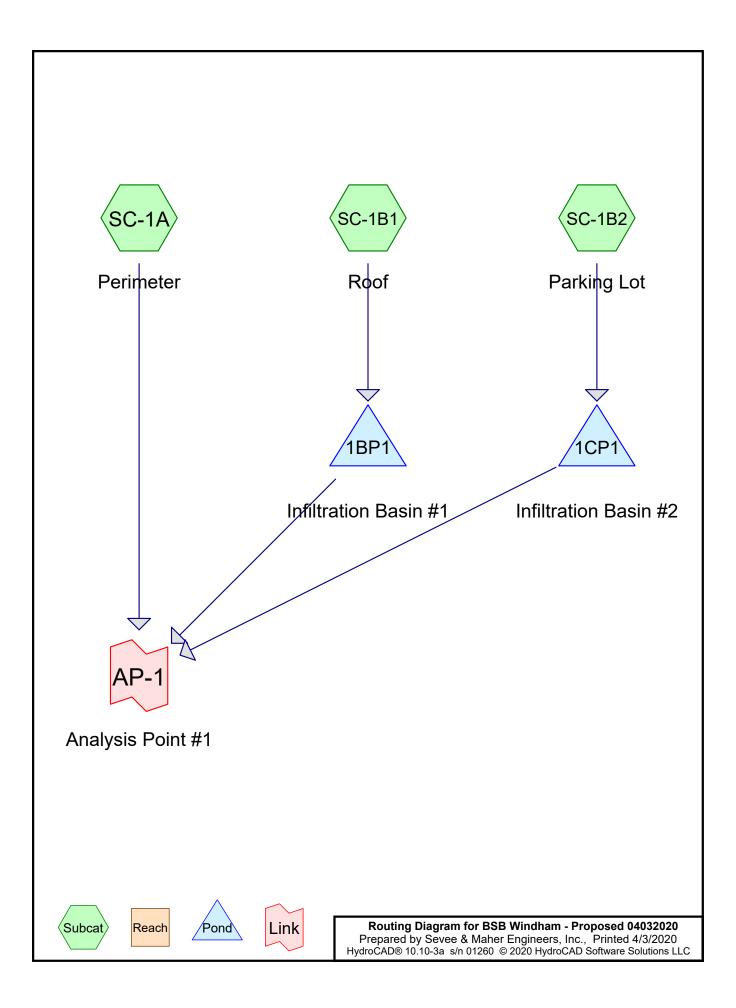
Stormwater quantity is managed to the maximum extent practicable through minimizing the amount of impervious area on the site and utilizing the storage characteristics of the infiltration basins in the southern portion of the project area.

Stormwater peak flow rates were modeled for the 2-, 10-, and 25-year/24-hour storm events with Type III Soil Conservation Service rainfall distribution, using the HydroCAD computer modeling system by Applied Microcomputer Systems of Chocorua, New Hampshire. The peak flow rates at each Analysis Point are summarized in Table 1. Copies of the calculations for the pre-development and post-development models are provided in Appendix B.

Table 1
STORMWATER QUANTITY SUMMARY

	2-yr Storm		10-yr 9	Storm	25-yr Storm		
AP	Pre- (cfs)	Post- (cfs)	Pre- (cfs)	Post- (cfs)	Pre- (cfs)	Post- (cfs)	
1	2.29	1.23	4.43	2.43	6.21	3.45	

Site drainage from the proposed redevelopment will generally follow the pre-development conditions. As outlined in Table 1, our model indicates decreased peak flow rates at AP-1 for the post-development conditions, which represents a reduction in surface runoff to the municipal storm drain system as compared to the existing conditions.



Type III 24-hr 2-yr Storm Rainfall=3.10"

Prepared by Sevee & Maher Engineers, Inc.

Printed 4/3/2020

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Time span=5.00-20.00 hrs, dt=0.05 hrs, 301 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment SC-1A: Perimeter Runoff Area=36,666 sf 68.23% Impervious Runoff Depth>1.16"

Tc=5.0 min CN=79 Runoff=1.23 cfs 0.082 af

Subcatchment SC-1B1: Roof Runoff Area=10,924 sf 64.08% Impervious Runoff Depth>1.05"

Tc=5.0 min CN=77 Runoff=0.33 cfs 0.022 af

Subcatchment SC-1B2: Parking Lot Runoff Area=17,180 sf 80.42% Impervious Runoff Depth>1.63"

Tc=5.0 min CN=86 Runoff=0.81 cfs 0.054 af

Pond 1BP1: Infiltration Basin #1 Peak Elev=308.11' Storage=88 cf Inflow=0.33 cfs 0.022 af

Discarded=0.18 cfs 0.022 af Primary=0.00 cfs 0.000 af Outflow=0.18 cfs 0.022 af

Pond 1CP1: Infiltration Basin #2 Peak Elev=308.56' Storage=529 cf Inflow=0.81 cfs 0.054 af

Discarded=0.23 cfs 0.054 af Primary=0.00 cfs 0.000 af Outflow=0.23 cfs 0.054 af

Link AP-1: Analysis Point #1 Inflow=1.23 cfs 0.082 af

Primary=1.23 cfs 0.082 af

Type III 24-hr 2-yr Storm Rainfall=3.10"

Prepared by Sevee & Maher Engineers, Inc.

Printed 4/3/2020

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#### **Summary for Subcatchment SC-1A: Perimeter**

Runoff 1.23 cfs @ 12.08 hrs, Volume= 0.082 af, Depth> 1.16"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 2-yr Storm Rainfall=3.10"

A	rea (sf)	CN	Description				
	131	32	Woods/gras	s comb., G	Good, HSG A		
	14,767	98	Paved road	s w/curbs &	& sewers, HSG A		
	11,517	39	Pasture/gra	ssland/rang	ge, Good, HSG A		
	10,251	98	Paved parki	ng, HSG A			
	36,666	79	Weighted Average				
	11,648		31.77% Pervious Area				
	25,018		68.23% Imp	ervious Are	ea		
Тс	Length	Slope	•	Capacity	Description		
(min)	(feet)	(ft/ft	) (ft/sec)	(cfs)			
5.0					Direct Entry, 5 minutes Minumum		

#### Summary for Subcatchment SC-1B1: Roof

0.33 cfs @ 12.08 hrs, Volume= 0.022 af, Depth> 1.05" Runoff

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 2-yr Storm Rainfall=3.10"

Are	ea (sf)	CN I	Description					
	7,000	98 I	Roofs, HSG	i A				
	3,924	39 I	Pasture/gra	ssland/rang	ge, Good, HSG A			
1	10,924	77 \	Weighted Average					
	3,924	;	35.92% Pervious Area					
	7,000	(	34.08% Imp	ervious Are	ea			
Тс	Length	Slope	Velocity	Capacity	Description			
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)				
5.0					Direct Entry, 5 minutes min			

Direct Entry, 5 minutes min

#### **Summary for Subcatchment SC-1B2: Parking Lot**

0.81 cfs @ 12.08 hrs, Volume= 0.054 af. Depth> 1.63" Runoff

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 2-yr Storm Rainfall=3.10"

Type III 24-hr 2-yr Storm Rainfall=3.10"

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Α	rea (sf)	CN	Description					
	13,816	98	Paved parking, HSG A					
	3,364	39	Pasture/grassland/range, Good, HSG A					
	17,180	86	Weighted Average					
	3,364		19.58% Pervious Area					
	13,816		80.42% Impervious Area					
_								
Тс	Length	Slope						
(min)	(feet)	(ft/ft	t) (ft/sec) (cfs)					

5.0

Direct Entry, 5 minutes minumum

#### **Summary for Pond 1BP1: Infiltration Basin #1**

Inflow Area = 0.251 ac, 64.08% Impervious, Inflow Depth > 1.05" for 2-yr Storm event 
Inflow = 0.33 cfs @ 12.08 hrs, Volume= 0.022 af 
Outflow = 0.18 cfs @ 12.24 hrs, Volume= 0.022 af, Atten= 46%, Lag= 9.2 min 
Discarded = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 308.11' @ 12.24 hrs Surf.Area= 833 sf Storage= 88 cf

Plug-Flow detention time= 3.3 min calculated for 0.022 af (100% of inflow)

Center-of-Mass det. time= 3.0 min (814.7 - 811.7)

Volume	Invert	Avail.Sto	rage Storage D	escription			
#1	308.00'	3,6	5 cf Custom Stage Data (Conic)Listed below (Recalc)				
Elevation		urf.Area	Inc.Store	Cum.Store	Wet.Area		
(fee	et)	(sq-ft)	(cubic-feet)	(cubic-feet)	(sq-ft)		
308.0	00	748	0	0	748		
309.0	00	1,683	1,184	1,184	1,691		
310.0	00	3,332	2,461	3,645	3,349		
Device	Routing	Invert	Outlet Devices				
#1	Discarded	308.00'	9.070 in/hr Exf	iltration over We	etted area		
#2	Primary	309.50'	10.0' long x 4.	0' breadth Broad	I-Crested Recta	ngular Weir	
	J		Head (feet) 0.2	0.40 0.60 0.8	0 1.00 1.20 1.4	10 1.60 1.80 2.00	
			2.50 3.00 3.50	4.00 4.50 5.00	5.50		
			Coef. (English)	2.38 2.54 2.69	2.68 2.67 2.67	2.65 2.66 2.66	
				3 2.76 2.79 2.88			

**Discarded OutFlow** Max=0.18 cfs @ 12.24 hrs HW=308.11' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.18 cfs)

Primary OutFlow Max=0.00 cfs @ 5.00 hrs HW=308.00' (Free Discharge) 2=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Type III 24-hr 2-yr Storm Rainfall=3.10"

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#### Summary for Pond 1CP1: Infiltration Basin #2

Inflow Area = 0.394 ac, 80.42% Impervious, Inflow Depth > 1.63" for 2-yr Storm event

Inflow = 0.81 cfs @ 12.08 hrs, Volume= 0.054 af

Outflow = 0.23 cfs @ 12.44 hrs, Volume= 0.054 af, Atten= 72%, Lag= 21.7 min

Discarded = 0.23 cfs @ 12.44 hrs, Volume= 0.054 af Primary = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 308.56' @ 12.44 hrs Surf.Area= 1,083 sf Storage= 529 cf

Plug-Flow detention time= 14.6 min calculated for 0.053 af (100% of inflow)

Center-of-Mass det. time= 14.4 min ( 802.4 - 788.0 )

Volume	Invert	Avail.Sto	rage Storage l	Description		
#1	308.00'	1,7	88 cf Custom	Stage Data (Coni	c)Listed below (F	Recalc)
Elevation (fee		urf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)	
308.0 309.0	00	810 1,325	0 1,057	0 1,057	810 1,338	
309.5	00	1,602	731	1,788	1,623	
Device	Routing	Invert	Outlet Devices	i		
#1	Discarded	308.00'	9.070 in/hr Ex	filtration over We	etted area	
#2	Primary	309.25'		0' breadth Broad-		•
			` ,			1.60 1.80 2.00
				0 4.00 4.50 5.00		
				2.38 2.54 2.69		2.65 2.66 2.66
			2.68 2.72 2.7	3 2.76 2.79 2.88	3.07 3.32	

**Discarded OutFlow** Max=0.23 cfs @ 12.44 hrs HW=308.56' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.23 cfs)

Primary OutFlow Max=0.00 cfs @ 5.00 hrs HW=308.00' (Free Discharge) 2=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

#### **Summary for Link AP-1: Analysis Point #1**

Inflow Area = 1.487 ac, 70.76% Impervious, Inflow Depth > 0.66" for 2-yr Storm event

Inflow = 1.23 cfs @ 12.08 hrs, Volume= 0.082 af

Primary = 1.23 cfs @ 12.08 hrs, Volume= 0.082 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Type III 24-hr 10-yr Storm Rainfall=4.60"

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Time span=5.00-20.00 hrs, dt=0.05 hrs, 301 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment SC-1A: Perimeter Runoff Area=36,666 sf 68.23% Impervious Runoff Depth>2.29"

Tc=5.0 min CN=79 Runoff=2.43 cfs 0.161 af

Subcatchment SC-1B1: Roof Runoff Area=10,924 sf 64.08% Impervious Runoff Depth>2.13"

Tc=5.0 min CN=77 Runoff=0.67 cfs 0.044 af

SubcatchmentSC-1B2: Parking Lot Runoff Area=17,180 sf 80.42% Impervious Runoff Depth>2.91"

Tc=5.0 min CN=86 Runoff=1.42 cfs 0.096 af

Pond 1BP1: Infiltration Basin #1 Peak Elev=308.41' Storage=378 cf Inflow=0.67 cfs 0.044 af

Discarded=0.23 cfs 0.044 af Primary=0.00 cfs 0.000 af Outflow=0.23 cfs 0.044 af

Pond 1CP1: Infiltration Basin #2 Peak Elev=309.14' Storage=1,247 cf Inflow=1.42 cfs 0.096 af

Discarded=0.30 cfs 0.096 af Primary=0.00 cfs 0.000 af Outflow=0.30 cfs 0.096 af

Link AP-1: Analysis Point #1 Inflow=2.43 cfs 0.161 af

Primary=2.43 cfs 0.161 af

Type III 24-hr 10-yr Storm Rainfall=4.60"

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#### **Summary for Subcatchment SC-1A: Perimeter**

Runoff 2.43 cfs @ 12.08 hrs, Volume= 0.161 af, Depth> 2.29"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 10-yr Storm Rainfall=4.60"

Ar	ea (sf)	CN	Description					
	131	32	Woods/gras	s comb., G	Good, HSG A			
1	14,767	98	Paved road	s w/curbs 8	& sewers, HSG A			
1	11,517	39	Pasture/gra	ssland/rang	ge, Good, HSG A			
1	10,251	98	Paved parki	ng, HSG A				
3	36,666	79	Weighted Average					
1	11,648		31.77% Pervious Area					
2	25,018		68.23% Imp	ervious Are	ea			
Tc	Length	Slope	,	Capacity	Description			
(min)	(feet)	(ft/ft	) (ft/sec)	(cfs)				
5.0					Direct Entry, 5 minutes Minumum			

#### Summary for Subcatchment SC-1B1: Roof

0.67 cfs @ 12.08 hrs, Volume= 0.044 af, Depth> 2.13" Runoff

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 10-yr Storm Rainfall=4.60"

Are	ea (sf)	CN I	Description					
	7,000	98 I	Roofs, HSG	i A				
	3,924	39 I	Pasture/gra	ssland/rang	ge, Good, HSG A			
1	10,924	77 \	Weighted Average					
	3,924	;	35.92% Pervious Area					
	7,000	(	34.08% Imp	ervious Are	ea			
Тс	Length	Slope	Velocity	Capacity	Description			
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)				
5.0					Direct Entry, 5 minutes min			

Direct Entry, 5 minutes min

#### **Summary for Subcatchment SC-1B2: Parking Lot**

1.42 cfs @ 12.07 hrs, Volume= 0.096 af. Depth> 2.91" Runoff

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 10-yr Storm Rainfall=4.60"

Type III 24-hr 10-yr Storm Rainfall=4.60"

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Α	rea (sf)	CN	Description						
	13,816	98	Paved parking, HSG A						
	3,364	39	Pasture/grassland/range, Good, HSG A						
	17,180	86	Veighted Average						
	3,364		19.58% Pervious Area						
	13,816		80.42% Impervious Area						
Tc	Length	Slope							
(min)	(feet)	(ft/ft	) (ft/sec) (cfs)						

5.0

Direct Entry, 5 minutes minumum

#### **Summary for Pond 1BP1: Infiltration Basin #1**

Inflow Area = 0.251 ac, 64.08% Impervious, Inflow Depth > 2.13" for 10-yr Storm event 
Inflow = 0.67 cfs @ 12.08 hrs, Volume= 0.044 af 
Outflow = 0.23 cfs @ 12.39 hrs, Volume= 0.044 af, Atten= 66%, Lag= 18.7 min 
Discarded = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 308.41' @ 12.39 hrs Surf.Area= 1,089 sf Storage= 378 cf

Plug-Flow detention time= 10.6 min calculated for 0.044 af (100% of inflow)

Center-of-Mass det. time= 10.3 min (806.1 - 795.7)

Volume	Invert	Avail.Sto	rage Storage	Description		
#1	308.00'	3,6	45 cf Custom	Stage Data (Coni	<b>c)</b> Listed below (F	Recalc)
Elevatio		ırf.Area	Inc.Store	Cum.Store	Wet.Area	
(fee	[)	(sq-ft)	(cubic-feet)	(cubic-feet)	(sq-ft)	
308.0	0	748	0	0	748	
309.0	0	1,683	1,184	1,184	1,691	
310.0	0	3,332	2,461	3,645	3,349	
Device	Routing	Invert	Outlet Devices	5		_
#1	Discarded	308.00'	9.070 in/hr Ex	filtration over We	etted area	
#2	Primary	309.50'	10.0' long x 4	4.0' breadth Broad	d-Crested Recta	ngular Weir
	,					10 1.60 1.80 2.00
			` ,	50 4.00 4.50 5.00		
			Coef. (English	i) 2.38 2.54 2.69 73 2.76 2.79 2.88	2.68 2.67 2.67	2.65 2.66 2.66

**Discarded OutFlow** Max=0.23 cfs @ 12.39 hrs HW=308.41' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.23 cfs)

Primary OutFlow Max=0.00 cfs @ 5.00 hrs HW=308.00' (Free Discharge) 2=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Type III 24-hr 10-yr Storm Rainfall=4.60"

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#### **Summary for Pond 1CP1: Infiltration Basin #2**

Inflow Area = 0.394 ac, 80.42% Impervious, Inflow Depth > 2.91" for 10-yr Storm event

Inflow = 1.42 cfs @ 12.07 hrs, Volume= 0.096 af

Outflow = 0.30 cfs @ 12.50 hrs, Volume= 0.096 af, Atten= 79%, Lag= 25.6 min

Discarded = 0.30 cfs @ 12.50 hrs, Volume= 0.096 af Primary = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 309.14' @ 12.50 hrs Surf.Area= 1,400 sf Storage= 1,247 cf

Plug-Flow detention time= 31.4 min calculated for 0.095 af (100% of inflow)

Center-of-Mass det. time= 31.2 min (805.6 - 774.4)

Volume	Inver	t Avail.Sto	rage Storage	Description		
#1	#1 308.00' 1,78		88 cf Custom	Stage Data (Con	<b>ic)</b> Listed below (	Recalc)
Elevation (fee		Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)	
308.0 309.0 309.0	00	810 1,325 1,602	0 1,057 731	0 1,057 1,788	810 1,338 1,623	
Device	Routing	Invert	Outlet Devices	S		
#1 #2	Discarded Primary	308.00' 309.25'	6.0' long x 4. Head (feet) 0 2.50 3.00 3.5 Coef. (English	xfiltration over We .0' breadth Broad .20 0.40 0.60 0.8 50 4.00 4.50 5.00 a) 2.38 2.54 2.69 73 2.76 2.79 2.88	-Crested Rectar 30 1.00 1.20 1. 0 5.50 2.68 2.67 2.67	40 1.60 1.80 2.00

**Discarded OutFlow** Max=0.30 cfs @ 12.50 hrs HW=309.14' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.30 cfs)

Primary OutFlow Max=0.00 cfs @ 5.00 hrs HW=308.00' (Free Discharge) 2=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

#### **Summary for Link AP-1: Analysis Point #1**

Inflow Area = 1.487 ac, 70.76% Impervious, Inflow Depth > 1.30" for 10-yr Storm event

Inflow = 2.43 cfs @ 12.08 hrs, Volume= 0.161 af

Primary = 2.43 cfs @ 12.08 hrs, Volume= 0.161 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Type III 24-hr 25-yr Storm Rainfall=5.80"

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Time span=5.00-20.00 hrs, dt=0.05 hrs, 301 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment SC-1A: Perimeter Runoff Area=36,666 sf 68.23% Impervious Runoff Depth>3.28"

Tc=5.0 min CN=79 Runoff=3.45 cfs 0.230 af

Subcatchment SC-1B1: Roof Runoff Area=10,924 sf 64.08% Impervious Runoff Depth>3.09"

Tc=5.0 min CN=77 Runoff=0.97 cfs 0.065 af

Subcatchment SC-1B2: Parking Lot Runoff Area=17,180 sf 80.42% Impervious Runoff Depth>3.98"

Tc=5.0 min CN=86 Runoff=1.92 cfs 0.131 af

Pond 1BP1: Infiltration Basin #1 Peak Elev=308.67' Storage=682 cf Inflow=0.97 cfs 0.065 af

Discarded=0.28 cfs 0.064 af Primary=0.00 cfs 0.000 af Outflow=0.28 cfs 0.064 af

Pond 1CP1: Infiltration Basin #2 Peak Elev=309.35' Storage=1,554 cf Inflow=1.92 cfs 0.131 af

Discarded=0.32 cfs 0.120 af Primary=0.45 cfs 0.010 af Outflow=0.77 cfs 0.131 af

Link AP-1: Analysis Point #1 Inflow=3.45 cfs 0.240 af

Primary=3.45 cfs 0.240 af

Type III 24-hr 25-yr Storm Rainfall=5.80"

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#### **Summary for Subcatchment SC-1A: Perimeter**

Runoff 3.45 cfs @ 12.08 hrs, Volume= 0.230 af, Depth> 3.28"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 25-yr Storm Rainfall=5.80"

Ar	rea (sf)	CN	Description				
	131	32	Woods/gras	s comb., G	Good, HSG A		
•	14,767	98	Paved road	s w/curbs &	& sewers, HSG A		
	11,517	39	Pasture/gra	ssland/rang	ge, Good, HSG A		
<u> </u>	10,251	98	Paved park	ng, HSG A			
;	36,666	79	Weighted Average				
•	11,648		31.77% Pervious Area				
	25,018		68.23% Imp	ervious Are	ea		
Тс	Length	Slope		Capacity	Description		
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)			
5.0					Direct Entry, 5 minutes Minumum		

#### **Summary for Subcatchment SC-1B1: Roof**

0.97 cfs @ 12.08 hrs, Volume= 0.065 af, Depth> 3.09" Runoff

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 25-yr Storm Rainfall=5.80"

Α	rea (sf)	CN	<u>Description</u>					
	7,000	98	Roofs, HSG A					
	3,924	39	asture/grassland/range, Good, HSG A					
	10,924	77	Weighted Average					
	3,924		35.92% Pervious Area					
	7,000		64.08% Impervious Area					
Тс	Length	Slope	,	Capacity	Description			
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)				
5.0					Direct Entry, 5 minutes min			

Direct Entry, 5 minutes min

#### **Summary for Subcatchment SC-1B2: Parking Lot**

1.92 cfs @ 12.07 hrs, Volume= 0.131 af, Depth> 3.98" Runoff

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 25-yr Storm Rainfall=5.80"

Type III 24-hr 25-yr Storm Rainfall=5.80"

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Α	rea (sf)	CN	Description				
	13,816	98	Paved parking, HSG A				
	3,364	39	Pasture/grassland/range, Good, HSG A				
	17,180	86	Weighted Average				
	3,364		19.58% Pervious Area				
	13,816		80.42% Impervious Area				
_							
Тс	Length	Slope					
(min)	(feet)	(ft/ft	t) (ft/sec) (cfs)				

5.0

Direct Entry, 5 minutes minumum

#### **Summary for Pond 1BP1: Infiltration Basin #1**

0.251 ac, 64.08% Impervious, Inflow Depth > 3.09" for 25-yr Storm event Inflow Area = Inflow 0.97 cfs @ 12.08 hrs, Volume= 0.065 af 0.28 cfs @ 12.43 hrs, Volume= Outflow 0.064 af, Atten= 71%, Lag= 21.3 min 0.28 cfs @ 12.43 hrs, Volume= Discarded = 0.064 af Primary 0.00 cfs @ 5.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 308.67' @ 12.43 hrs Surf.Area= 1,329 sf Storage= 682 cf

Plug-Flow detention time= 17.1 min calculated for 0.064 af (100% of inflow)

Center-of-Mass det. time= 16.9 min (804.2 - 787.3)

Volume	Invert	Avail.Sto	rage Storage	Description		
#1	308.00'	3,6	45 cf Custom	Stage Data (Coni	<b>c)</b> Listed below (R	lecalc)
Elevation (fee		ırf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)	
308.0	00	748	0	0	748	
309.0	00	1,683	1,184	1,184	1,691	
310.0	00	3,332	2,461	3,645	3,349	
Device	Routing	Invert	Outlet Devices	<b>S</b>		
#1	Discarded	308.00'	9.070 in/hr Ex	filtration over We	tted area	
#2	Primary	309.50'	10.0' long x 4	I.0' breadth Broad	I-Crested Rectar	ngular Weir
			Head (feet) 0.	20 0.40 0.60 0.8	0 1.00 1.20 1.4	0 1.60 1.80 2.00
			2.50 3.00 3.5	0 4.00 4.50 5.00	5.50	
				) 2.38 2.54 2.69		2.65 2.66 2.66
			2.68 2.72 2.7	3 2.76 2.79 2.88	3.07 3.32	

**Discarded OutFlow** Max=0.28 cfs @ 12.43 hrs HW=308.66' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.28 cfs)

Primary OutFlow Max=0.00 cfs @ 5.00 hrs HW=308.00' (Free Discharge) 2=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Type III 24-hr 25-yr Storm Rainfall=5.80"

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#### Summary for Pond 1CP1: Infiltration Basin #2

Inflow Area = 0.394 ac, 80.42% Impervious, Inflow Depth > 3.98" for 25-yr Storm event

Inflow = 1.92 cfs @ 12.07 hrs, Volume= 0.131 af

Outflow = 0.77 cfs @ 12.30 hrs, Volume= 0.131 af, Atten= 60%, Lag= 13.6 min

Discarded = 0.32 cfs @ 12.30 hrs, Volume= 0.120 af Primary = 0.45 cfs @ 12.30 hrs, Volume= 0.010 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 309.35' @ 12.30 hrs Surf.Area= 1,516 sf Storage= 1,554 cf

Plug-Flow detention time= 33.3 min calculated for 0.130 af (100% of inflow)

Center-of-Mass det. time= 33.0 min ( 799.9 - 766.9 )

Volume	Inver	t Avail.Sto	orage Storage Description				
#1	308.00	1,7	88 cf Custom	Stage Data (Con	<b>ic)</b> Listed below (	Recalc)	
Elevation (fee		Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)		
308.0 309.0 309.0	00	810 1,325 1,602	0 1,057 731	0 1,057 1,788	810 1,338 1,623		
Device	Routing	Invert	Outlet Devices	S			
#1 #2	Discarded Primary	308.00' 309.25'	6.0' long x 4. Head (feet) 0 2.50 3.00 3.5 Coef. (English	xfiltration over We .0' breadth Broad .20 0.40 0.60 0.8 50 4.00 4.50 5.00 a) 2.38 2.54 2.69 73 2.76 2.79 2.88	-Crested Rectar 30 1.00 1.20 1. 0 5.50 2.68 2.67 2.67	40 1.60 1.80 2.00	

**Discarded OutFlow** Max=0.32 cfs @ 12.30 hrs HW=309.35' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.32 cfs)

Primary OutFlow Max=0.45 cfs @ 12.30 hrs HW=309.35' (Free Discharge) 2=Broad-Crested Rectangular Weir (Weir Controls 0.45 cfs @ 0.75 fps)

#### **Summary for Link AP-1: Analysis Point #1**

Inflow Area = 1.487 ac, 70.76% Impervious, Inflow Depth > 1.94" for 25-yr Storm event

Inflow = 3.45 cfs @ 12.08 hrs, Volume= 0.240 af

Primary = 3.45 cfs @ 12.08 hrs, Volume= 0.240 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

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April 3, 2020

Jeffrey T. Read, P.E.
Civil Engineer
Sevee & Maher Engineers, Inc.
4 Blanchard Road
Cumberland, ME 04021

#### RE: WINDHAM PEER REVIEW RESPONSE

#### INTRODUCTION

This is written to respond to peer review comments provided by Randy Dunton, P.E. PTOE at Gorrill Palmer (GP) in an email dated March 31, 2020 to the Town of Windham regarding the traffic analysis we prepared for the new Bangor Savings Bank, dated March 16, 2020. The original GP comments are repeated below along with our response in italics:

The study was well done and generally followed acceptable standards and methodology. This review included the following:

1. GP agrees with the use of the 10<sup>th</sup> edition of the Institute of Transportation Engineers' (ITE) *Trip Generation* manual. GP agrees that the most representative Land Use Codes (LUC) were used for the existing/proposed office area (LUC 710 – General Office) and proposed bank area (LUC 912 – Drive-In Bank). As mentioned in the report, there is not a representative land use code for retail. The LUC used (820 – Shopping Center) for the existing 938 SF retail building (iPhone repair store), in our opinion, does not accurately represent the use; however, based on the size of the retail building and potential other options that may have been used, changing this trip generation would not be expected to change any of the conclusions of the study.

No response necessary.

2. GP agrees with the existing trip generation for office and retail space.

No response necessary.

3. GP agrees with the proposed trip generation for office and bank development, with the exception of the PM Peak Hour of the Generator for the Bank, which we could not reproduce. Since the adjacent street trip generation is used for the remainder of the



study and not the trip generation of the generator, the conclusions of the study would not change.

No response necessary.

4. GP agrees with the methods used to seasonally and annually adjust the traffic counts to a 2021 no-build condition.

No response necessary.

- 5. The Trip Assignments provided on Figure 4 do not appear to add from a roadway network perspective. The volumes entering and exiting the site appear correct, but the volumes flowing through the rest of the system do not appear to agree. Resulting changes to other figures or capacity analysis should be revisited.
  - GP is correct. There were two typos in the diagram involving the trip assignments at the Route 302 intersection. The corrected diagram is attached. Note that it did not impact the Abby Road intersection volumes so it had no impact on the analysis since the Route 302 intersection was not analyzed.
- 6. The results of the traffic analysis for level of service are correctly identified from the simulation to the report (see above comment for possible changes). The applicant has noted that the level of service of one <u>approach</u> does change from an "E" to an "F". Per the Town of Windham Ordinance, if the level of service of an <u>intersection</u> is an "E" or worse, the level of service should not decrease because of the additional traffic. The overall intersection level of service is not provided. The applicants traffic engineer should provide a response to this item. This criteria can be waived by the Board.

The analysis originally was performed utilizing Synchro and the HCM approach. This approach only calculates level of service (LOS) for the minor, opposed movements at unsignalized intersections. To determine overall intersection LOS Sewall ran Synchro/SimTraffic, the average of five simulation runs. These LOS ranges are described below for reference:

#### **Unsignalized Intersection Level of Service**

<u>LOS</u>	<u>Delay Range</u>
A	< = 10.0 seconds
В	$> 10.0$ and $\leq 15.0$
C	$> 15.0$ and $\leq 25.0$
D	$> 25.0$ and $\leq 35.0$
E	$> 35.0$ and $\leq 50.0$
F	> 50.0

ATFIC Company



The results by approach and for the overall intersection are attached to this memorandum and summarized below:

	Route 115 and Abby Road			
	AM Peak Hour Lev	els of Service		
	2021	2021		
Approach/Movement	<u>No-Build</u>	<u>Build</u>		
Eastbound Route 115	A (1.2)	A (1.0)		
Westbound Route 115	A (0.2)	A (0.3)		
Northbound Walgreens	A (5.3)	A (5.0)		
Southbound Abby Road	A (3.8)	A (4.6)		
Overall Intersection	A (1.3)	A (1.2)		
	PM Peak Hour Leve	els of Service		
	2021	2021		
Approach/Movement	No-Build	<u>Build</u>		
Eastbound Route 115	A (2.2)	A (3.5)		
Westbound Route 115	A (0.6)	A (1.1)		
Northbound Walgreens	D (26.8)	C (24.4)		
Southbound Abby Road	D (25.1)	E (40.0)		
Overall Intersection	A (3.2)	A (4.2)		

As seen in the above tables, SimTraffic gave much better results than the Synchro HCM approach. These results similarly show that there are no capacity concerns in the AM peak hour. The SimTraffic results show no constraints on the northbound Walgreens approach which HCM showed to be failing. The results show that the Abby Road approach will operate at LOS "E" overall and not "F". Further, and most importantly, the analysis shows that the overall intersection functions at LOS "A" during both peak hour periods so there are no concerns in regard to meeting the ordinance which prohibits LOS "E" or lower for an <u>intersection</u>. The minor improvements shown for some approaches between No Build and Build conditions is simply due to the low approach volumes and the variability in the SimTraffic runs.



7. It should be noted that the results of the capacity analysis provided in the study are most likely not accurate due to the impacts on traffic flow from the adjacent signalized intersection. However, the results provided in the study can be used as an indicator of the level of impact of the project on the intersection.

Sewall concurs with this comment. Without analysis of the Route 302 intersection, which this project will have no measurable impact on, it isn't possible to truly model operations at Abby Road since signal queues can potentially interfere with Abby Road movements. As noted by GP the intent was to simply show the level of impact to Abby Road.

8. GP agrees with the safety analysis for High Crash Locations and mitigation tactics to improve these locations. This includes additional striping and signage to not block the intersection.

No response necessary.

9. It should be noted that the proposed access management measures (reduction of driveways and restriction of movements) to this corner should have a net positive impact to the overall area, reducing potential conflicts and improving safety. However, the applicant should address the Town's double frontage requirements. We recommend the applicant revisit the channelization of the proposed driveways to improve the enforcement of right turn movements only. As currently shown at both driveways, the restrictions do not appear to be prohibitive enough.

It is understood that Sevee & Maher will be revising the site plan and addressing this site access and design comment.

As always, please do not hesitate to contact me if you or the Town of Windham have any additional questions or concerns.

DIANE

MORABITO

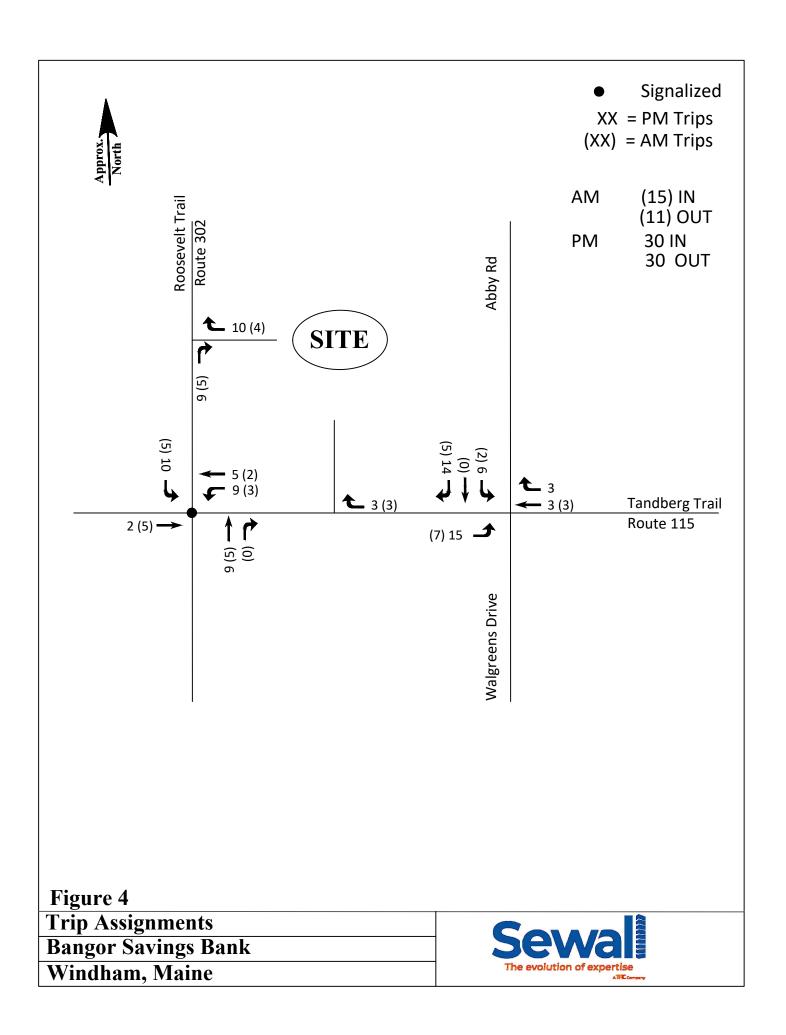
No. 5077

VICENSED ON FNORTH

Sincerely,

Diane W. Morabito, P.E. PTOE Vice President Traffic Engineering

)iane W. Moras.



#### Summary of All Intervals

					-		
Run Number	11	2	3	4	5	Avg	
Start Time	6:57	6:57	6:57	6:57	6:57	6:57	
End Time	7:10	7:10	7:10	7:10	7:10	7:10	
Total Time (min)	13	13	13	13	13	13	
Time Recorded (min)	10	10	10	10	10	10	
# of Intervals	2	2	2	2	2	2	
# of Recorded Intervals	1	1	1	1	1	1	
Vehs Entered	226	236	209	227	204	220	
Vehs Exited	232	231	207	226	201	220	
Starting Vehs	10	9	8	12	6	9	
Ending Vehs	4	14	10	13	9	9	
Travel Distance (mi)	49	50	44	48	44	47	
Travel Time (hr)	1.8	1.8	1.6	1.8	1.6	1.7	
Total Delay (hr)	0.1	0.1	0.1	0.1	0.1	0.1	
Total Stops	12	11	14	11	9	12	
Fuel Used (gal)	1.5	1.6	1.4	1.5	1.3	1.5	

#### Interval #0 Information Seeding

Start Time	6:57
End Time	7:00
Total Time (min)	3
Volumes adjusted by Growth Fa	actors.
No data recorded this interval.	

Interval #1 Information Recording

Start Time	7:00
End Time	7:10
Total Time (min)	10
Volumes adjusted by Growth	n Factors.

- 11	1	2	3	4	5	Avg	
Run Number	ı			227	204	220	
Vehs Entered	226	236	209	227			
Vehs Exited	232	231	207	226	201	220	
Starting Vehs	10	9	8	12	6	9	
	4	14	10	13	9	9	
Ending Vehs	49	50	44	48	44	47	
Travel Distance (mi)					1.6	1.7	
Travel Time (hr)	1.8	1.8	1.6	1.8			
Total Delay (hr)	0.1	0.1	0.1	0.1	0.1	0.1	
	12	11	14	11	9	12	
Total Stops				1.5	1.3	1.5	
Fuel Used (gal)	1.5	1.6	1.4	1.0	1.0		

#### 3: Walgreens Dr/Abby Road & Route 115 Performance by approach

Approach	EB	WB	NB	SB	All
Denied Delay (hr)	0.0	0.0	0.0	0.0	0.0
Denied Del/Veh (s)	0.5	0.1	4.6	0.1	0.4
Total Delay (hr)	0.0	0.0	0.0	0.0	0.1
Total Del/Veh (s)	1.2	0.2	5.3	3.8	0.9
Stop Delay (hr)	0.0	0.0	0.0	0.0	0.0
Stop Del/Veh (s)	0.1	0.0	4.9	3.7	0.2

#### **Total Network Performance**

Denied Delay (hr)	0.0	
Denied Del/Veh (s)	0.4	
Total Delay (hr)	0.1	
Total Del/Veh (s)	1.3	
Stop Delay (hr)	0.0	
Stop Del/Veh (s)	0.2	

#### Summary of All Intervals

Run Number	1	2	3	4	5	Avg	
Start Time	6:57	6:57	6:57	6:57	6:57	6:57	
End Time	7:10	7:10	7:10	7:10	7:10	7:10	
Total Time (min)	13	13	13	13	13	13	
Time Recorded (min)	10	10	10	10	10	10	
# of Intervals	2	2	2	2	2	2	
# of Recorded Intervals	1	1	1	1	1	1	
Vehs Entered	237	246	224	222	222	231	
Vehs Exited	240	243	225	214	229	230	
Starting Vehs	13	6	12	4	14	9	
Ending Vehs	10	9	11	12	7	9	
Travel Distance (mi)	50	52	48	47	49	49	
Travel Time (hr)	1.9	1.9	1.7	1.7	1.8	1.8	
Total Delay (hr)	0.1	0.1	0.1	0.1	0.1	0.1	
Total Stops	18	12	8	10	10	12	
Fuel Used (gal)	1.6	1.6	1.5	1.4	1.5	1.5	

#### Interval #0 Information Seeding

Start Time	6:57
End Time	7:00
Total Time (min)	3
Volumes adjusted by Growth Factors	<b>S</b> .

No data recorded this interval.

#### Interval #1 Information Recording

Start Time	7:00
End Time	7:10
Total Time (min)	10
Volumes adjusted by Grov	wth Factors.

Totalines singuistry		^	2	4	5	Avg	
Run Number	1	2	3				
Vehs Entered	237	246	224	222	222	231	
Vehs Exited	240	243	225	214	229	230	
	13	6	12	4	14	9	
Starting Vehs	10	9	11	12	7	9	
Ending Vehs		52	48	47	49	49	
Travel Distance (mi)	50			1.7	1.8	1.8	
Travel Time (hr)	1.9	1.9	1.7		0.1	0.1	
Total Delay (hr)	0.1	0.1	0.1	0.1	and the second s		
Total Stops	18	12	8	10	10	12	
Fuel Used (gal)	1.6	1.6	1.5	1.4	1.5	1.5	

#### 3: Walgreens Dr/Abby Road & Route 115 Performance by approach

Approach	EB	WB	NB	SB	All
Denied Delay (hr)	0.0	0.0	0.0	0.0	0.0
Denied Del/Veh (s)	0.5	0.2	2.4	0.1	0.4
Total Delay (hr)	0.0	0.0	0.0	0.0	0.1
Total Del/Veh (s)	1.0	0.3	5.0	4.6	8.0
Stop Delay (hr)	0.0	0.0	0.0	0.0	0.0
Stop Del/Veh (s)	0.1	0.0	4.5	4.5	0.2

#### Total Network Performance

0.0	
0.4	
0.1	
1.2	
0.0	
0.2	
	0.4 0.1 1.2 0.0

#### Summary of All Intervals

Run Number	1	2	3	4	5	Avg	
Start Time	6:57	6:57	6:57	6:57	6:57	6:57	
End Time	7:10	7:10	7:10	7:10	7:10	7:10	
Total Time (min)	13	13	13	13	13	13	
Time Recorded (min)	10	10	10	10	10	10	
# of Intervals	2	2	2	2	2	2	
# of Recorded Intervals	1	1	1	1	1	1.	
Vehs Entered	327	339	324	326	319	326	
Vehs Exited	329	338	328	321	326	328	
Starting Vehs	16	12	19	12	18	13	
Ending Vehs	14	13	15	17	11	13	
Travel Distance (mi)	70	73	69	69	69	70	
Travel Time (hr)	2.8	2.8	2.8	2.6	2.7	2.8	
Total Delay (hr)	0.4	0.3	0.4	0.2	0.4	0.3	
Total Stops	41	23	25	11	29	23	
Fuel Used (gal)	2.4	2.3	2.3	2.2	2.3	2.3	

#### Interval #0 Information Seeding

Start Time	6:57
End Time	7:00
Total Time (min)	3
Volumes adjusted by Growth I	actors.
No data recorded this interval.	

#### Interval #1 Information Recording

Start Time	7:00
End Time	7:10
Total Time (min)	10
Volumes adjusted by Growth Fac	ctors.

Run Number	1	2	3	4	5	Avg	
Vehs Entered	327	339	324	326	319	326	
Vehs Exited	329	338	328	321	326	328	
Starting Vehs	16	12	19	12	18	13	
Ending Vehs	14	13	15	17	11	13	
Travel Distance (mi)	70	73	69	69	69	70	
Travel Time (hr)	2.8	2.8	2.8	2.6	2.7	2.8	
Total Delay (hr)	0.4	0.3	0.4	0.2	0.4	0.3	
Total Stops	41	23	25	11	29	23	
Fuel Used (gal)	2.4	2.3	2.3	2.2	2.3	2.3	

#### 3: Walgreens Dr/Abby Road & Route 115 Performance by approach

Approach	EB	WB	NB	SB	All
Denied Delay (hr)	0.0	0.0	0.0	0.0	0.0
Denied Del/Veh (s)	0.8	0.2	2.5	0.2	0.5
Total Delay (hr)	0.1	0.0	0.1	0.0	0.2
Total Del/Veh (s)	2.2	0.6	26.8	25.1	2.5
Stop Delay (hr)	0.0	0.0	0.1	0.0	0.1
Stop Del/Veh (s)	0.5	0.1	25.5	24.7	1.5

#### **Total Network Performance**

Denied Delay (hr)	0.0	
Denied Del/Veh (s)	0.5	
Total Delay (hr)	0.3	
Total Del/Veh (s)	3.2	
Stop Delay (hr)	0.1	
Stop Del/Veh (s)	1.5	

#### Summary of All Intervals

Run Number	1	2	3	4	5	Avg	
Start Time	6:57	6:57	6:57	6:57	6:57	6:57	
End Time	7:10	7:10	7:10	7:10	7:10	7:10	
Total Time (min)	13	13	13	13	13	13	
Time Recorded (min)	10	10	10	10	10	10	
# of Intervals	2	2	2	2	2	2	
# of Recorded Intervals	1	1	1	1	1	1	
Vehs Entered	312	347	339	338	344	335	
Vehs Exited	324	346	337	332	341	336	
Starting Vehs	19	11	17	11	14	13	
Ending Vehs	7	12	19	17	17	13	
Travel Distance (mi)	67	74	71	71	73	71	
Travel Time (hr)	2.7	2.9	3.0	2.7	3.2	2.9	
Total Delay (hr)	0.4	0.4	0.5	0.3	0.7	0.5	
Total Stops	40	25	53	25	44	36	
Fuel Used (gal)	2.3	2.4	2.4	2.3	2.5	2.4	

Interval #0 Information Seeding

Start Time	6:57
End Time	7:00
Total Time (min)	3
Volumes adjusted by Growth F	actors.
No data recorded this interval.	

Interval #1 Information Recording

Start Time	7:00
End Time	7:10
Total Time (min)	10
Volumes adjusted by Growth F	actors.

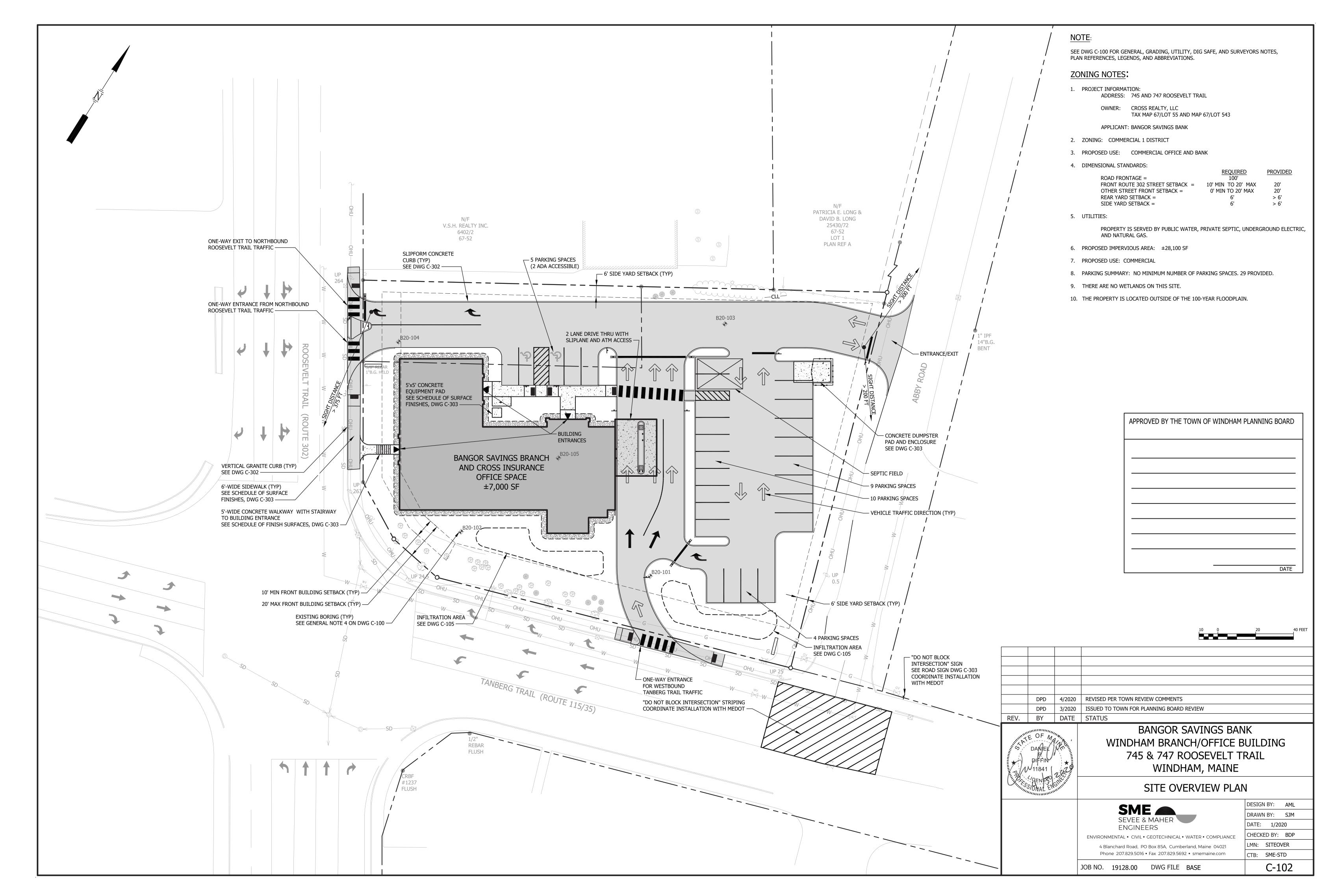
Run Number	1	2	3	4	5	Avg	
Vehs Entered	312	347	339	338	344	335	
Vehs Exited	324	346	337	332	341	336	
	19	11	17	11	14	13	
Starting Vehs	7	12	19	17	17	13	
Ending Vehs Travel Distance (mi)	67	74	71	71	73	71	
Travel Time (hr)	2.7	2.9	3.0	2.7	3.2	2.9	
Total Delay (hr)	0.4	0.4	0.5	0.3	0.7	0.5	
Total Stops	40	25	53	25	44	36	
Fuel Used (gal)	2.3	2.4	2.4	2.3	2.5	2.4	

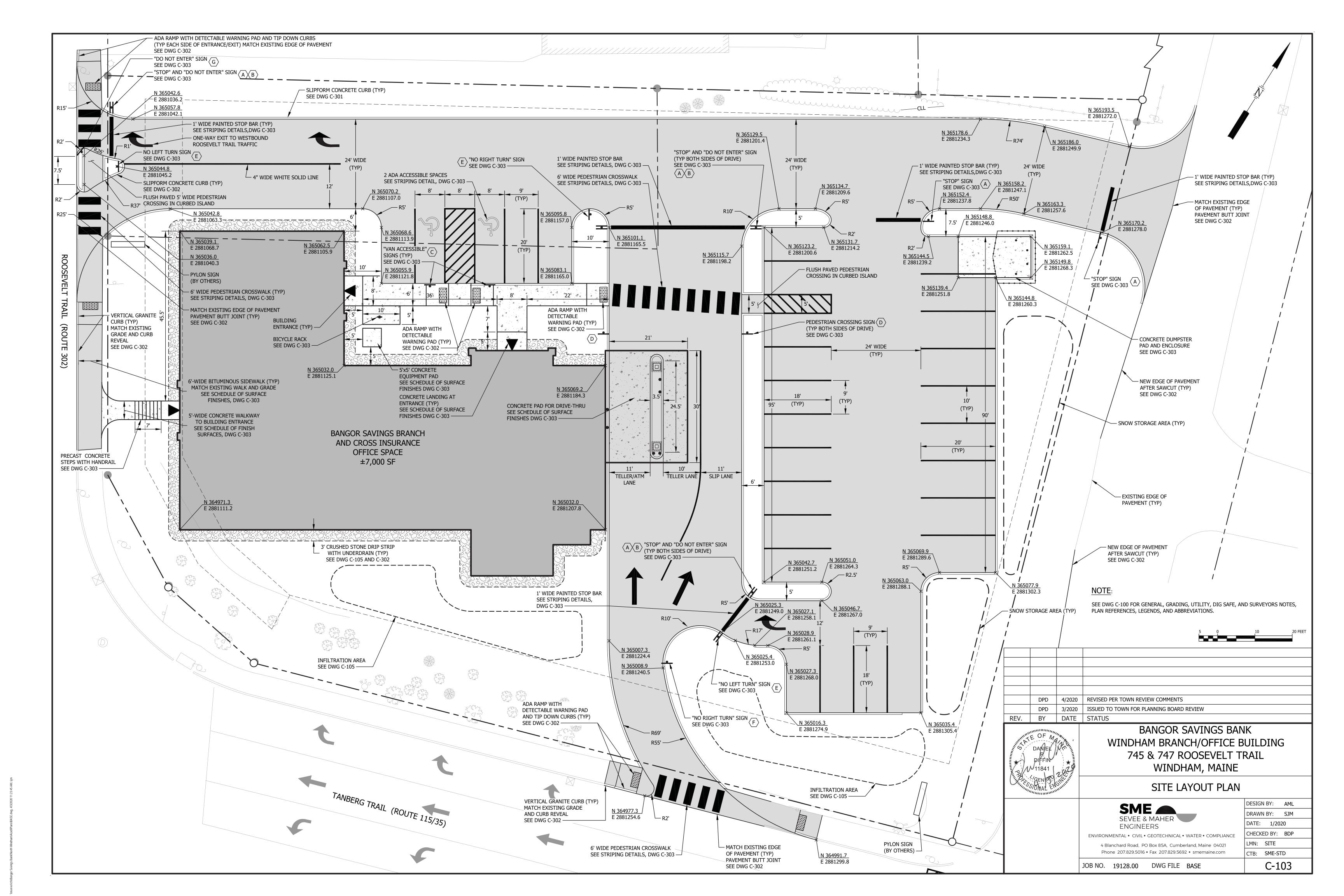
#### 3: Walgreens Dr/Abby Road & Route 115 Performance by approach

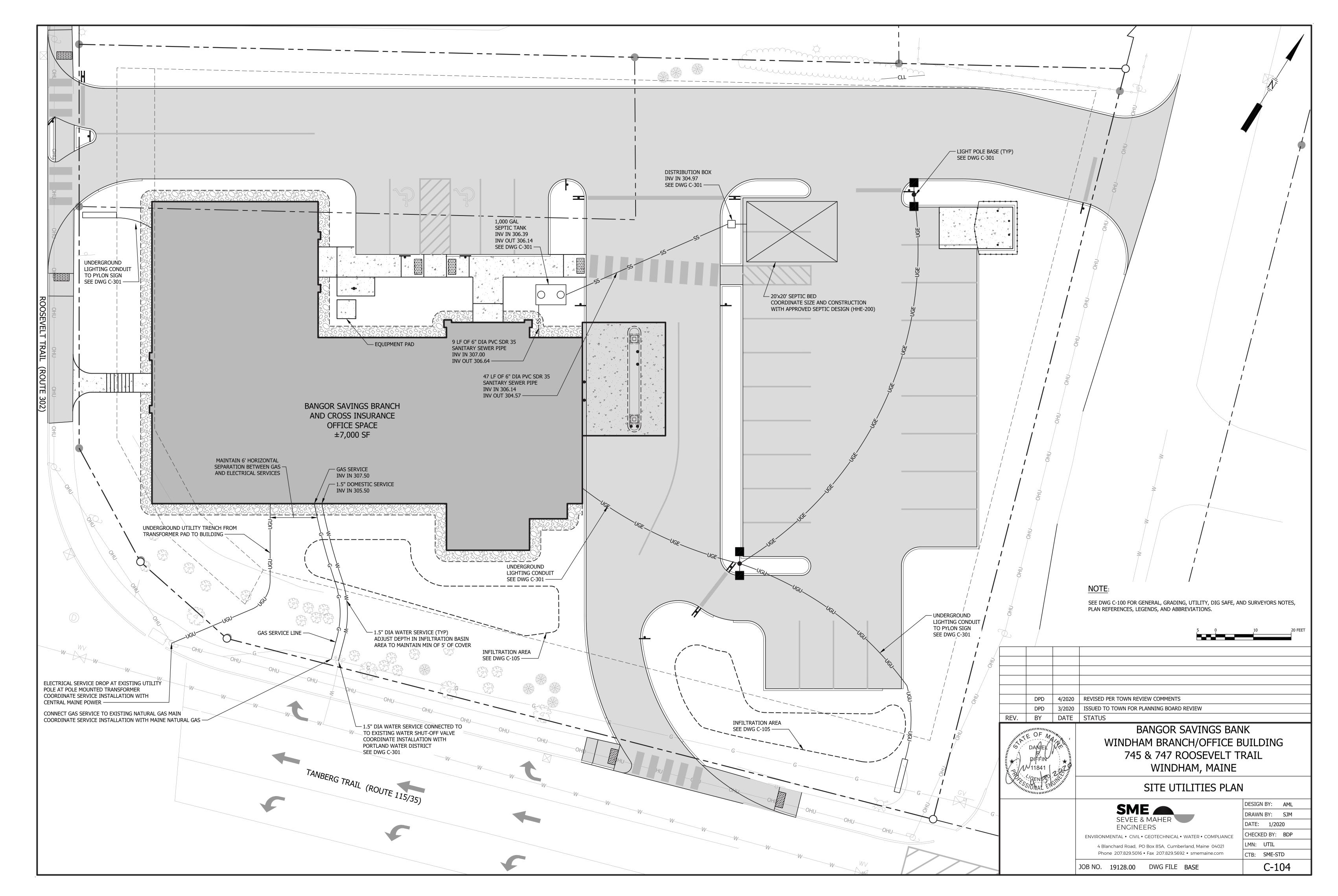
Approach	EB	WB	NB	SB	All	
Denied Delay (hr)	0.0	0.0	0.0	0.0	0.0	
Denied Del/Veh (s)	0.8	0.2	2.7	0.8	0.5	
Total Delay (hr)	0.1	0.1	0.0	0.1	0.3	
Total Del/Veh (s)	3.5	1.1	24.4	40.0	3.4	
Stop Delay (hr)	0.0	0.0	0.0	0.1	0.2	
Stop Del/Veh (s)	1.0	0.3	23.6	40.0	1.9	

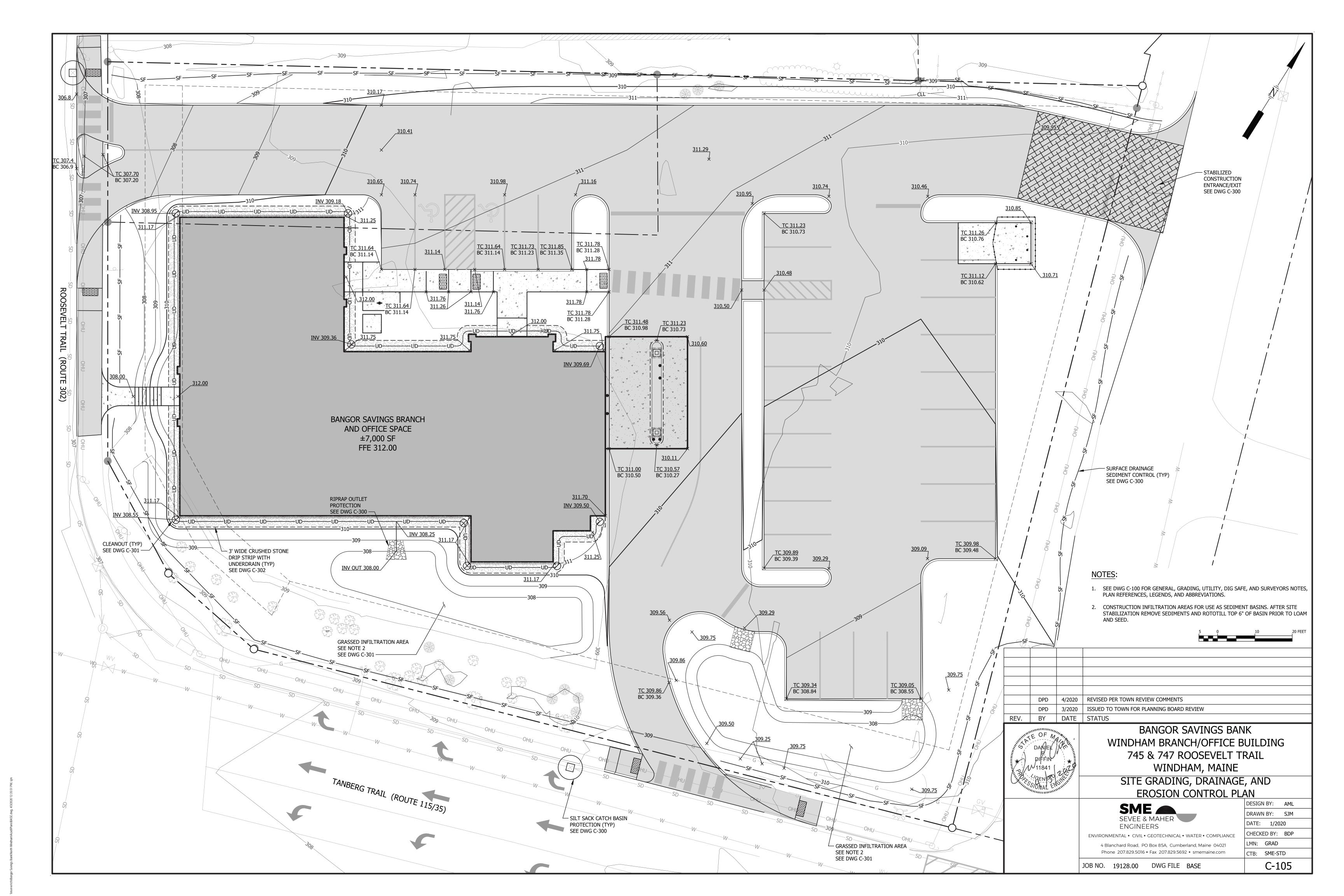
#### **Total Network Performance**

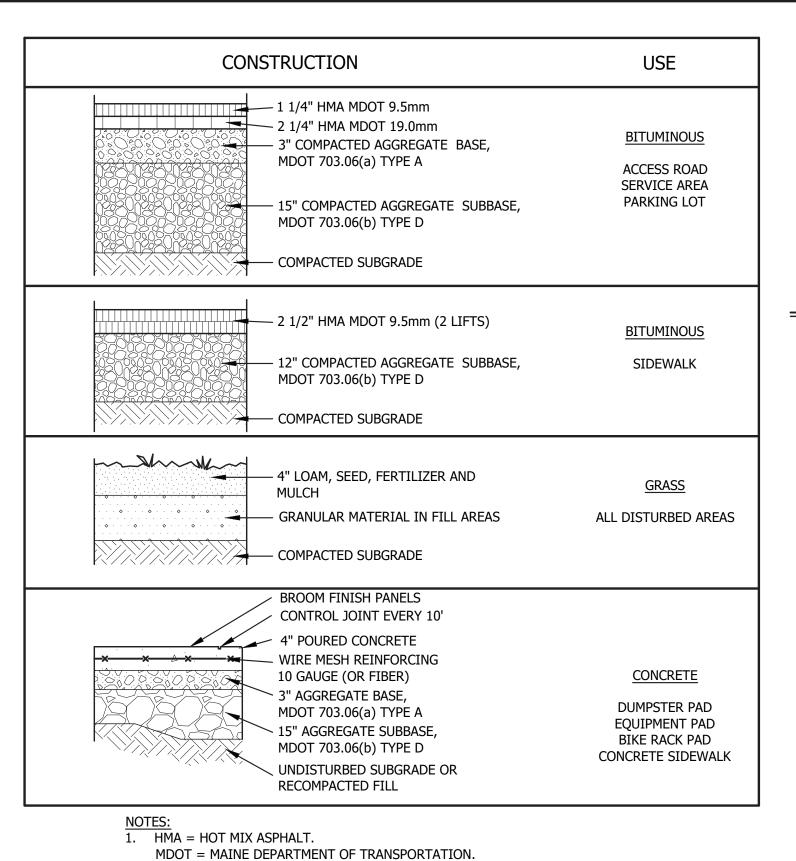
Denied Delay (hr)	0.0	
Denied Del/Veh (s)	0.5	
Total Delay (hr)	0.4	
Total Del/Veh (s)	4.2	
Stop Delay (hr)	0.2	
Stop Del/Veh (s)	1.9	





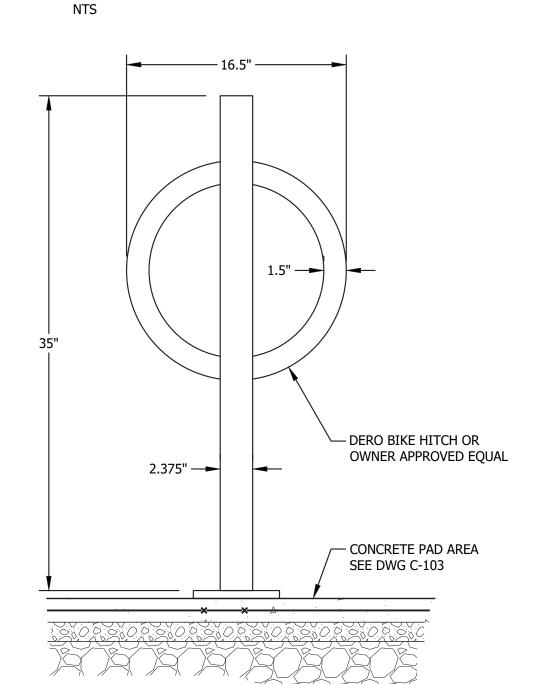


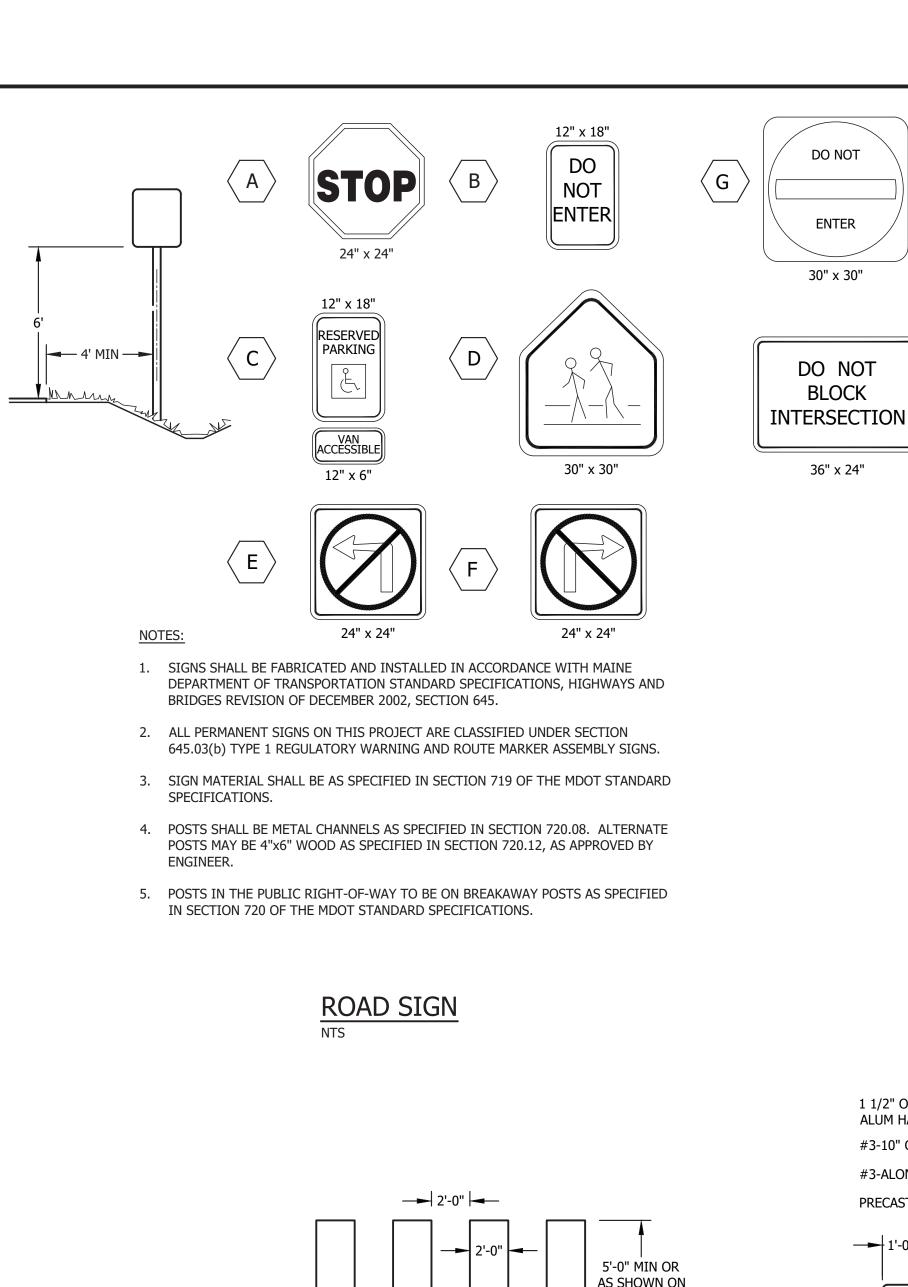




2. ALL COURSE THICKNESS AFTER FINAL COMPACTION.

### SCHEDULE OF SURFACE FINISHES





FULL BORDER —

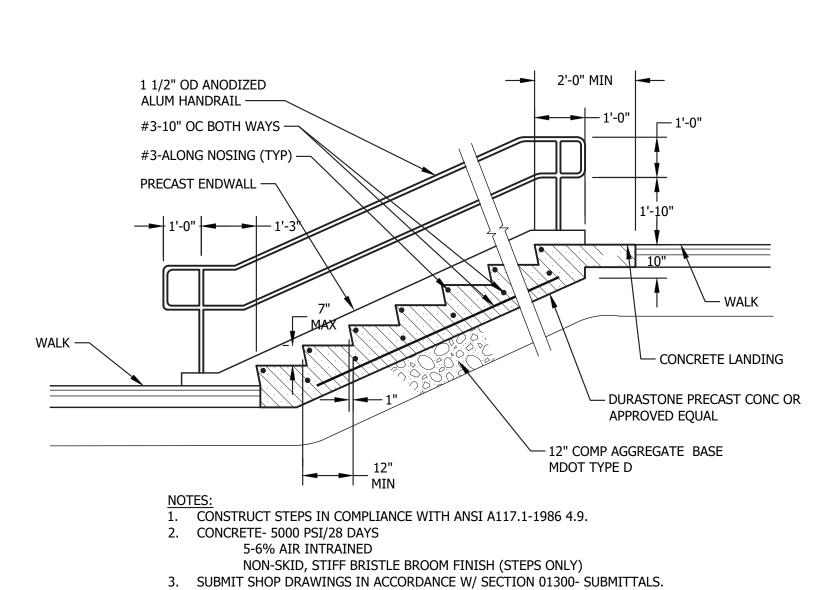
NO PARKING

LAYOUT AS

SHOWN ON PLAN

PARKING SPACE

ALL 4" STRIPES —



- 6" DIA SCH-40 GALVANIZED STEEL

FINISH PAINT: EPOXY COLOR BY

PRECAST CONCRETE BOLLARD BY PRECAST CONCRETE PRODUCTS

- BACKFILL WITH SUITABLE EXCAVATED

MATERIAL, COMPACTED SAND OR 3/4"

OF MAINE OR EQUAL

PIPE FILLED WITH CONCRETE

OWNER

FINISH GRADE

PRECAST STEEL BOLLARD

1'-6"

SLEEVES FOR HANDRAIL POSTS 2"~, 6" DEEP ADD 3RD SLEEVE MIDWAY AS REQ'D -1" CHAMFER ON ALL EXPOSED EDGES — - DURASTONE PRECAST CONC END WALL OR APPROVED EQUAL 7 3/4" — - 1"~ HOLES TO ALIGN W/ 3/4" THREADED INSERTS IN STEPS **ENDWALL ELEVATION** 

6" DIA BOLLARD (TYP) — SCREEN PANELS ARE TO BE FORTRESS BY ALUMI-GARD OR APPROVED EQUAL. 6" VERTICAL GRANITE CURB -DUMPSTER PAD AND ENCLOSURE DPD 4/2020 REVISED PER TOWN COMMENTS DPD | 3/2020 | ISSUED TO TOWN FOR PLANNING BOARD REVIEW REV. BY DATE STATUS BANGOR SAVINGS BANK WINDHAM BRANCH/OFFICE BUILDING 745 & 747 ROOSEVELT TRAIL WINDHAM, MAINE

**GATE DETAIL** 

SIDE ELEVATION

1'-0"±

1'-0" (TYP) -

1'-0"± —

POST (TYP) -

14'-0" EQ

THICKEN SLAB 4

- 2 - #4 CONT ALL SIDES

SIDES (TYP) ——

- 12" COMPACTED

AGGREGATE BASE

(CONT ALONG ALL

LOAMED SIDES)

1'-6" WIDE x 4" DEEP

CRUSHED STONE STRIP

- VARIES -

SECTIONS AND DETAILS

11'-0"

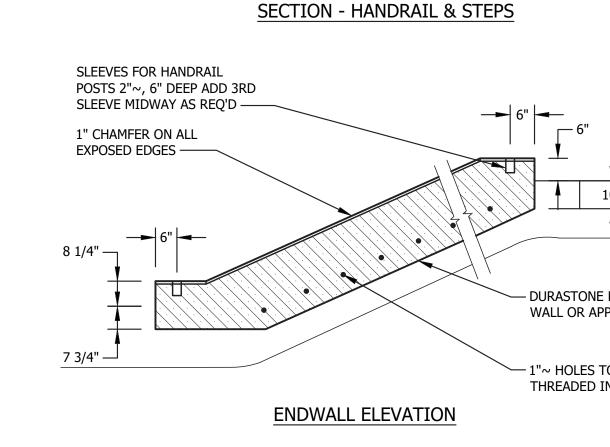
 $\triangleleft$ 

DESIGN BY: AML SME \_ DRAWN BY: SJM SEVEE & MAHER DATE: 10/2019 **ENGINEERS** CHECKED BY: BDP ENVIRONMENTAL • CIVIL • GEOTECHNICAL • WATER • COMPLIANCE \_MN: NONE 4 Blanchard Road, PO Box 85A, Cumberland, Maine 04021 Phone 207.829.5016 • Fax 207.829.5692 • smemaine.com CTB: SME-STD C-303 JOB NO. 19128.00 DWG FILE DETAILS

AS SHOWN ON PLAN CROSSWALK AS SHOWN ON PLAN ---STOP BAR --- 6'-0"x6'-0" BLUE BACKGROUND 

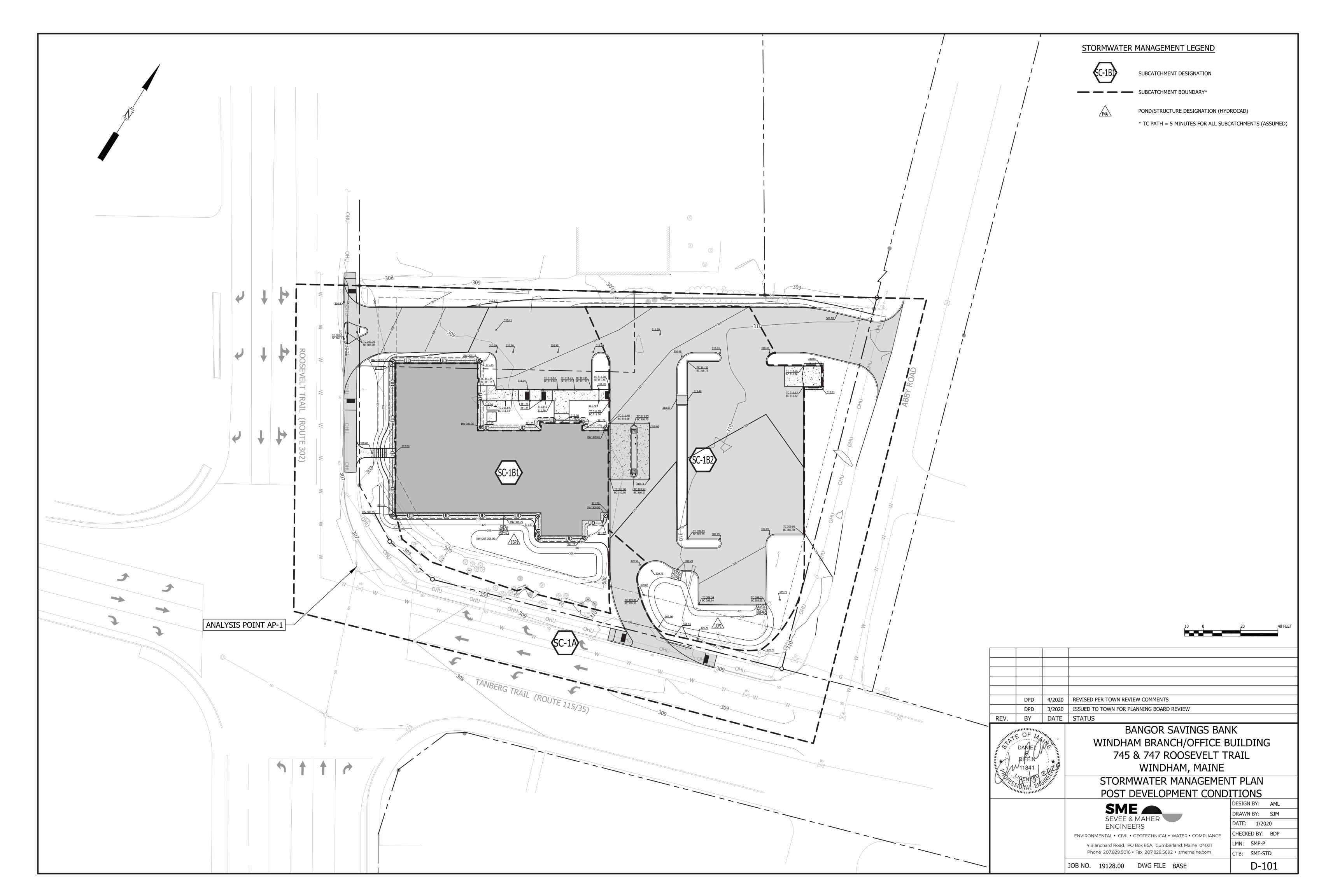
ADA ACCESSIBLE PARKING

**STRIPING** 



4. BOLT ENDWALLS TO STEPS W/ 3/4" BOLT & FLAT WASHER. 5. CENTER HANDRAIL REQUIRED WHERE NOTED ON THE PLANS.

PRECAST CONCRETE STEPS



erverldfs\Bangor Savings Bank\North Windham\Acad\Plans\BASE.dwg, 4/3/2020 12:31:59 PM, sjm